



# ALABAMA DEPARTMENT OF TRANSPORTATION

1409 Coliseum Boulevard, Montgomery, Alabama 36110



## Bureau of Materials and Tests

3700 Fairground Road, Montgomery, Alabama 36110

Phone (334)206-2200 FAX (334)264-6263

*Kay Ivey*  
Governor

*John R. Cooper*  
Transportation Director

July 31, 2018

### Memo

To: **Mr. Matt Erickson, P.E.**  
MRB & Bayway Project Director

From: Ms. Kaye Chancellor Davis, P.E. *AKCD*  
State Geotechnical Engineer

Re: **I-10 Mobile River Bridge- US-98 Interchange**  
**Subsurface Data Report**  
Project No.: **DPI-0030 (005)**  
I-10 Mobile River Bridge  
Mobile County

The Materials & Tests Bureau, Geotechnical Division, has reviewed the Subsurface Data Report. This office agrees with the information held within this report. Please contact this office if there any question or concerns.

AKCD/rld

### Attachments

C: Project File  
File

# REPORT OF GEOTECHNICAL CONSULTING SERVICES

## GEOTECHNICAL SUBSURFACE DATA REPORT

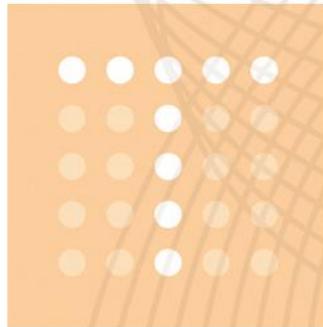
I-10 Mobile River Bridge – US-98 Interchange

Baldwin County, Alabama

ALDOT PE Project No.: DPI-0030(005)

Thompson Engineering Project No.: 17-1101-0145

July 31, 2018



*knowledge • ideas • impact*



July 31, 2018

Mr. Scott W. George, P.E.  
Materials and Test Engineer  
**Alabama Department of Transportation**  
**Bureau of Materials and Test**  
3700 Fairgrounds Road  
Montgomery, Alabama 36130

Attention: **Kaye Chancellor Davis, P.E.**  
**ALDOT Geotechnical Engineer**

Subject: **Report of Geotechnical Consulting Services**  
Subsurface Data Report  
I-10 Mobile River Bridge – US-98 Interchange  
ALDOT PE Project No.: DPI-0030(005)  
Spanish Fort, Baldwin County, Alabama  
Thompson Project No. 17-1101-0145

Dear Ms. Davis:

Thompson Engineering is pleased to transmit this geotechnical subsurface data report for the project referenced above. This submittal summarizes the field exploration and laboratory testing results for the referenced design build operate and maintain project. Our services were performed in general accordance with the Thompson Fee provided in an email dated May 9, 2018.

We appreciate the opportunity to assist the Alabama Department of Transportation with project-related geotechnical matters. Please do not hesitate to contact our office with any questions concerning this submittal.

Respectfully submitted,

**THOMPSON ENGINEERING, INC.**

  
Michael Davis, Jr., P.E.  
Geotechnical Project Engineer

  
Cameron L. Crigler, P.E.  
Geotechnical Team Leader

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- Consolidated Undrained (C.U.) Triaxial Shear Tests
- Unconsolidated Undrained (U.U.) Triaxial Shear Tests
- Direct Shear Test
- One Dimensional Consolidation Tests

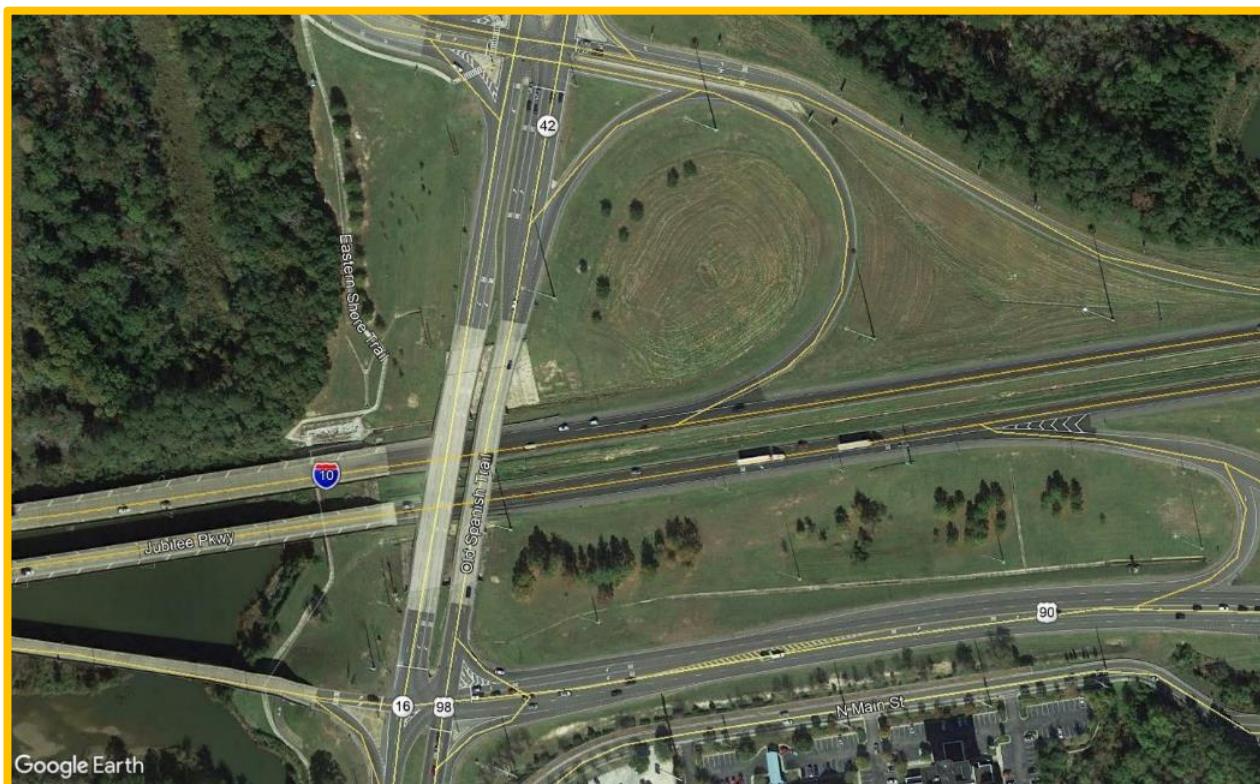
Appendix D – Drill Rig Hammer Energy Efficiency Report

## 1.0 SCOPE OF SERVICES

Thompson Engineering (Thompson) has completed the field exploration and laboratory testing for the US-98 Interchange in support of the overall Mobile River Bridge (MRB) located in Mobile and Baldwin Counties, Alabama. This scope of work was performed in general accordance with the contracted scope of services between the Alabama Department of Transportation (ALDOT) and Thompson, dated July 20, 2017 and in an email dated May 9, 2018. Our services were authorized in the ALDOT Work Order #71,002 on Contract ID #2096.

## 2.0 PROJECT DESCRIPTION

The US-98 Interchange is located along interstate I-10 in Spanish Fort, Baldwin County, Alabama. This portion of the project begins on the southern side of the bridge at approximate station 17+00 and proceeds north to approximate station 27+00 along the US-98 Mainline. The scope of services included landside subsurface exploration and associated laboratory testing for the I-10 modifications in support of the design build or design build operate and maintain (DBFOM) delivery method. The overall intent was to provide subsurface information to the prospective teams in an effort to reduce the risk and unknowns associated with the subsurface conditions. **Figure 1** below depicts the project location and immediate surrounding areas.



*Figure 1: Project location and immediate surrounding area.*

## 3.0 SUBSURFACE EXPLORATION PROGRAM

Thompson geotechnical drilling crews performed soil test borings and sampling operations at the approximate locations shown on the appended Boring Location Plan in **Appendix A**. A Diedrich D-50 track-mounted drilling rig, equipped with an automatic standard penetration test hammer, was utilized to advance the borings using mud rotary drilling techniques. Drilling and field operations took place between May 23, 2017 and June 6, 2017. The hammer energy report for the automatic SPT hammer on the drill rig is attached in **Appendix D** of this report.

Borings were drilled to depths of 150 feet below the existing ground surface as shown on the attached Record of Test Borings in **Appendix B**. Boring locations were surveyed by Thompson Survey crews upon completion.

Brief descriptions of the testing protocols are presented below.

### 3.1 Standard Penetration Test (SPT) Borings

The SPT borings were performed in general accordance with AASHTO T-206 guidelines. Recovered samples were examined and visually classified in the field or in the geotechnical laboratory by a geologist or engineer. Samples were returned to Thompson's geotechnical laboratory for additional testing. The results of the classification and stratification are shown on the appended Record of Test Borings.

### 3.2 Undisturbed Soil Sampling

Undisturbed soil specimens were recovered utilizing thin-wall "Shelby" tube sampling equipment at select depths within soft to firm cohesive soil zones. Undisturbed samples were collected in general accordance AASHTO T-207. The recovered soil samples were sealed and transported to Thompson's geotechnical laboratory.

### 3.3 Cone Penetration Tests

The cone penetration tests were carried out using an integrated electronic piezocone (CPTU). The cone reaction system consisted of a S4 track-mounted rig. The cone was advanced to termination depths at a rate of 2 cm/s. Tip resistance ( $q_c$ ), sleeve friction ( $f_s$ ), and dynamic pore pressure measurements ( $u_2$ ) were recorded every 5 centimeters (2 inches). Pore pressure dissipation data was also obtained at two locations during the cone penetration tests. Testing was performed in general accordance with the methods and procedures described in ASTM Specification D5778-07. Samples are not recovered with cone penetration tests.

The results of the soundings are shown on the CPT logs, presented in **Appendix B**. The corrected tip resistance ( $Q_t$ ) is the recorded tip resistance ( $Q_c$ ) which has been corrected to account for the pore water pressures acting on unequal tip areas of the cone.

## 4.0 LABORATORY TESTING

Samples selected for laboratory testing were assigned by Thompson. **Table 1** provides a quantitative summary of the lab tests performed.

Table 1: Laboratory Testing Summary	
Test Type	Quantity
Atterberg Limits	88
Full Sieve Analysis	88
Consolidation	1
Unconsolidated Undrained (U.U.) Triaxial Shear Tests	3
Consolidated Undrained (C.U.) Triaxial Shear Tests	4
Direct Shear Tests	1

A laboratory test summary table, BMT-5 sheets, and individual test results are included in **Appendix C.**

## 5.0 SUBSURFACE FINDINGS

While establishment of generalized subsurface conditions is useful for the geotechnical engineering evaluation process, such generalizations should be reviewed with caution as they promote extrapolation of recovered data between soil test boring locations. The stratifications shown on the Soil Test Borings represent the conditions only at the actual boring locations. The actual transition between soil types may be more gradual than those depicted.

### 5.1 Groundwater Conditions

Groundwater depth measurements are provided in **Table 2**. Delayed measurements were whenever possible. Fluctuations in groundwater depth measurements can be attributed to elevations and/or drilling techniques used in the field. Groundwater depths depicted on the appended CPT logs were calculated using pore pressure readings obtained in clean sands.

Table 2: Groundwater Depth Measurements						
Boring	Completion of Boring (ft.)	Day 1 (ft.)	Day 2 (ft.)	June 6, 2018 (ft.)	July 10, 2018 (ft.)	Date of Boring Completion
TH-28	Not Obtained	42.5	41.8	41.0	--	June 1
TH-29	Not Obtained	5.6	5.2	4.5	--	June 4
TH-30	18.0	Not Obtained	Not Obtained	18.0	16.1	June 7
TH-31	Not Obtained	16.9	Not Obtained	16.9	--	May 31
TH-32	Not Obtained	32.0	32.6	32.6	--	May 24

Fluctuations of the groundwater level on this project may be expected to occur seasonally as a result of rainfall, surface runoff, tidal issues, and immediate area construction activities.

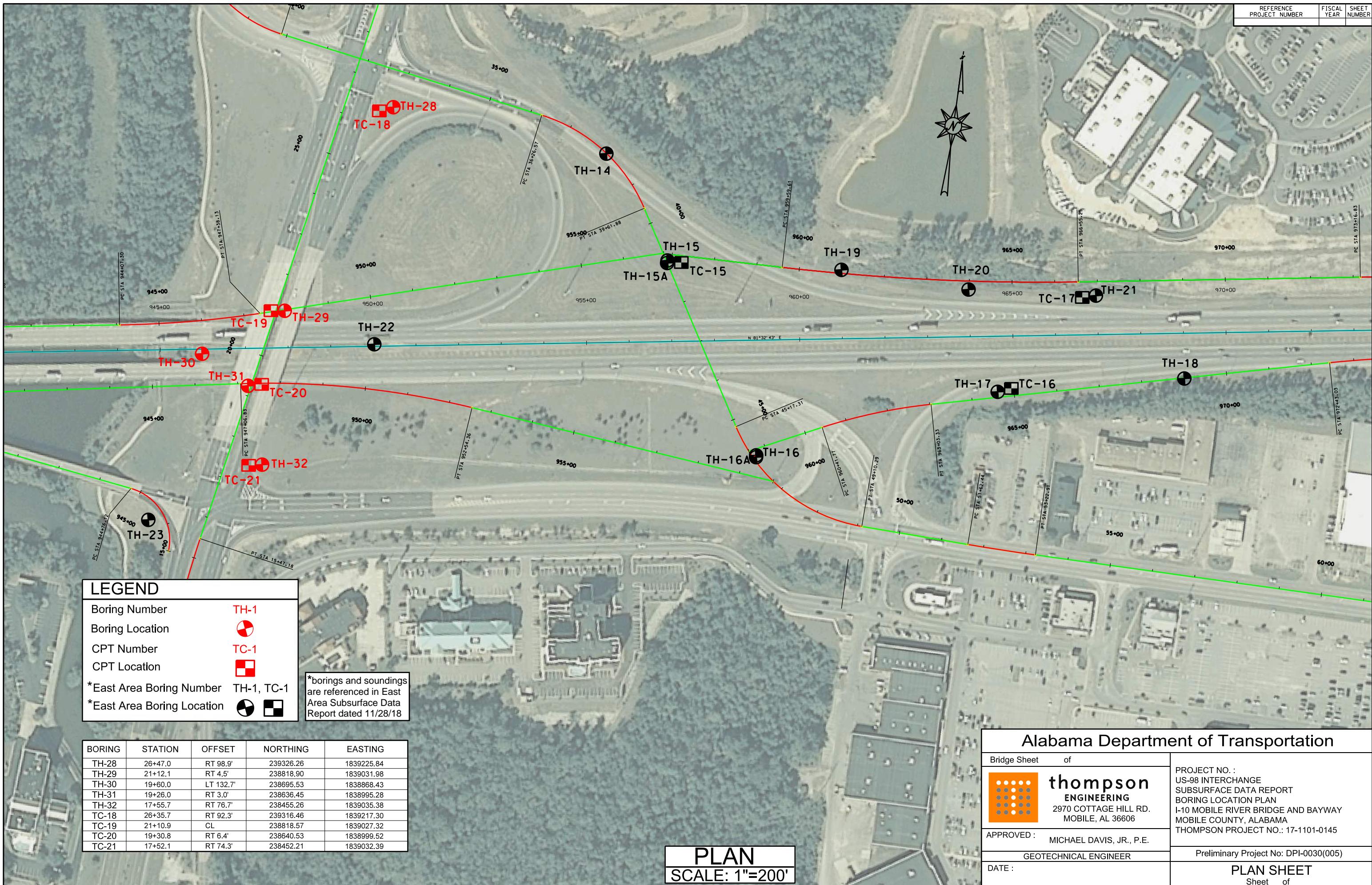
## 6.0 REPORT LIMITATIONS

This Geotechnical Subsurface Data Report has been prepared for the exclusive use of ALDOT for the specific project discussed herein. This Geotechnical Subsurface Data Report has been prepared in accordance with generally accepted local geotechnical engineering practices; no other warranty is expressed or implied. The recovered samples were not examined, either visually or analytically, for chemical composition or environmental hazards.

The observations from field sample recovery, laboratory examination of samples and testing, and computed data analysis, which are presented in this data report, should be considered preliminary investigation and are subject to change upon the acquisition of additional data during the final investigation for the final design. Additional subsurface exploration including borings and laboratory testing for the purposes of evaluating cut slopes, embankment slopes, embankment settlements, retaining walls and bridge foundation types and capacities will be required for final design and applicable to the specific final design layout. The Geotechnical Engineer of Record for the project must review the data submitted in this report and develop their own interpretation of the testing results as they apply to design.

# **APPENDIX A**

- **Boring Location Plan**



## **APPENDIX B**

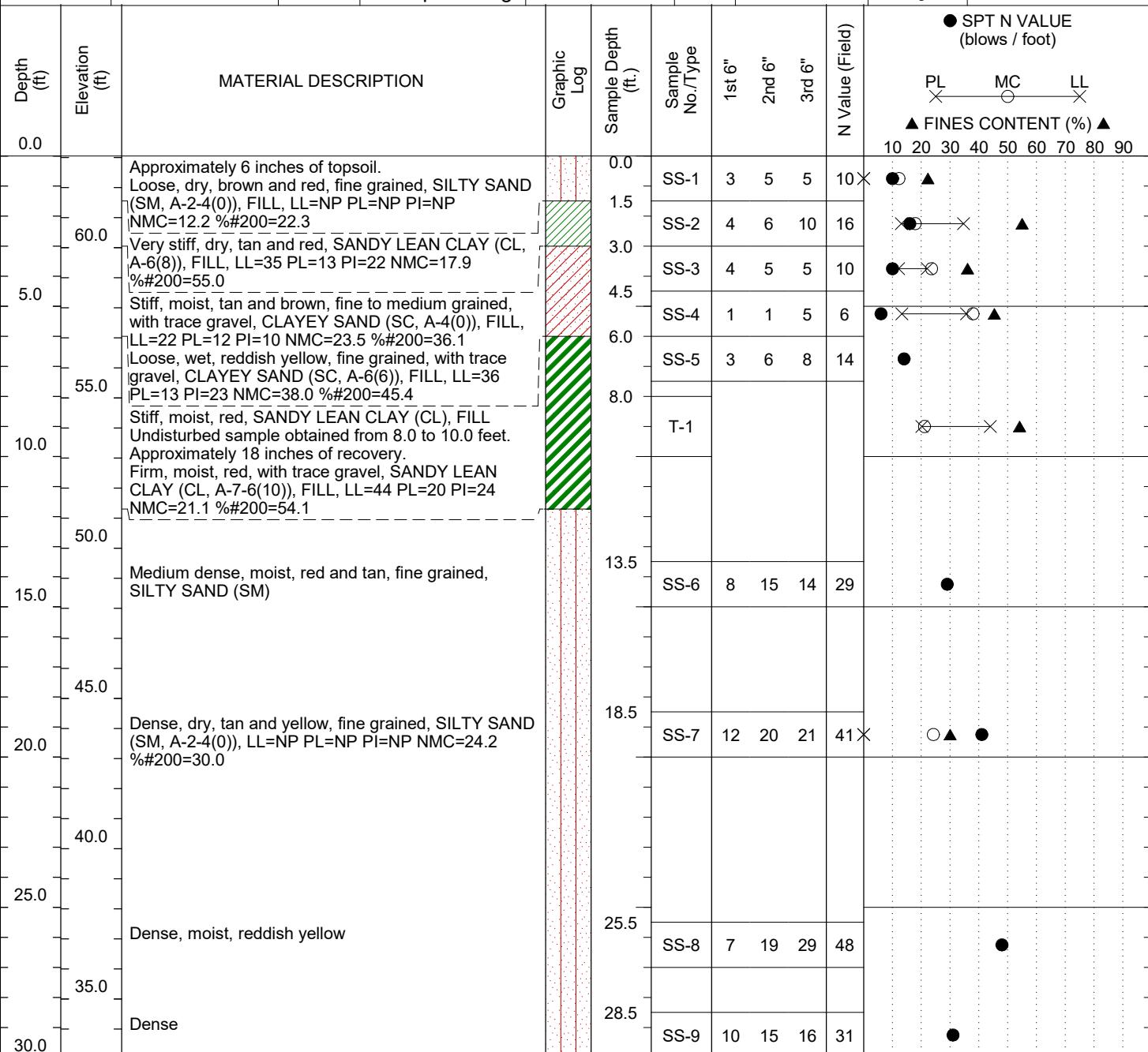
- **Records of Test Borings**
- **CPT Soundings**
- **Legend**



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-28	Boring Location: 26+47.0		Offset: RT 98.9	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 63.1 ft.	Northing: 239326.26	Easting: 1839225.84	Date Started: 5/31/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/1/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	42.5 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County: Mobile				
Boring No.: TH-28	Boring Location: 26+47.0		Offset: RT 98.9	Alignment: US-98							
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick								
Elev.: 63.1 ft.	Northing: 239326.26	Easting: 1839225.84	Date Started: 5/31/2018								
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/1/2018								
Bore Hole Diameter (in): 4-inch AASHTO / ASTM Sampling Methods:				AASHTO T206 & T207							
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%								
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	42.5 ft.						
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	● SPT N VALUE (blows / foot)	PL MC LL
30.0											
30.0											
35.0		Very dense, moist, tan, reddish yellow, fine grained, POORLY GRADED SAND with SILT (SP-SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=25.4 %#200=11.1		33.5	SS-10	27	38	48	86X	▲ ● ○	PL MC LL
35.0											
40.0		Very dense, moist, reddish yellow, fine to medium grained, SILTY SAND (SM)		38.5	SS-11	17	25	29	54	●	
40.0											
45.0		Dense, moist, reddish yellow, fine to medium grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=22.6 %#200=12.6		43.5	SS-12	10	12	25	37X	▲ ○ ●	
45.0											
50.0		Loose, moist, reddish yellow, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=24.4 %#200=31.7		48.5	SS-13	6	5	5	10X	● ○ ▲	
50.0											
55.0		Loose, brown		53.5	SS-14	3	3	3	6	●	
55.0											
60.0		Loose, moist, brown, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=35.2		58.5	SS-15	3	2	3	5X	● ○ ▲	
60.0											

### LEGEND

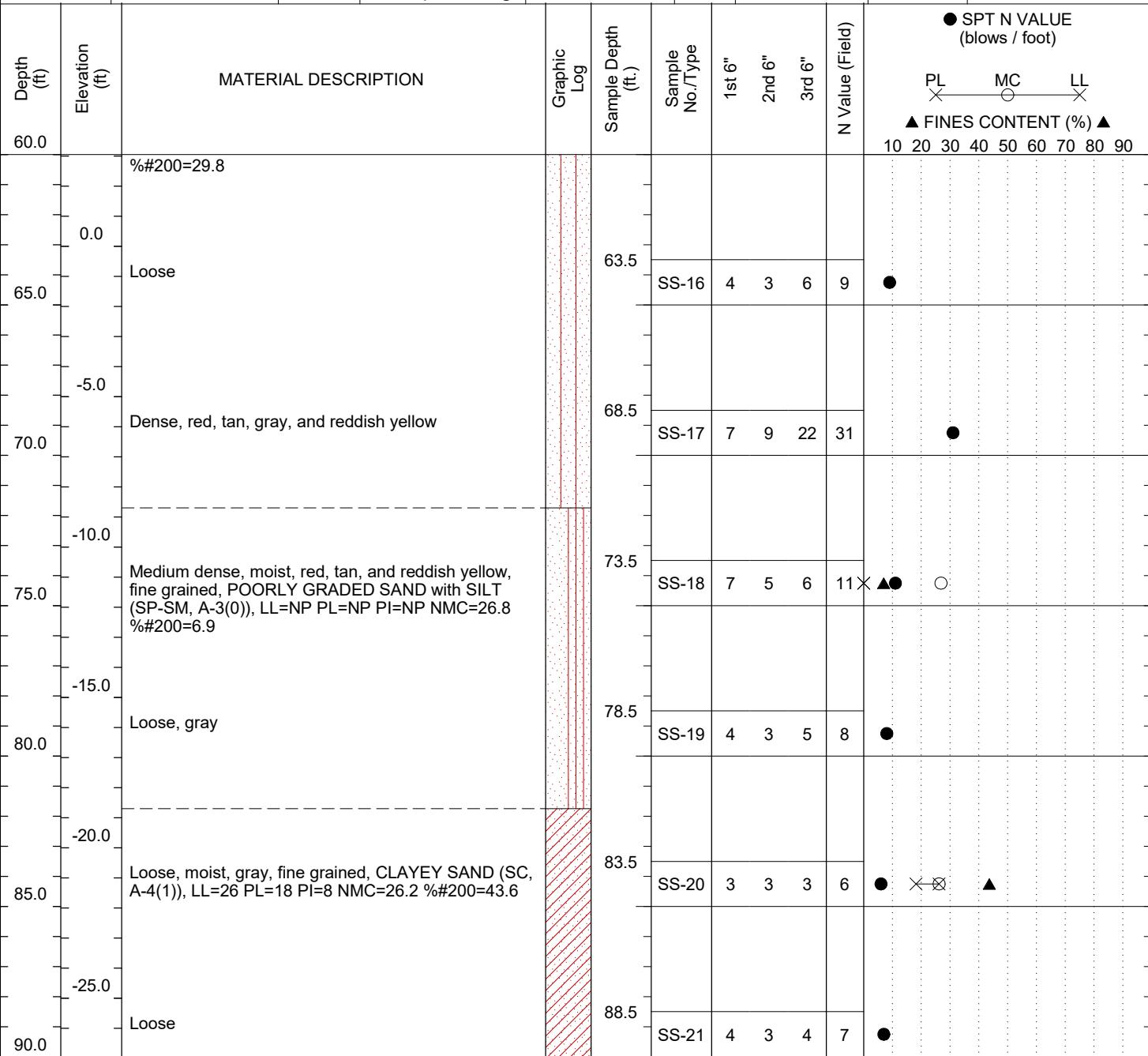
SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
HSA - Hollow Stem Augers	MR - Mud Rotary Wash
SSA - Solid Stem Augers	RC - Rock Coring
HA - Hand Auger	



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ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 63.1 ft.	Northing: 239326.26	Easting: 1839225.84	Date Started: 5/31/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/1/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	42.5 ft.	



### LEGEND

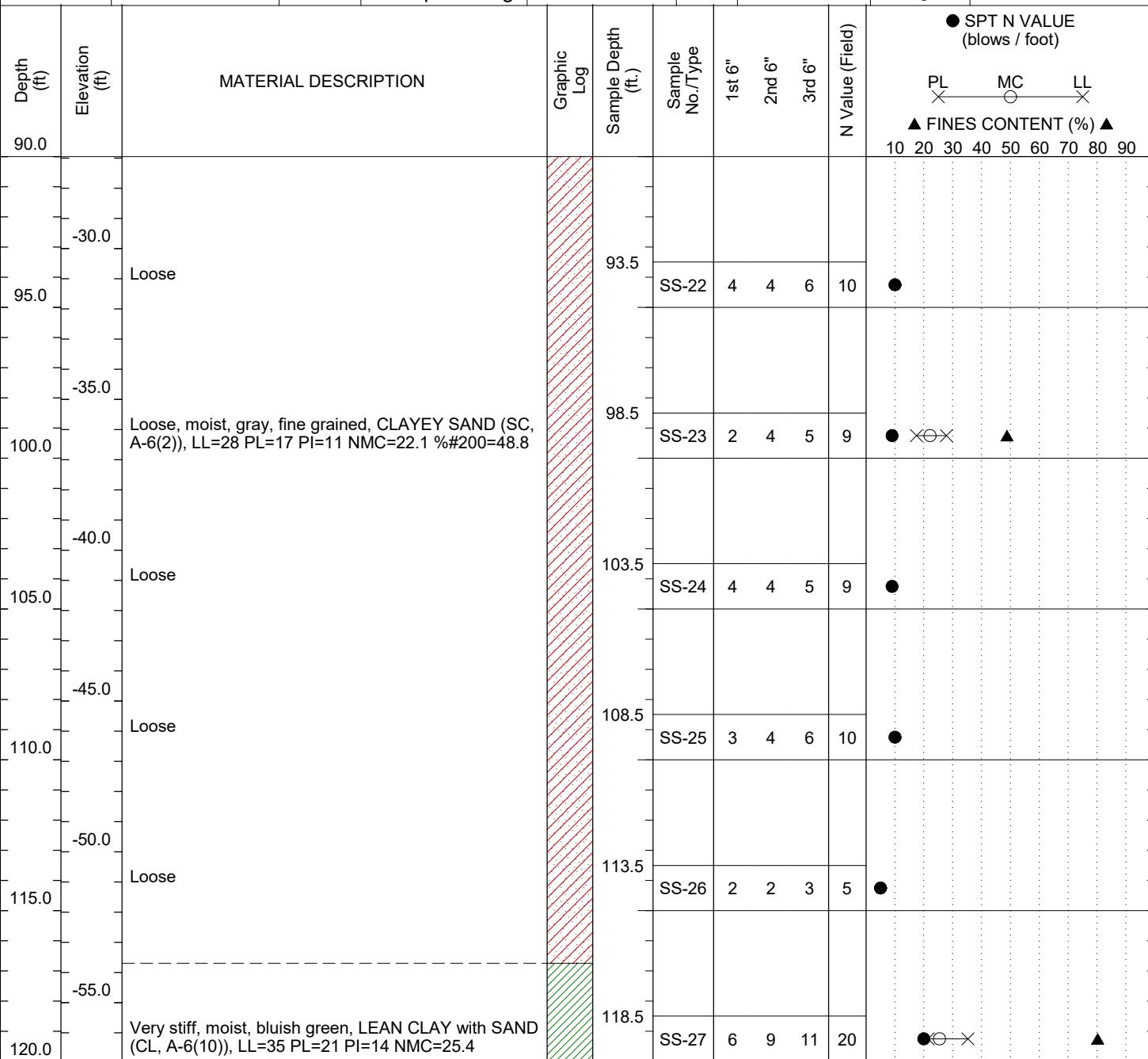
SAMPLER TYPE				DRILLING METHOD			
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Elev.: 63.1 ft.	Northing: 239326.26	Easting: 1839225.84	Date Started:	5/31/2018		
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Bore Hole Diameter (in): 4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207		
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio:	94%		
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	42.5 ft.	



### LEGEND

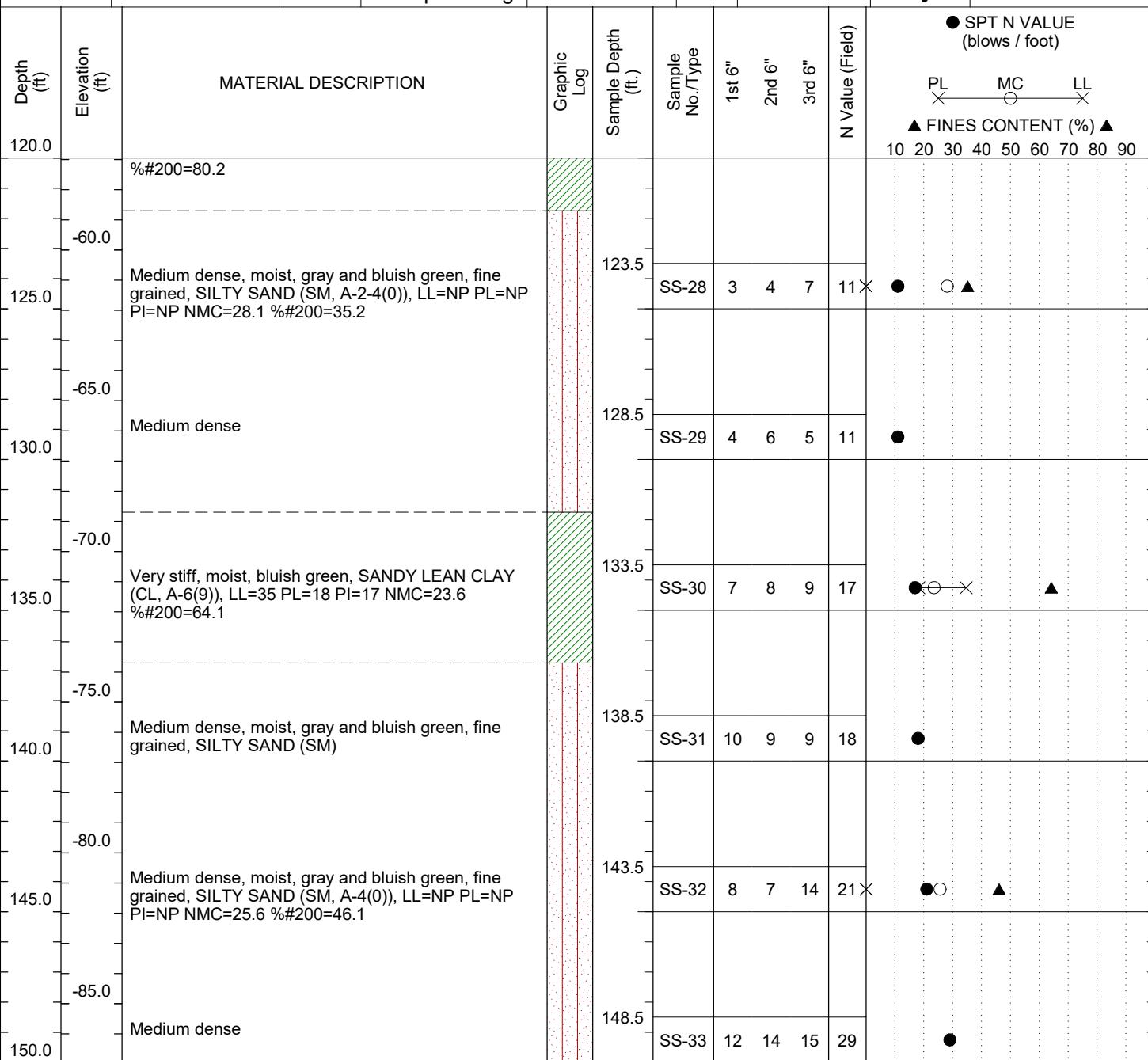
SAMPLER TYPE				DRILLING METHOD			
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Elev.: 63.1 ft.	Northing: 239326.26	Easting: 1839225.84	Date Started: 5/31/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/1/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	42.5 ft.	



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SAMPLER TYPE				DRILLING METHOD			
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## RECORD OF TEST BORING

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Boring No.:	TH-28	Boring Location:	26+47.0	Offset:	RT 98.9	Alignment:	US-98		
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228			Eng./Geo.:	P.McKissick	
Elev.:	63.1 ft.	Northing:	239326.26	Easting:	1839225.84	Date Started:	5/31/2018		
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed:	6/1/2018		
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207				
Drill Machine:	D-50	Drill Method:	MR	Hammer Type:	Automatic		Energy Ratio:	94%	
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	N.O.	Delayed:	42.5 ft.	
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION			Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6" 2nd 6" 3rd 6"	N Value (Field)
		Boring Terminated at 150.0 feet.							● SPT N VALUE (blows / foot)
									PL MC LL
									▲ FINES CONTENT (%) ▲
									10 20 30 40 50 60 70 80 90

### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
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	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County: Mobile					
Boring No.: TH-29	Boring Location: 21+12.1		Offset: RT 4.5	Alignment: US-98								
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick									
Elev.: 20.0 ft.	Northing: 238818.9	Easting: 1839031.98		Date Started: 6/3/2018								
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 6/4/2018								
Bore Hole Diameter (in): 4-inch				AASHTO / ASTM Sampling Methods: AASHTO T206 & T207								
Drill Machine: D-50	Drill Method: MR		Hammer Type: Automatic	Energy Ratio: 94%								
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed: 5.6 ft.								
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	● SPT N VALUE (blows / foot)	PL MC LL	▲ FINES CONTENT (%) ▲
0.0	20.0	Approximately 4 inches of topsoil. Medium dense, dry, brown and red, fine to medium grained, with trace gravel and organics, CLAYEY SAND (SC), FILL		0.0	SS-1	7	8	9	17	●	X	
		Medium dense, moist, red, fine to medium grained, CLAYEY SAND (SC, A-2-4(0)), FILL, LL=21 PL=12 PI=9 NMC=13.5 %#200=25.6		1.5	SS-2	6	5	8	13	● X	○	▲
5.0	15.0	Firm, moist, tan and brown, with trace gravel, FAT CLAY with SAND (CH, A-7-6(32)), FILL, LL=55 PL=17 PI=38 NMC=28.6 %#200=81.8		3.0	SS-3	3	2	3	5	● X	○	
		Very loose, wet, reddish brown, fine grained, CLAYEY SAND with GRAVEL (SC, A-6(3)), FILL, LL=37 PL=13 PI=24 NMC=45.9 %#200=36.5		4.5	SS-4	2	1	2	3	● X	○	▲
		Firm, moist, tan and brown, with few sand, LEAN CLAY (CL), FILL		6.0	SS-5	2	1	3	4	●		
10.0	10.0	Undisturbed sample obtained from 8.5 to 10.0 feet. Approximately 24 inches of recovery.		8.5	T-1					X	○ X	▲
		Moist, pale brown, with few sand, LEAN CLAY (CL, A-7-6(25)), FILL, LL=44 PL=16 PI=28 NMC=37.8 %#200=87.8		13.5	SS-6	4	4	4	8	●		
15.0	5.0	Loose, moist, yellow, fine grained, POORLY GRADED SAND with SILT (SP-SM)		18.5	SS-7	6	5	6	11X	●	○	
		Medium dense, moist, yellow, fine grained, POORLY GRADED SAND with SILT (SP-SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=26.4 %#200=10.7		23.5	SS-8	5	2	2	4	●		
20.0	0.0	Very loose		28.5	SS-9	2	2	2	4	● X O	▲	
25.0	-5.0	Very loose, moist, yellow, fine grained, SILTY, CLAYEY SAND (SC-SM, A-2-4(0)), LL=25 PL=18										
30.0												

### LEGEND

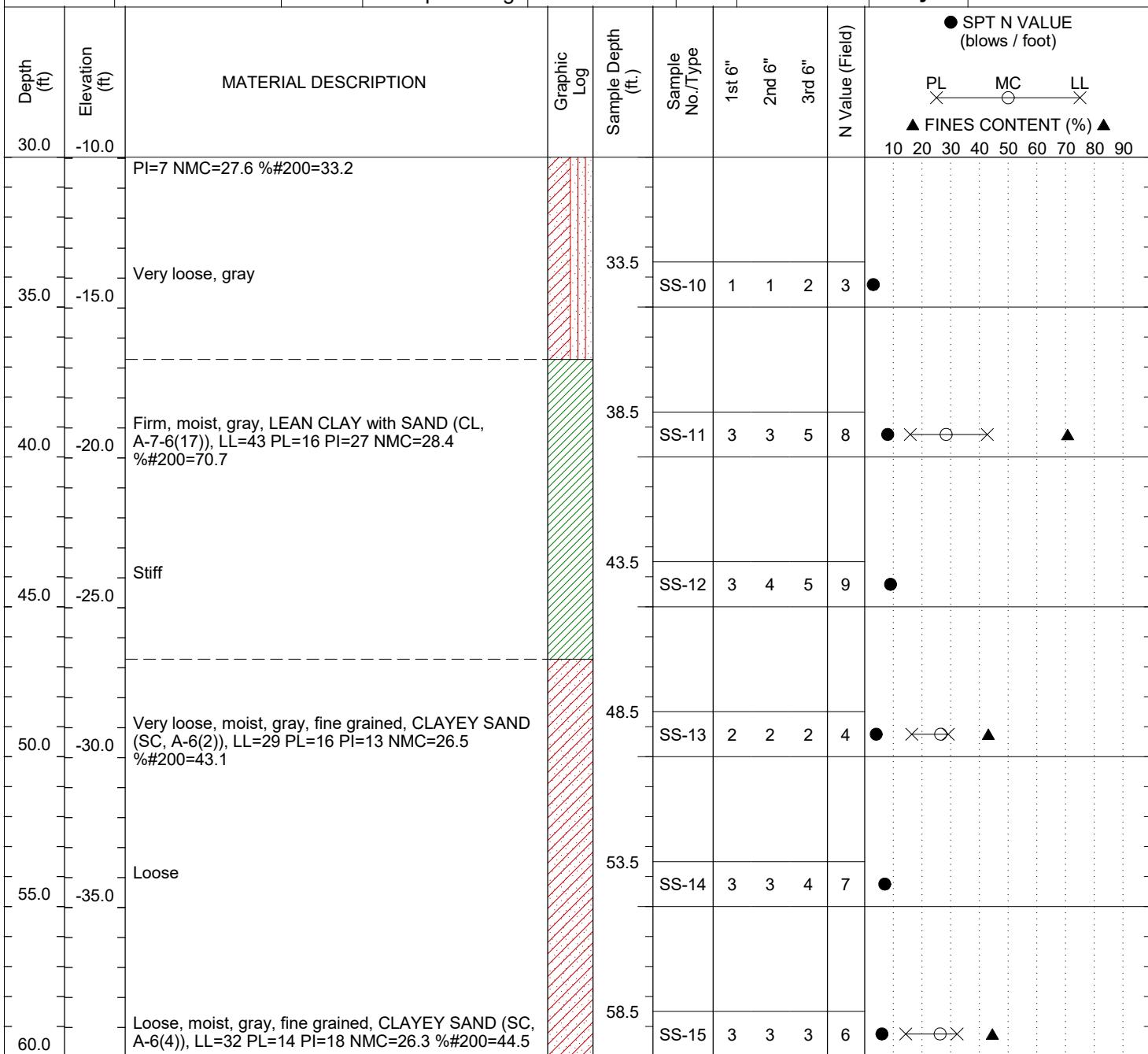
SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



**thompson**  
ENGINEERING

## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-29	Boring Location: 21+12.1		Offset: RT 4.5	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 20.0 ft.	Northing: 238818.9	Easting: 1839031.98	Date Started: 6/3/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/4/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed: 5.6 ft.		



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County: Mobile					
Boring No.: TH-29	Boring Location: 21+12.1		Offset: RT 4.5	Alignment: US-98								
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick									
Elev.: 20.0 ft.	Northing: 238818.9	Easting: 1839031.98		Date Started: 6/3/2018								
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 6/4/2018								
Bore Hole Diameter (in): 4-inch				AASHTO / ASTM Sampling Methods: AASHTO T206 & T207								
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic		Energy Ratio: 94%								
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	5.6 ft.							
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	● SPT N VALUE (blows / foot)	PL MC LL	▲ FINES CONTENT (%) ▲
60.0	-40.0											
65.0	-45.0	Medium dense		63.5	SS-16	5	5	7	12	●		
70.0	-50.0	Medium dense, moist, gray, fine grained, CLAYEY SAND (SC, A-6(2)), LL=31 PL=16 PI=15 NMC=23.0 %#200=40.7		68.5	SS-17	4	5	7	12	● X O X ▲		
75.0	-55.0	Medium dense, moist, gray, fine grained, SILTY, CLAYEY SAND (SC-SM)		73.5	SS-18	4	7	7	14	●		
80.0	-60.0	Medium dense, moist, gray, fine grained, SILTY, CLAYEY SAND (SC-SM, A-2-4(0)), LL=26 PL=19 PI=7 NMC=24.9 %#200=29.2		78.5	SS-19	5	6	7	13	● X O X ▲		
85.0	-65.0	Medium dense		83.5	SS-20	4	6	8	14	●		
90.0	-70.0	Medium dense, moist, gray, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP		88.5	SS-21	10	12	11	23*	● X		

### LEGEND

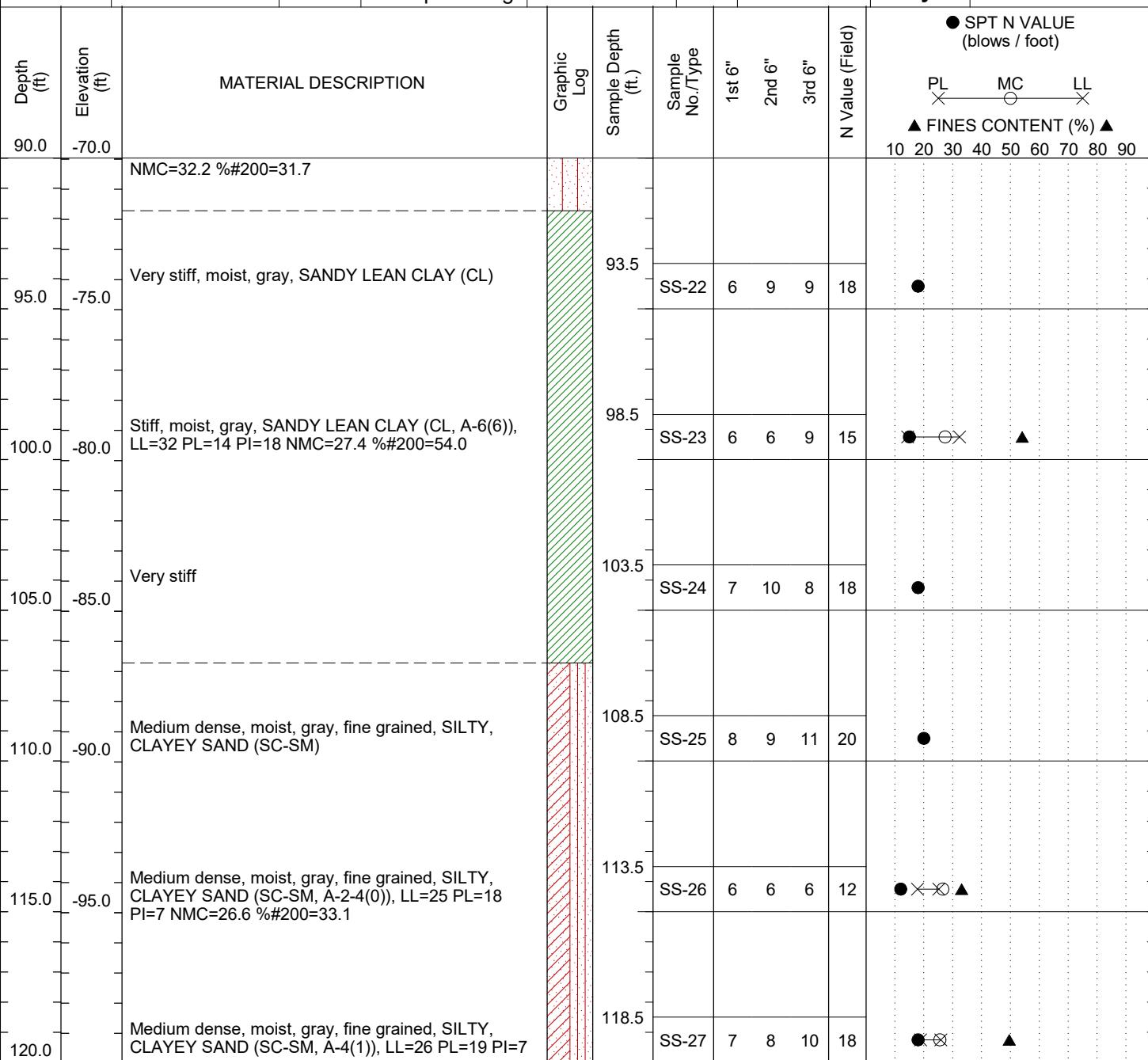
SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
HSA - Hollow Stem Augers	MR - Mud Rotary Wash
SSA - Solid Stem Augers	RC - Rock Coring
HA - Hand Auger	



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-29	Boring Location: 21+12.1		Offset: RT 4.5	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 20.0 ft.	Northing: 238818.9	Easting: 1839031.98	Date Started: 6/3/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/4/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	5.6 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County: Mobile					
Boring No.: TH-29	Boring Location: 21+12.1		Offset: RT 4.5	Alignment: US-98								
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick									
Elev.: 20.0 ft.	Northing: 238818.9	Easting: 1839031.98		Date Started: 6/3/2018								
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 6/4/2018								
Bore Hole Diameter (in): 4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207								
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic		Energy Ratio: 94%								
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	5.6 ft.							
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	● SPT N VALUE (blows / foot)	PL MC LL	▲ FINES CONTENT (%) ▲
120.0	-100.0	NMC=25.5 %#200=49.6										
125.0	-105.0	Stiff, moist, gray, SANDY LEAN CLAY (CL)		123.5	SS-28	4	4	9	13	●		
130.0	-110.0	Very stiff		128.5	SS-29	7	7	10	17	●		
135.0	-115.0	Hard, moist, gray and bluish green, SANDY LEAN CLAY (CL, A-6(11)), LL=40 PL=21 PI=19 NMC=24.3 %#200=65.9		133.5	SS-30	10	14	40	54	X X ● ▲		
140.0	-120.0	Hard		138.5	SS-31	14	16	19	35	●		
145.0	-125.0	Hard		143.5	SS-32	21	23	22	45	●		
150.0		Dense, moist, gray and bluish gray, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP		148.5	SS-33	16	25	25	50 X	▲ ●		

### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	HSA - Hollow Stem Augers
T - Shelby Tube	SSA - Solid Stem Augers
DCP - Dynamic Cone Penetrometer	HA - Hand Auger
AC - Auger Cuttings	MR - Mud Rotary Wash
GB - Grab Bag	RC - Rock Coring
NQ - Rock Core	



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County:	Mobile	
Boring No.:	TH-29	Boring Location:	21+12.1	Offset:	RT 4.5	Alignment:	US-98		
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228			Eng./Geo.:	P.McKissick	
Elev.:	20.0 ft.	Northing:	238818.9	Easting:	1839031.98	Date Started:	6/3/2018		
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed:	6/4/2018		
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207				
Drill Machine:	D-50	Drill Method:	MR	Hammer Type:	Automatic		Energy Ratio:	94%	
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	N.O.	Delayed:	5.6 ft.	
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION			Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6" 2nd 6" 3rd 6"	N Value (Field)
		NMC=26.8 %#200=25.3 Boring Terminated at 150.0 feet.							● SPT N VALUE (blows / foot)
									PL MC LL
									▲ FINES CONTENT (%) ▲
									10 20 30 40 50 60 70 80 90

### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County: Mobile				
Boring No.: TH-30	Boring Location: 19+60.0		Offset: LT 132.7	Alignment: US-98							
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick								
Elev.: 22.5 ft.	Northing: 238695.53	Easting: 1838868.43		Date Started: 6/6/2018							
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 6/7/2018							
Bore Hole Diameter (in): 4-inch				AASHTO / ASTM Sampling Methods: AASHTO T206 & T207							
Drill Machine: D50	Drill Method: MR		Hammer Type: Automatic	Energy Ratio: 94%							
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	18.0 ft.	Delayed:	16.1 ft.						
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION	Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	SPT N VALUE (blows / foot)	PL MC LL
0.0		Approximately 12 inches of topsoil. Loose, moist, brown, fine grained, with trace organics, SILTY SAND (SM, A-2-4(0)), FILL, LL=NP PL=NP PI=NP NMC=14.2 %#200=29.7		0.0	SS-1	2	2	3	5	● X ○ ▲	X O ▲
20.0		Loose, moist, red, fine to medium grained, with trace gravel and trace organics, CLAYEY SAND (SC, A-2-4(0)), FILL, LL=21 PL=11 PI=10 NMC=10.2 %#200=31.5		1.5	SS-2	3	3	5	8	● X X ▲	O X ▲
5.0		Very loose, moist, red, fine grained, CLAYEY SAND (SC, A-6(3)), FILL, LL=26 PL=12 PI=14 NMC=21.5 %#200=49.6		3.0	SS-3	2	1	1	2	● X ○	● ▲
15.0		Very soft, wet, red, brown and tan, with trace gravel, SANDY LEAN CLAY (CL, A-6(4)), FILL, LL=28 PL=13 PI=15 NMC=27.4 %#200=51.2		4.5	SS-4	1	1	1	2	● X ○	● ▲
10.0		Very soft, moist, red, reddish brown Firm, moist, red, brown and tan, LEAN CLAY with SAND (CL, A-7-6(26)), FILL, LL=46 PL=14 PI=32 NMC=29.0 %#200=82.8		6.0	SS-5	6	1	1	2	●	
15.0		Undisturbed sample obtained from 13.5 to 15.5 feet. Approximately 24 inches of recovery. Wet, brown and gray, with few sand, FAT CLAY (CH, A-7-6(36)), LL=57 PL=19 PI=38 NMC=55.5 %#200=87.7		8.5	SS-6	2	2	3	5	● X ○ X	▲
20.0		Medium dense, moist, yellow, fine to medium grained, POORLY GRADED SAND with SILT (SP-SM, A-3(0)), LL=NP PL=NP PI=NP NMC=19.9 %#200=5.9		13.5	T-1					X ○	▲
25.0		Medium dense, moist, yellow, fine to medium grained, SILTY, CLAYEY SAND (SC-SM, A-2-4(0)), LL=20 PL=15 PI=5 NMC=24.9 %#200=17.1		18.5	SS-7	10	9	11	20	● X ▲	
30.0		Loose, moist, yellow, tan, and red, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP		23.5	SS-8	10	8	8	16	● X ○	
				28.5	SS-9	3	3	3	6	● X ○ ▲	

### LEGEND

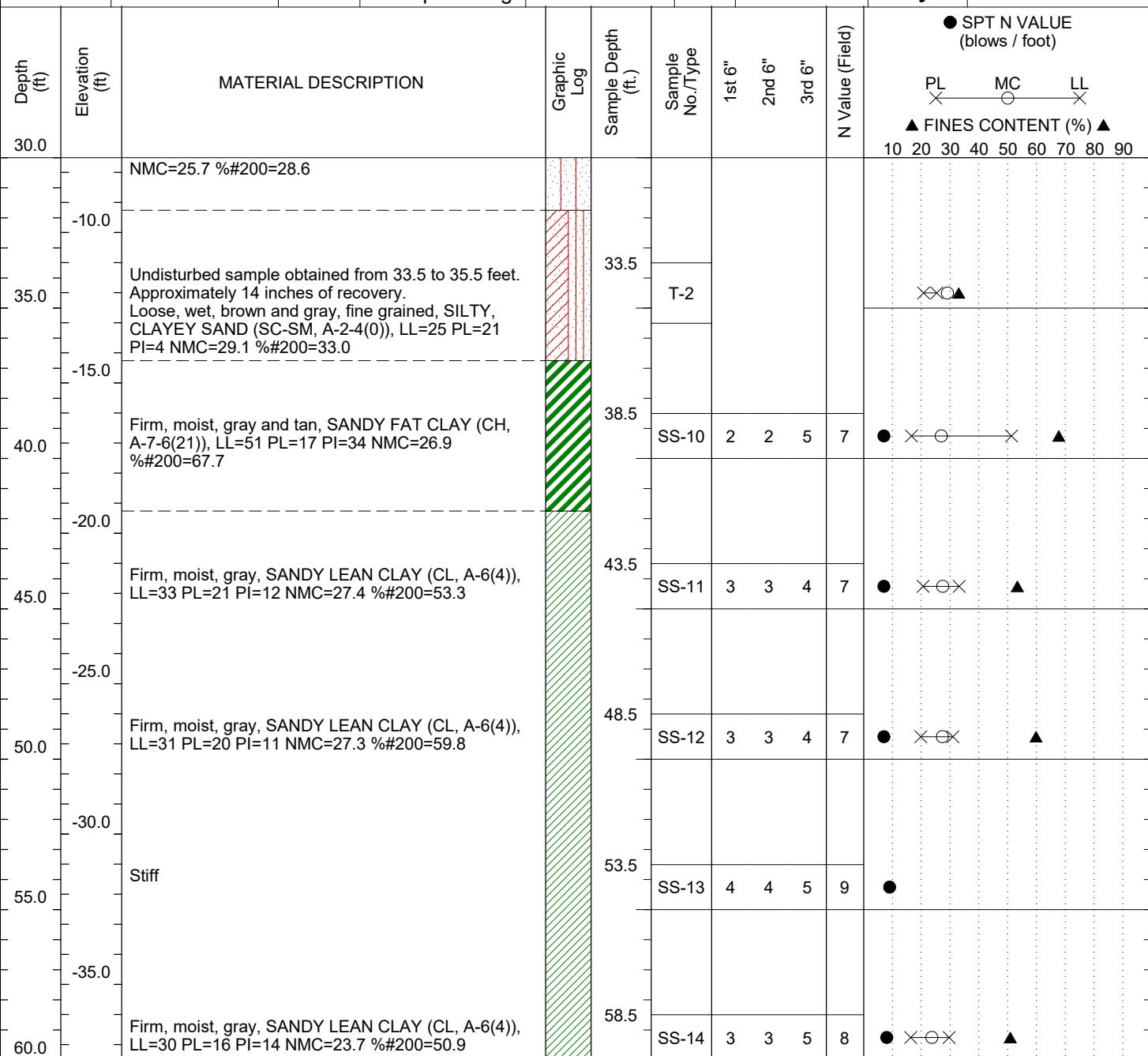
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-30	Boring Location: 19+60.0		Offset: LT 132.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 22.5 ft.	Northing: 238695.53	Easting: 1838868.43	Date Started: 6/6/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/7/2018			
Bore Hole Diameter (in): 4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207		
Drill Machine: D50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	18.0 ft.	Delayed:	16.1 ft.	



### LEGEND

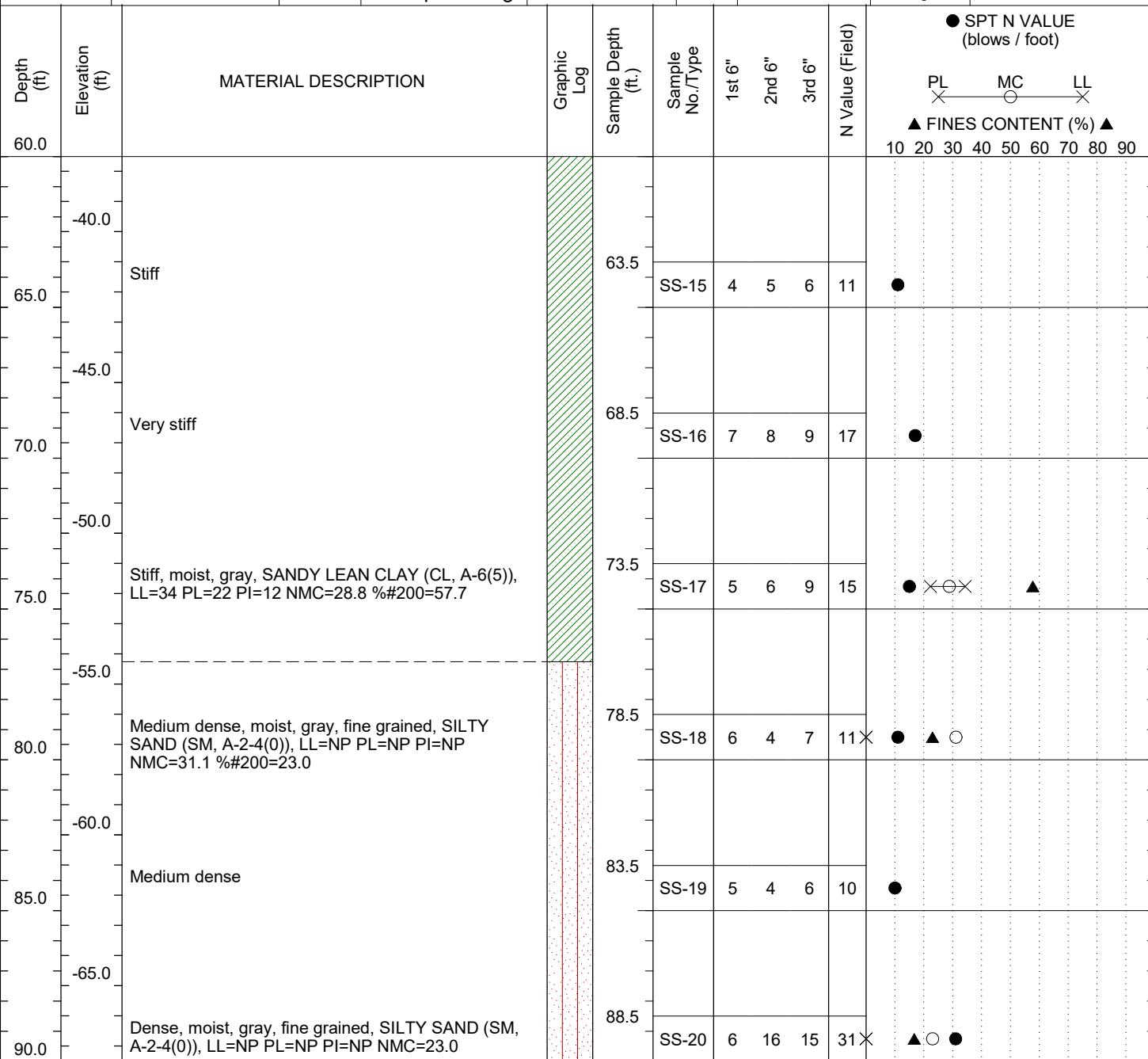
SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	HSA - Hollow Stem Augers
T - Shelby Tube	SSA - Solid Stem Augers
DCP - Dynamic Cone Penetrometer	HA - Hand Auger
AC - Auger Cuttings	MR - Mud Rotary Wash
GB - Grab Bag	RC - Rock Coring
NQ - Rock Core	



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-30	Boring Location: 19+60.0		Offset: LT 132.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 22.5 ft.	Northing: 238695.53	Easting: 1838868.43	Date Started: 6/6/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 6/7/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	18.0 ft.	Delayed:	16.1 ft.	



### LEGEND

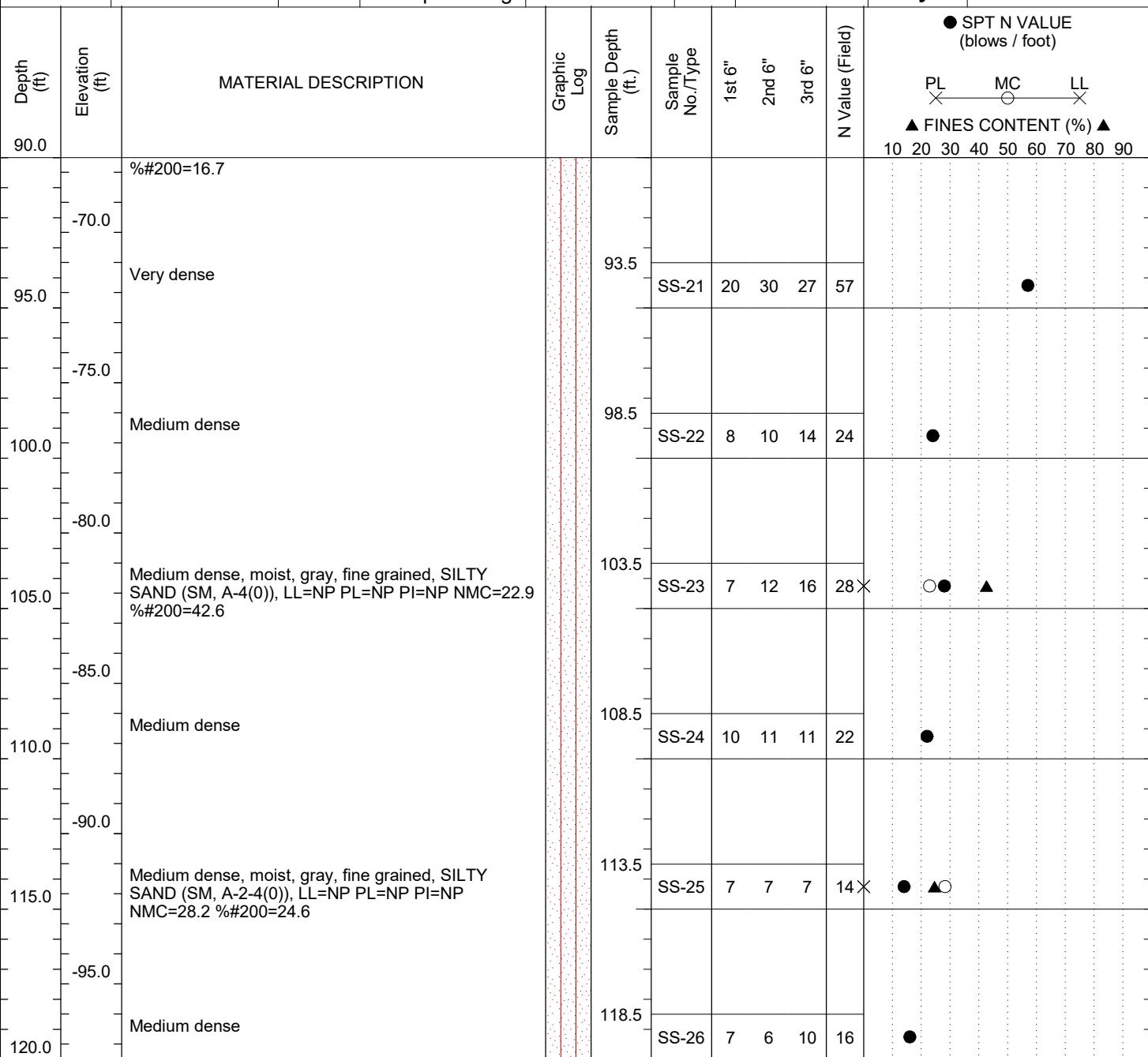
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County:	Mobile	
Boring No.:	TH-30	Boring Location:		19+60.0	Offset:	LT 132.7	Alignment:	US-98
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228		Eng./Geo.:	P.McKissick	
Elev.:	22.5 ft.	Northing:	238695.53		Easting:	1838868.43		Date Started: 6/6/2018
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed: 6/7/2018		
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207			
Drill Machine:	D50	Drill Method:	MR	Hammer Type:	Automatic		Energy Ratio: 94%	
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	18.0 ft.	Delayed: 16.1 ft.	



### LEGEND

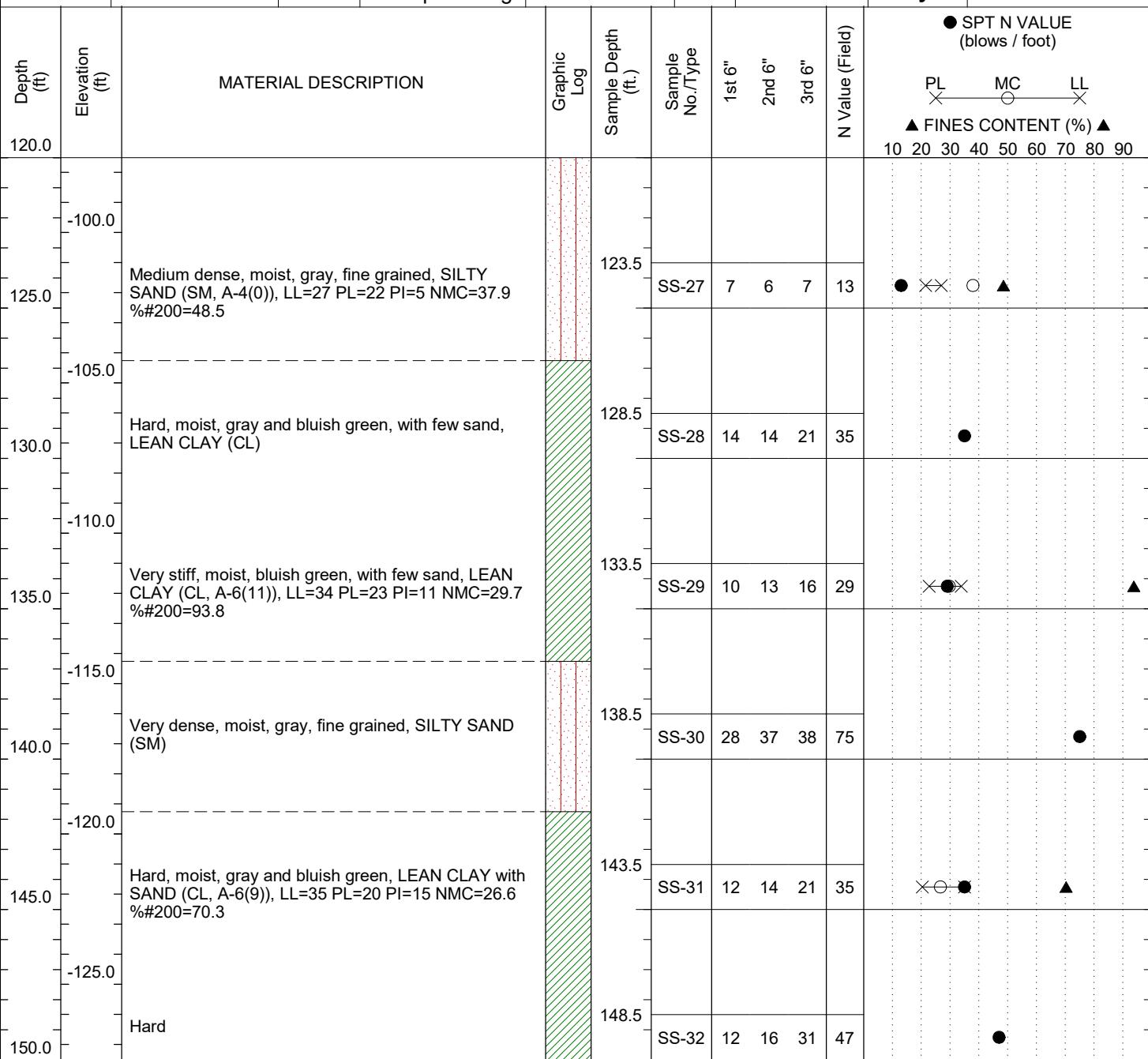
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County:	Mobile	
Boring No.:	TH-30	Boring Location:		19+60.0	Offset:	LT 132.7	Alignment:	US-98
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228		Eng./Geo.:	P.McKissick	
Elev.:	22.5 ft.	Northing:	238695.53		Easting:	1838868.43		Date Started: 6/6/2018
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed: 6/7/2018		
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207			
Drill Machine:	D50	Drill Method:	MR	Hammer Type:	Automatic		Energy Ratio: 94%	
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	18.0 ft.	Delayed: 16.1 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway							County:	Mobile	
Boring No.:	TH-30	Boring Location:	19+60.0	Offset:	LT 132.7	Alignment:	US-98		
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228		Eng./Geo.:	P.McKissick		
Elev.:	22.5 ft.	Northing:	238695.53	Easting:	1838868.43	Date Started:	6/6/2018		
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed:	6/7/2018		
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207				
Drill Machine:	D50	Drill Method:	MR	Hammer Type:	Automatic	Energy Ratio:	94%		
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	18.0 ft.	Delayed:	16.1 ft.	
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION			Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6" 2nd 6" 3rd 6"	N Value (Field)
		Boring Terminated at 150.0 feet.							● SPT N VALUE (blows / foot)
									PL MC LL
									▲ FINES CONTENT (%) ▲
									10 20 30 40 50 60 70 80 90

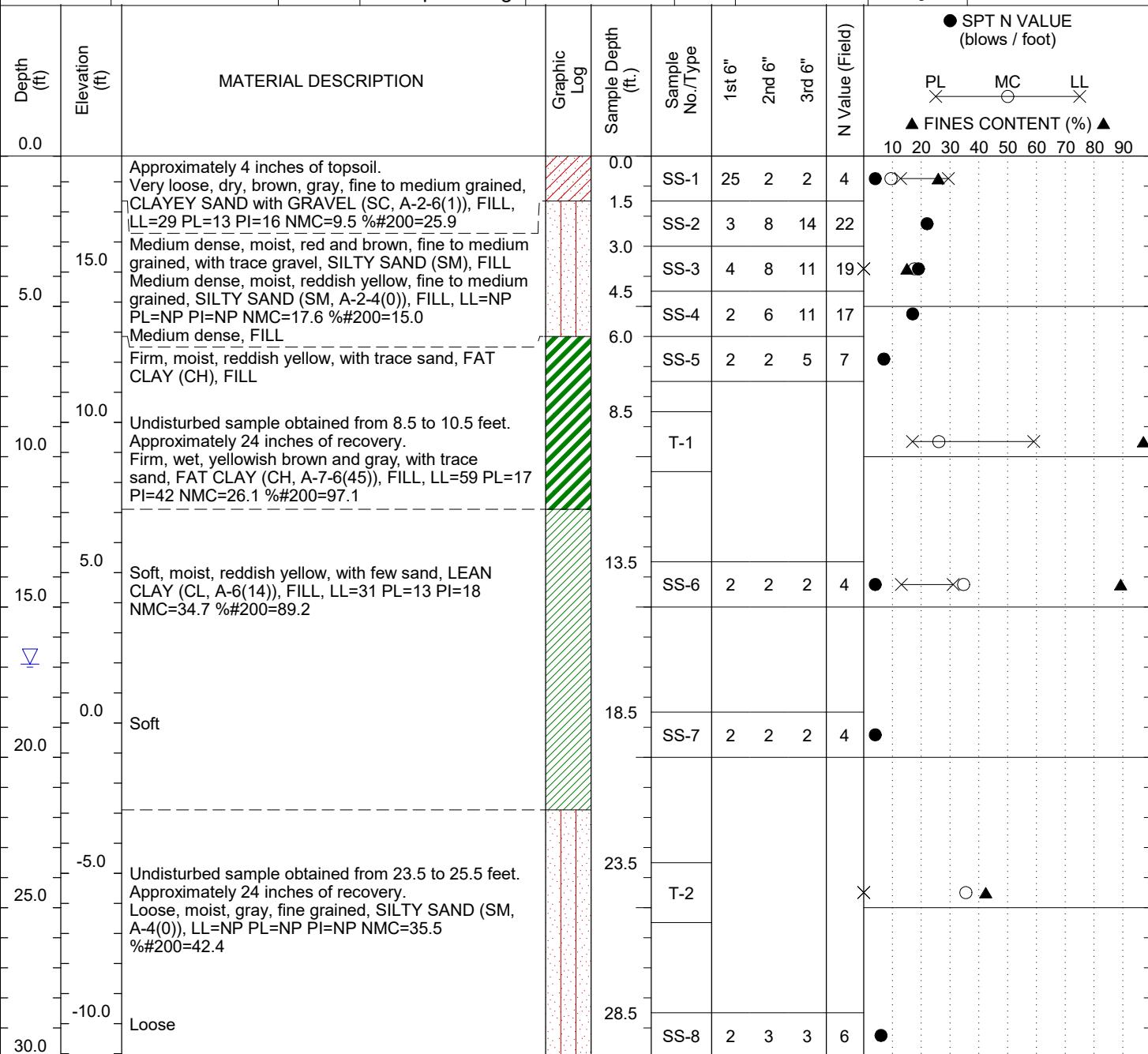
### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-31	Boring Location: 19+26.0		Offset: RT 3.0	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 18.9 ft.	Northing: 238636.45	Easting: 1838995.28	Date Started: 5/29/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 5/31/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed: 16.9 ft.		



### LEGEND

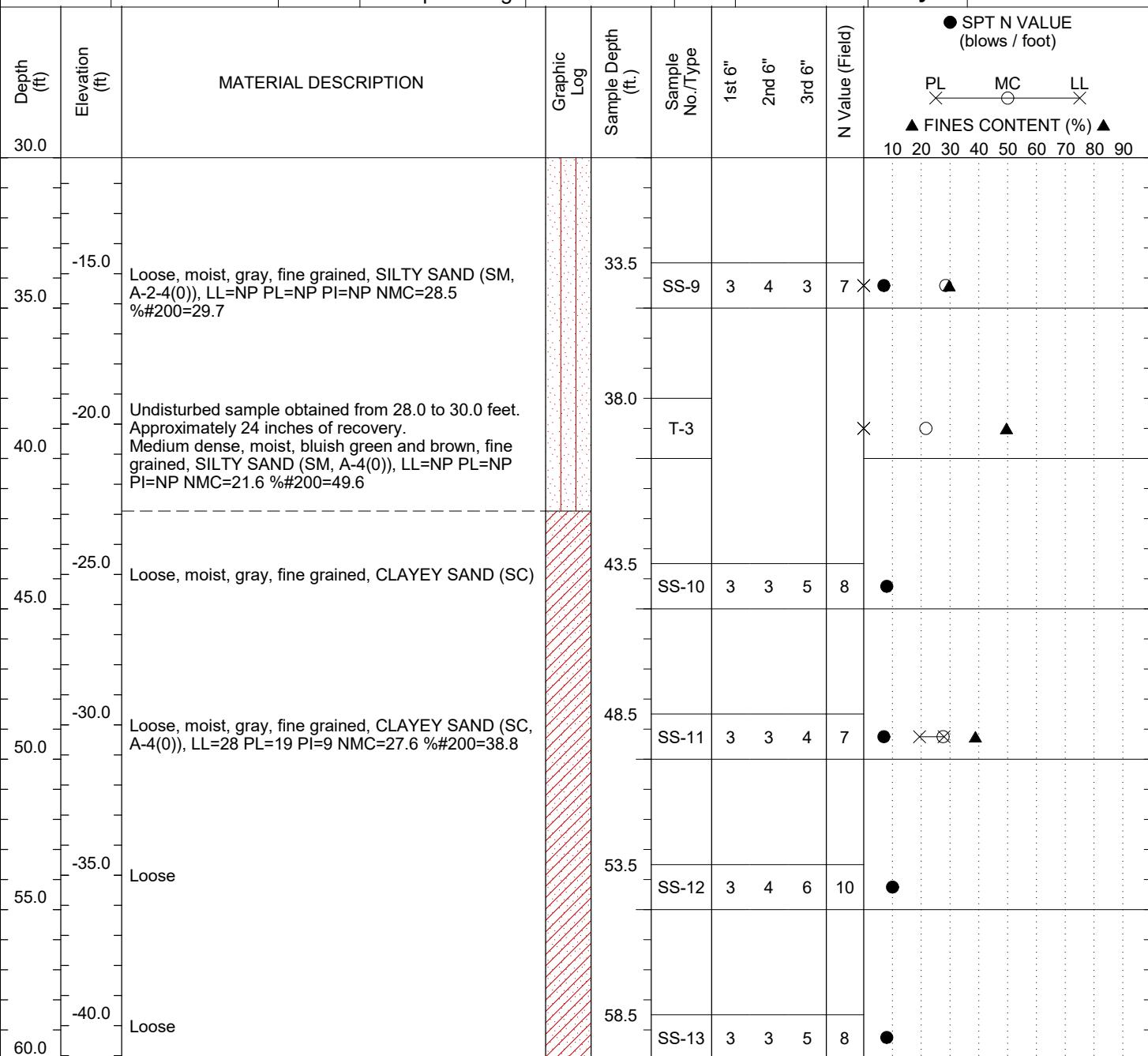
SAMPLER TYPE			DRILLING METHOD		
SS - Split Spoon	AC - Auger Cuttings		HSA - Hollow Stem Augers	MR - Mud Rotary Wash	
T - Shelby Tube	GB - Grab Bag		SSA - Solid Stem Augers	RC - Rock Coring	
DCP - Dynamic Cone Penetrometer	NQ - Rock Core		HA - Hand Auger		



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-31	Boring Location: 19+26.0		Offset: RT 3.0	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 18.9 ft.	Northing: 238636.45	Easting: 1838995.28	Date Started: 5/29/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 5/31/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	16.9 ft.	



### LEGEND

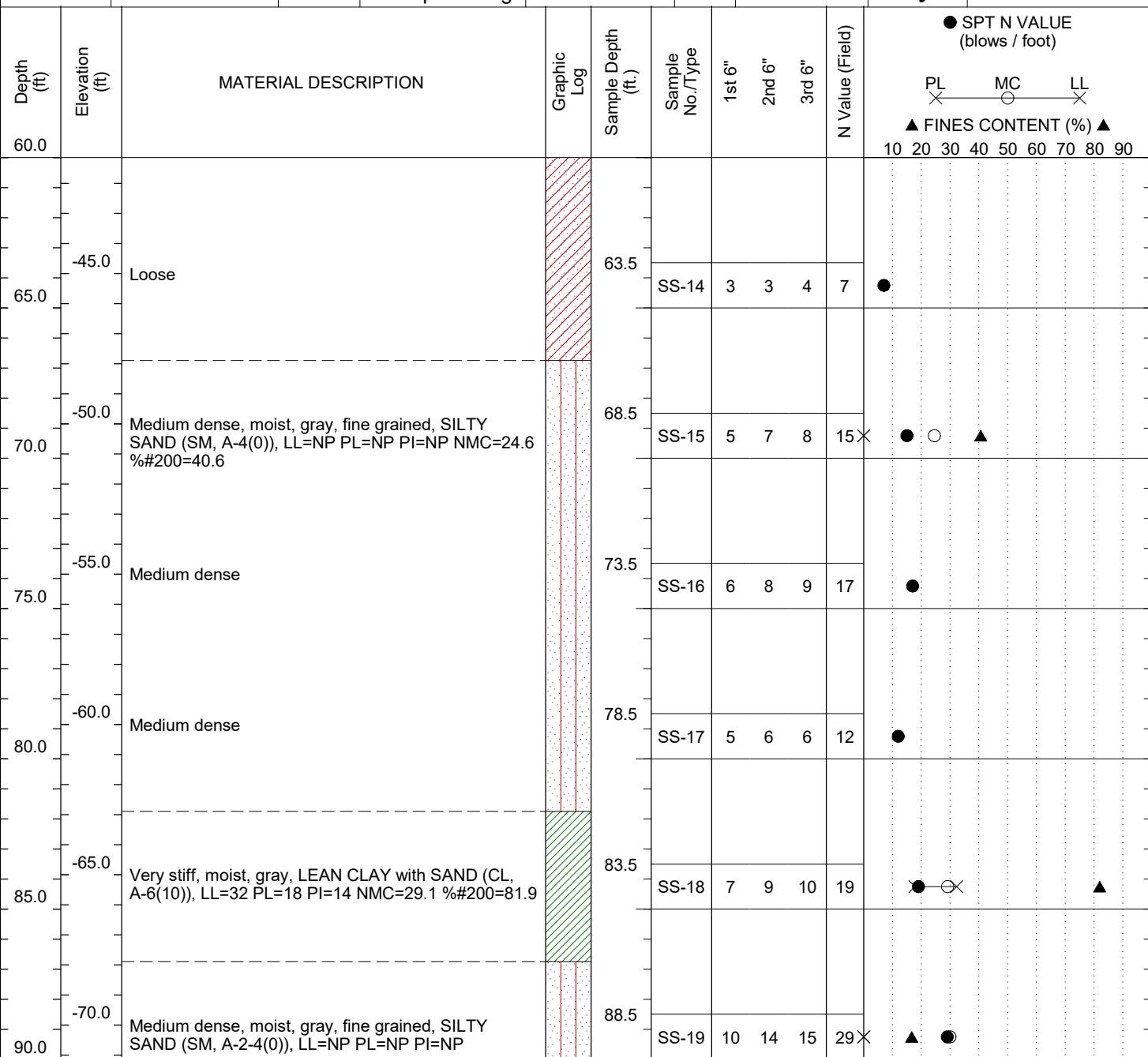
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-31	Boring Location: 19+26.0		Offset: RT 3.0	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 18.9 ft.	Northing: 238636.45	Easting: 1838995.28	Date Started: 5/29/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 5/31/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	16.9 ft.	



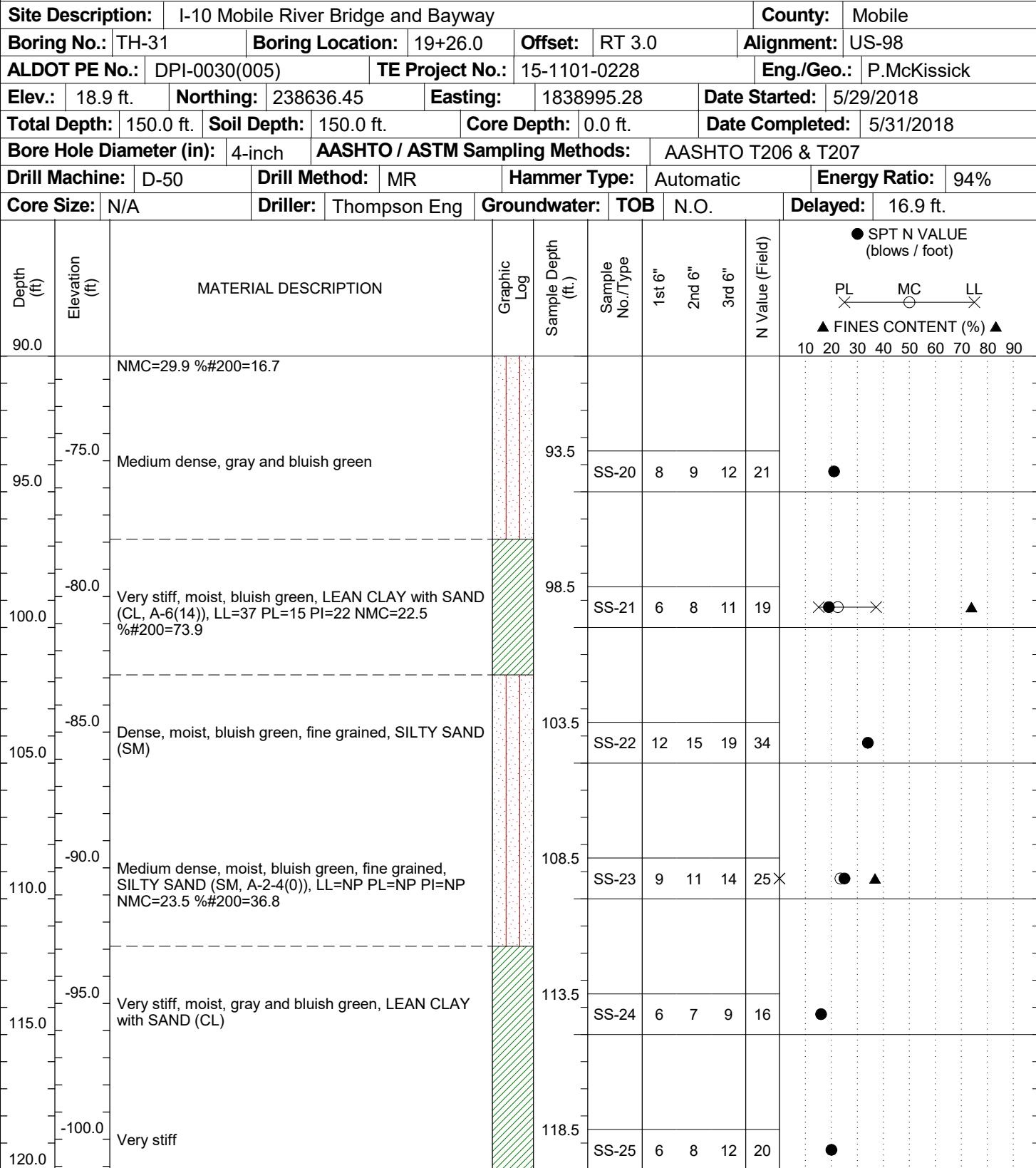
### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING



### LEGEND

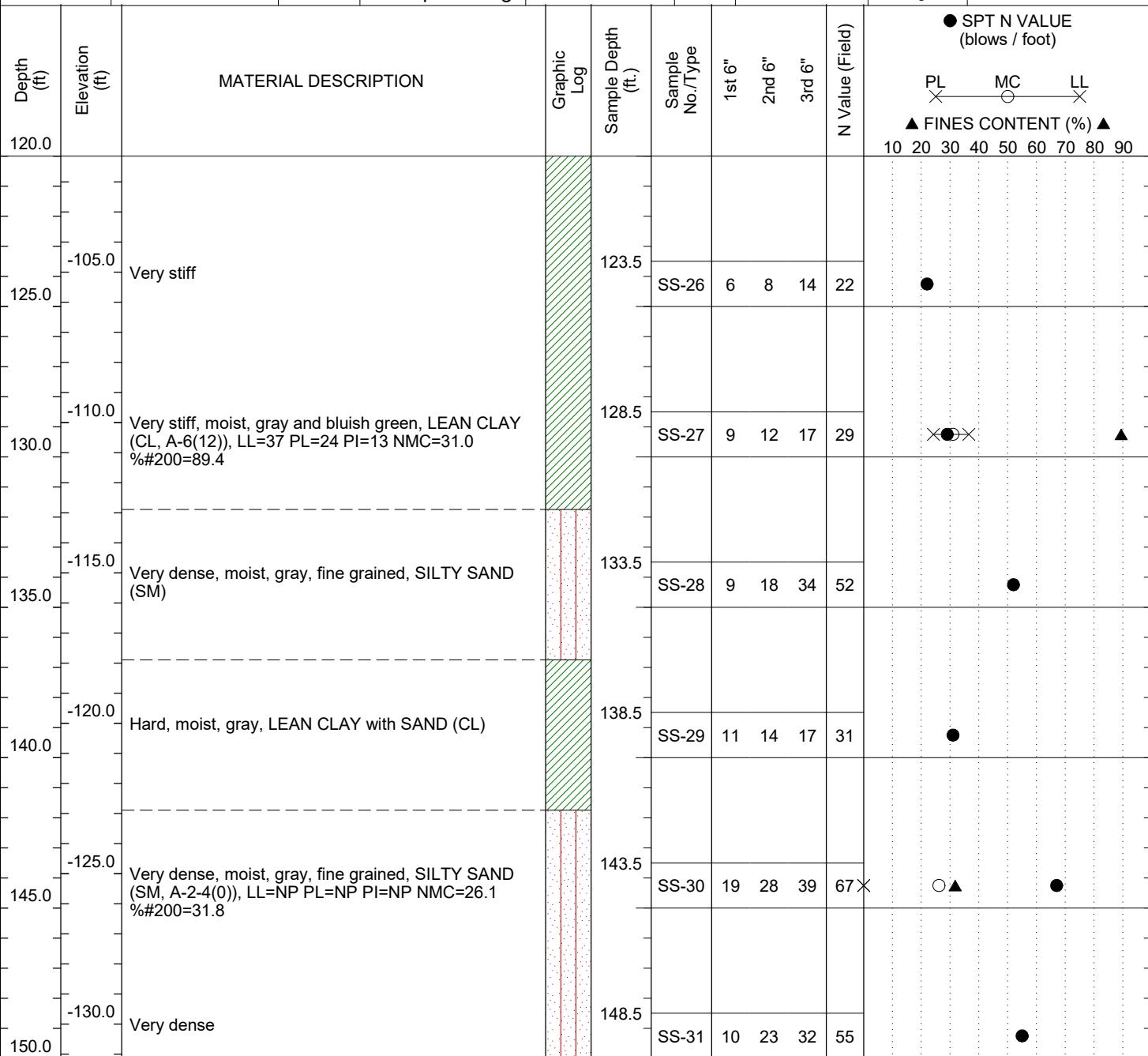
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-31	Boring Location: 19+26.0		Offset: RT 3.0	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 18.9 ft.	Northing: 238636.45	Easting: 1838995.28	Date Started: 5/29/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 5/31/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	16.9 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway								County:	Mobile			
Boring No.:	TH-31	Boring Location:		19+26.0	Offset:	RT 3.0	Alignment:					
ALDOT PE No.:	DPI-0030(005)			TE Project No.:	15-1101-0228			Eng./Geo.:	P.McKissick			
Elev.:	18.9 ft.	Northing:	238636.45		Easting:	1838995.28		Date Started:	5/29/2018			
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.		Core Depth:	0.0 ft.		Date Completed:	5/31/2018			
Bore Hole Diameter (in): 4-inch				AASHTO / ASTM Sampling Methods:				AASHTO T206 & T207				
Drill Machine:	D-50	Drill Method:	MR		Hammer Type:	Automatic		Energy Ratio:	94%			
Core Size:	N/A	Driller:	Thompson Eng		Groundwater:	TOB	N.O.	Delayed:	16.9 ft.			
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION				Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6" 2nd 6" 3rd 6"	N Value (Field)		
		Boring Terminated at 150.0 feet.								● SPT N VALUE (blows / foot)		
										PL MC LL		
										▲ FINES CONTENT (%) ▲		
										10 20 30 40 50 60 70 80 90		

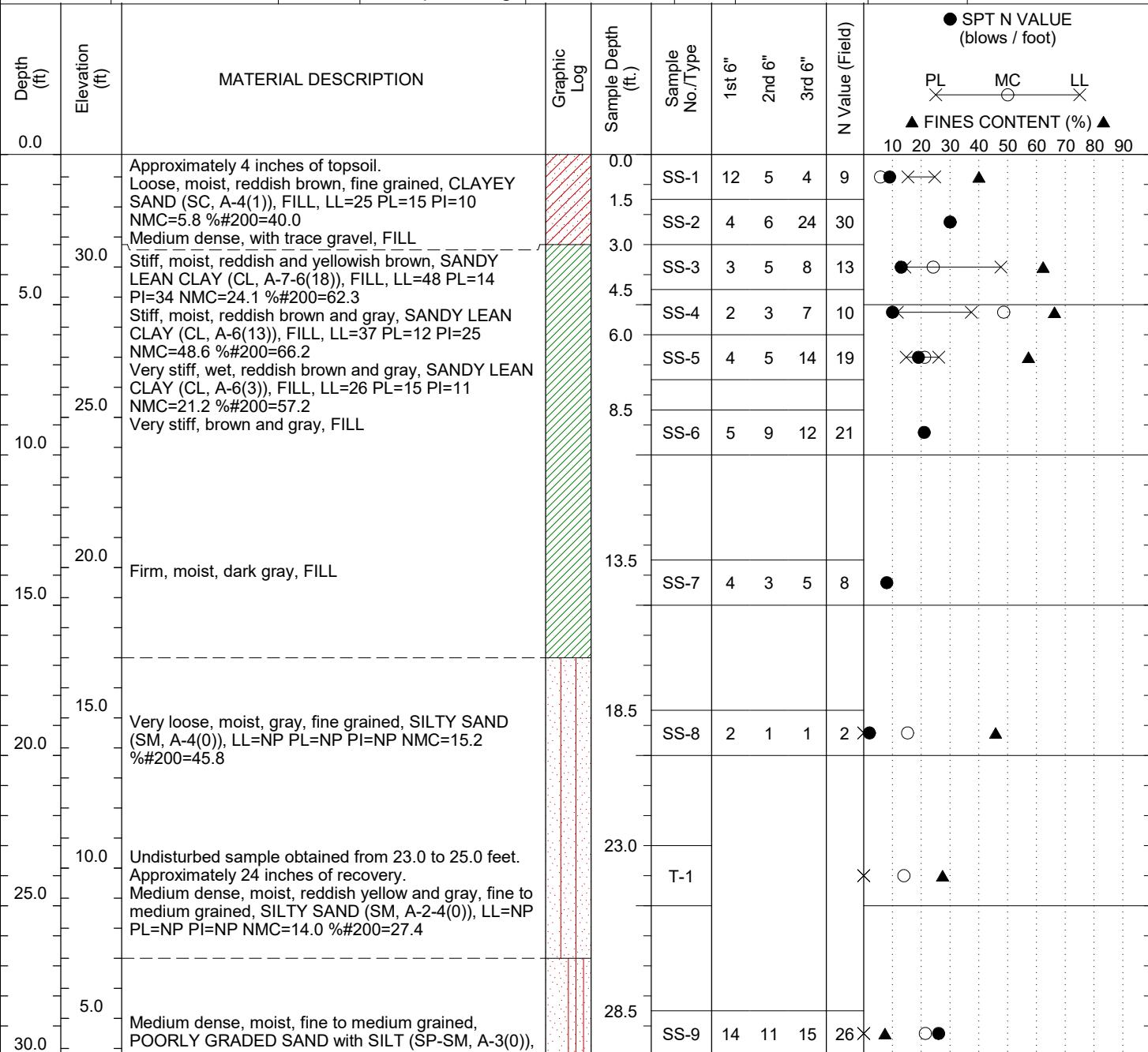
### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile		
Boring No.: TH-32	Boring Location: 17+55.7		Offset: RT 76.7	Alignment: US-98				
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick					
Elev.: 33.8 ft.	Northing: 238455.26	Easting: 1839035.38	Date Started:	5/23/2018				
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed:	5/24/2018				
Bore Hole Diameter (in): 4-inch		AASHTO / ASTM Sampling Methods:		AASHTO T206 & T207				
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio:	94%				
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	32.0 ft.			



### LEGEND

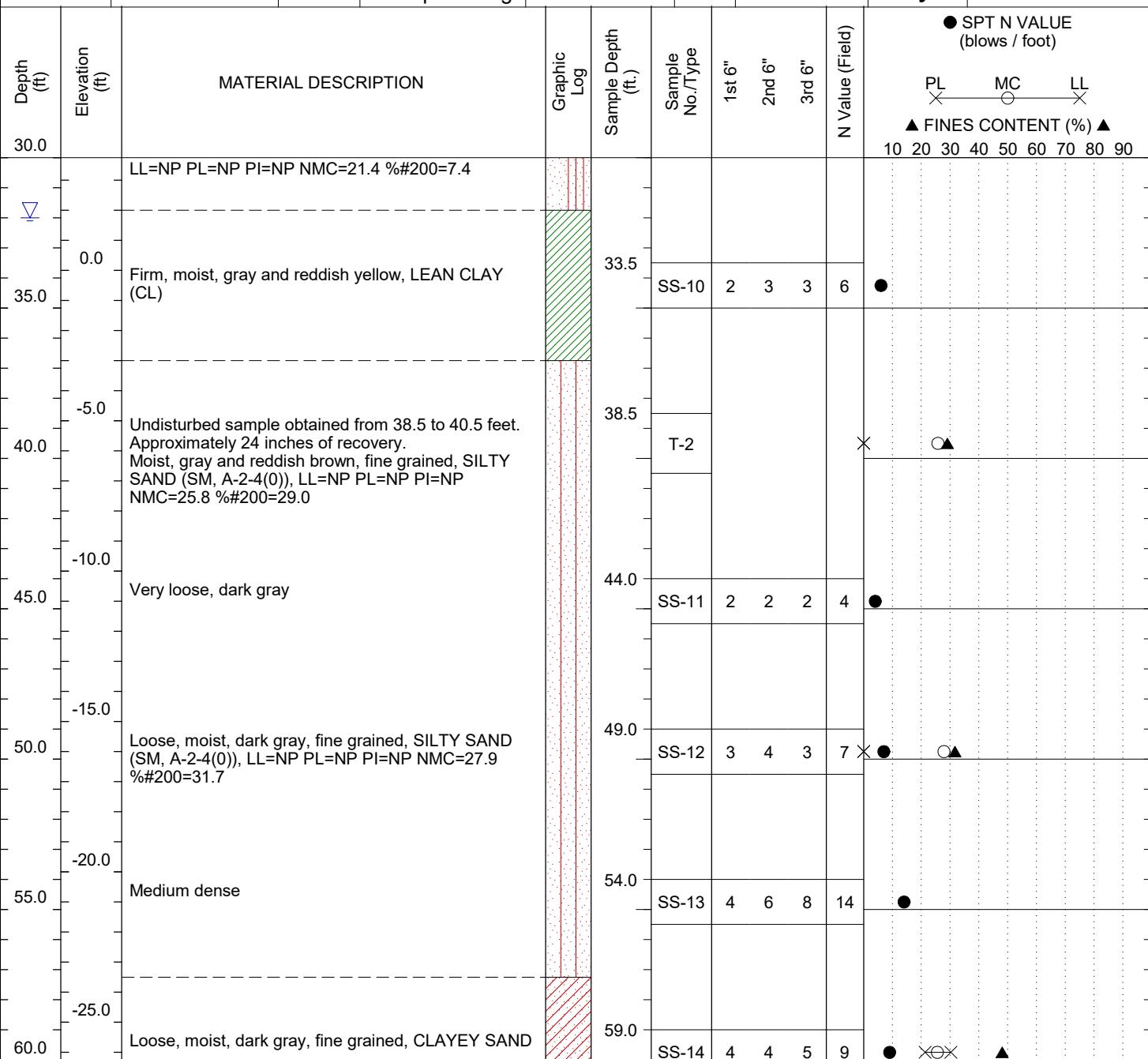
SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-32	Boring Location: 17+55.7		Offset: RT 76.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 33.8 ft.	Northing: 238455.26	Easting: 1839035.38	Date Started: 5/23/2018			
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.	Date Completed: 5/24/2018			
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic	Energy Ratio: 94%			
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	32.0 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-32	Boring Location: 17+55.7		Offset: RT 76.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 33.8 ft.	Northing: 238455.26	Easting: 1839035.38		Date Started: 5/23/2018		
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 5/24/2018		
Bore Hole Diameter (in): 4-inch			AASHTO / ASTM Sampling Methods: AASHTO T206 & T207			
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic		Energy Ratio: 94%		
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	32.0 ft.	
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION			Graphic Log	Sample Depth (ft.)
60.0		(SC, A-4(2)), LL=30 PL=21 PI=9 NMC=25.6 %#200=48.1				Sample No./Type
-30.0		Loose				1st 6"
65.0		Loose				2nd 6"
-35.0		Loose				3rd 6"
70.0		Loose				N Value (Field)
-40.0		Loose				● SPT N VALUE (blows / foot)
75.0						PL MC LL
-45.0		Medium dense, moist, dark gray, fine grained, SILTY SAND (SM, A-4(0)), LL=NP PL=NP PI=NP NMC=24.1 %#200=43.1				▲ FINES CONTENT (%) ▲
80.0						10 20 30 40 50 60 70 80 90
-50.0		Medium dense, moist, bluish green, fine grained, SILTY SAND (SM, A-2-4(0)), LL=NP PL=NP PI=NP NMC=22.8 %#200=34.5				
85.0						
-55.0		Medium dense, gray				
90.0						

### LEGEND

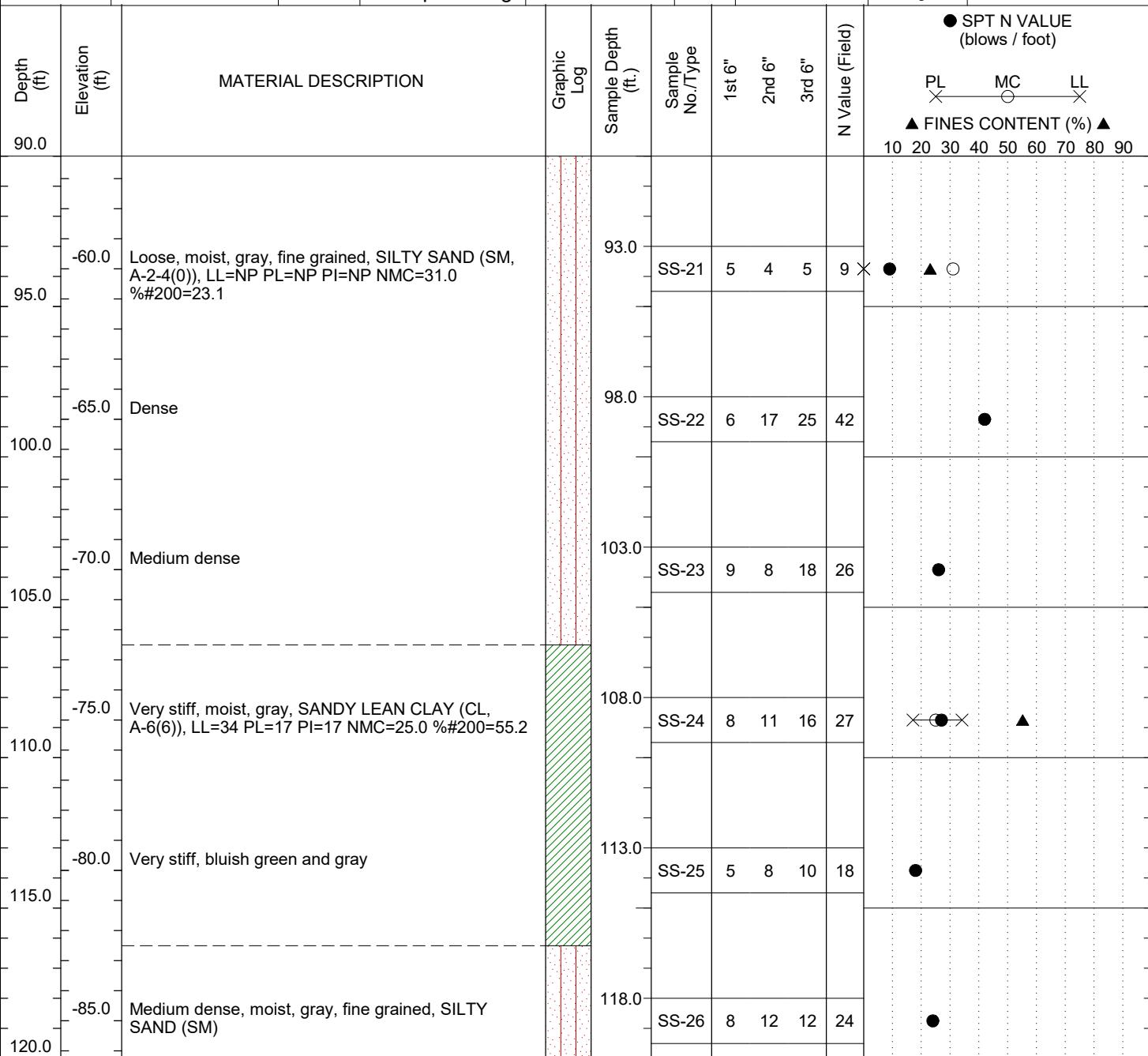
SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-32	Boring Location: 17+55.7		Offset: RT 76.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 33.8 ft.	Northing: 238455.26	Easting: 1839035.38		Date Started:	5/23/2018	
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed:	5/24/2018	
Bore Hole Diameter (in): 4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207		
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic		Energy Ratio:	94%	
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	32.0 ft.	



### LEGEND

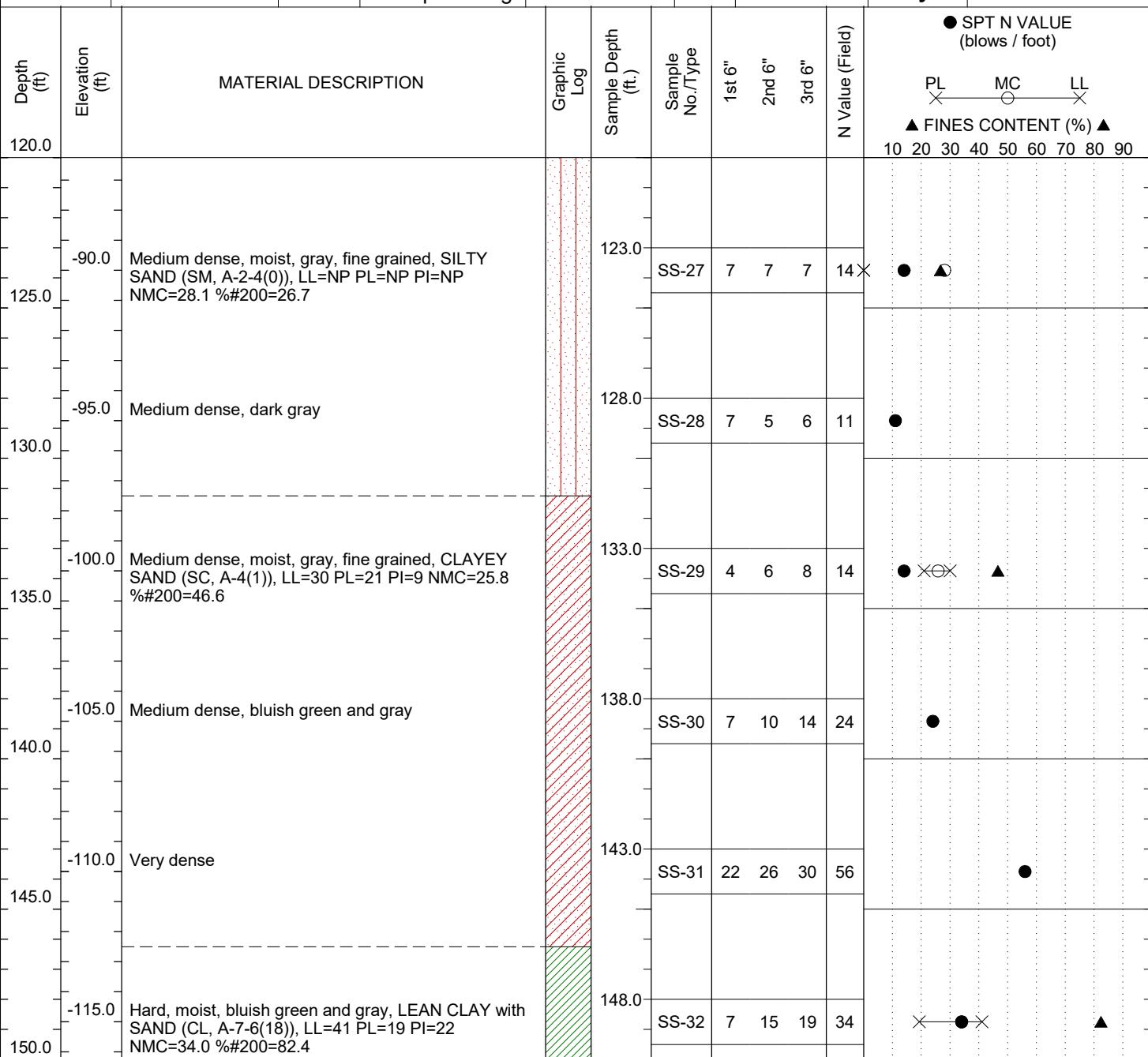
SAMPLER TYPE			DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings		HSA - Hollow Stem Augers	MR - Mud Rotary Wash		
T - Shelby Tube	GB - Grab Bag		SSA - Solid Stem Augers	RC - Rock Coring		
DCP - Dynamic Cone Penetrometer	NQ - Rock Core		HA - Hand Auger			



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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway						County: Mobile
Boring No.: TH-32	Boring Location: 17+55.7		Offset: RT 76.7	Alignment: US-98		
ALDOT PE No.: DPI-0030(005)	TE Project No.: 15-1101-0228		Eng./Geo.: P.McKissick			
Elev.: 33.8 ft.	Northing: 238455.26	Easting: 1839035.38		Date Started: 5/23/2018		
Total Depth: 150.0 ft.	Soil Depth: 150.0 ft.	Core Depth: 0.0 ft.		Date Completed: 5/24/2018		
Bore Hole Diameter (in): 4-inch		AASHTO / ASTM Sampling Methods: AASHTO T206 & T207				
Drill Machine: D-50	Drill Method: MR	Hammer Type: Automatic		Energy Ratio: 94%		
Core Size: N/A	Driller: Thompson Eng	Groundwater: TOB	N.O.	Delayed:	32.0 ft.	



### LEGEND

SAMPLER TYPE				DRILLING METHOD			
SS - Split Spoon	AC - Auger Cuttings	HSA - Hollow Stem Augers	MR - Mud Rotary Wash				
T - Shelby Tube	GB - Grab Bag	SSA - Solid Stem Augers	RC - Rock Coring				
DCP - Dynamic Cone Penetrometer	NQ - Rock Core	HA - Hand Auger					



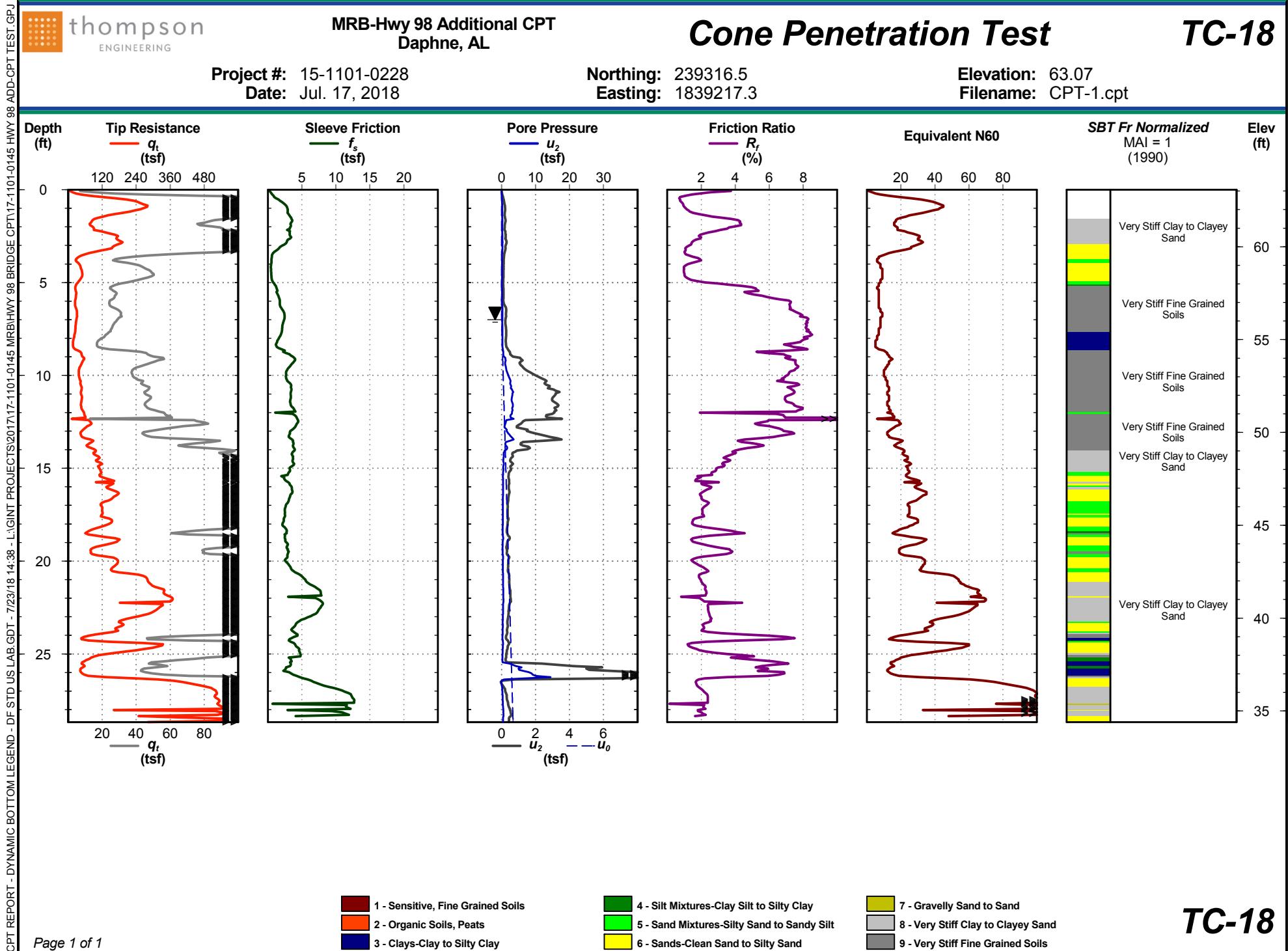
**thompson**  
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## RECORD OF TEST BORING

Site Description: I-10 Mobile River Bridge and Bayway								County:	Mobile				
Boring No.:	TH-32	Boring Location:	17+55.7	Offset:	RT 76.7	Alignment:	US-98						
ALDOT PE No.:	DPI-0030(005)		TE Project No.:	15-1101-0228			Eng./Geo.:	P.McKissick					
Elev.:	33.8 ft.	Northing:	238455.26	Easting:	1839035.38	Date Started:	5/23/2018						
Total Depth:	150.0 ft.	Soil Depth:	150.0 ft.	Core Depth:	0.0 ft.	Date Completed:	5/24/2018						
Bore Hole Diameter (in):	4-inch	AASHTO / ASTM Sampling Methods:			AASHTO T206 & T207								
Drill Machine:	D-50	Drill Method:	MR	Hammer Type:	Automatic		Energy Ratio:	94%					
Core Size:	N/A	Driller:	Thompson Eng	Groundwater:	TOB	N.O.	Delayed:	32.0 ft.					
Depth (ft)	Elevation (ft)	MATERIAL DESCRIPTION				Graphic Log	Sample Depth (ft.)	Sample No./Type	1st 6"	2nd 6"	3rd 6"	N Value (Field)	● SPT N VALUE (blows / foot)
		Boring Terminated at 150.0 feet.											PL MC LL
													▲ FINES CONTENT (%) ▲
													10 20 30 40 50 60 70 80 90

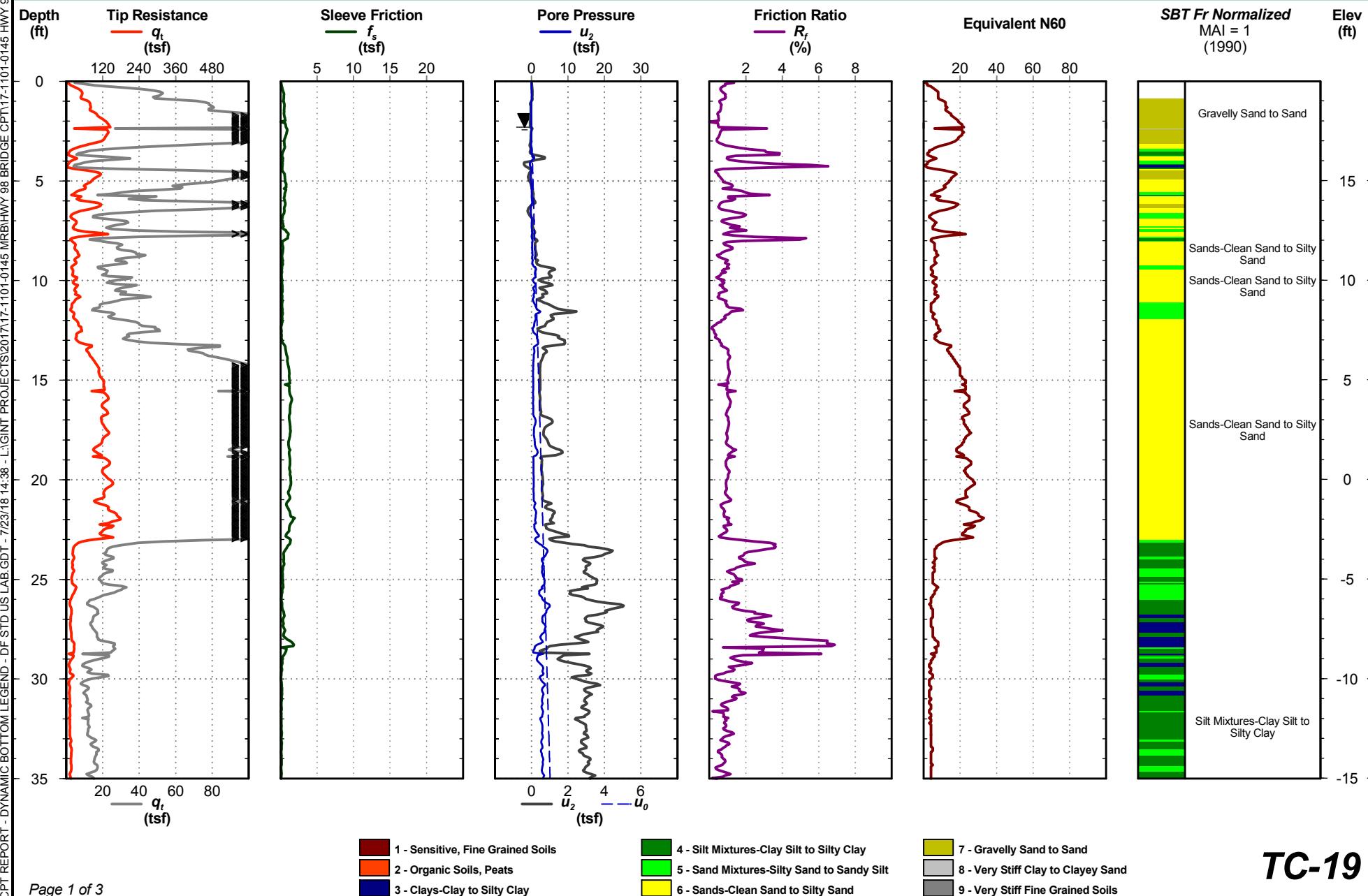
### LEGEND

SAMPLER TYPE	DRILLING METHOD
SS - Split Spoon	AC - Auger Cuttings
T - Shelby Tube	GB - Grab Bag
DCP - Dynamic Cone Penetrometer	NQ - Rock Core
	HSA - Hollow Stem Augers
	SSA - Solid Stem Augers
	HA - Hand Auger
	MR - Mud Rotary Wash
	RC - Rock Coring



Project #: 15-1101-0228  
Date: Jul. 17, 2018

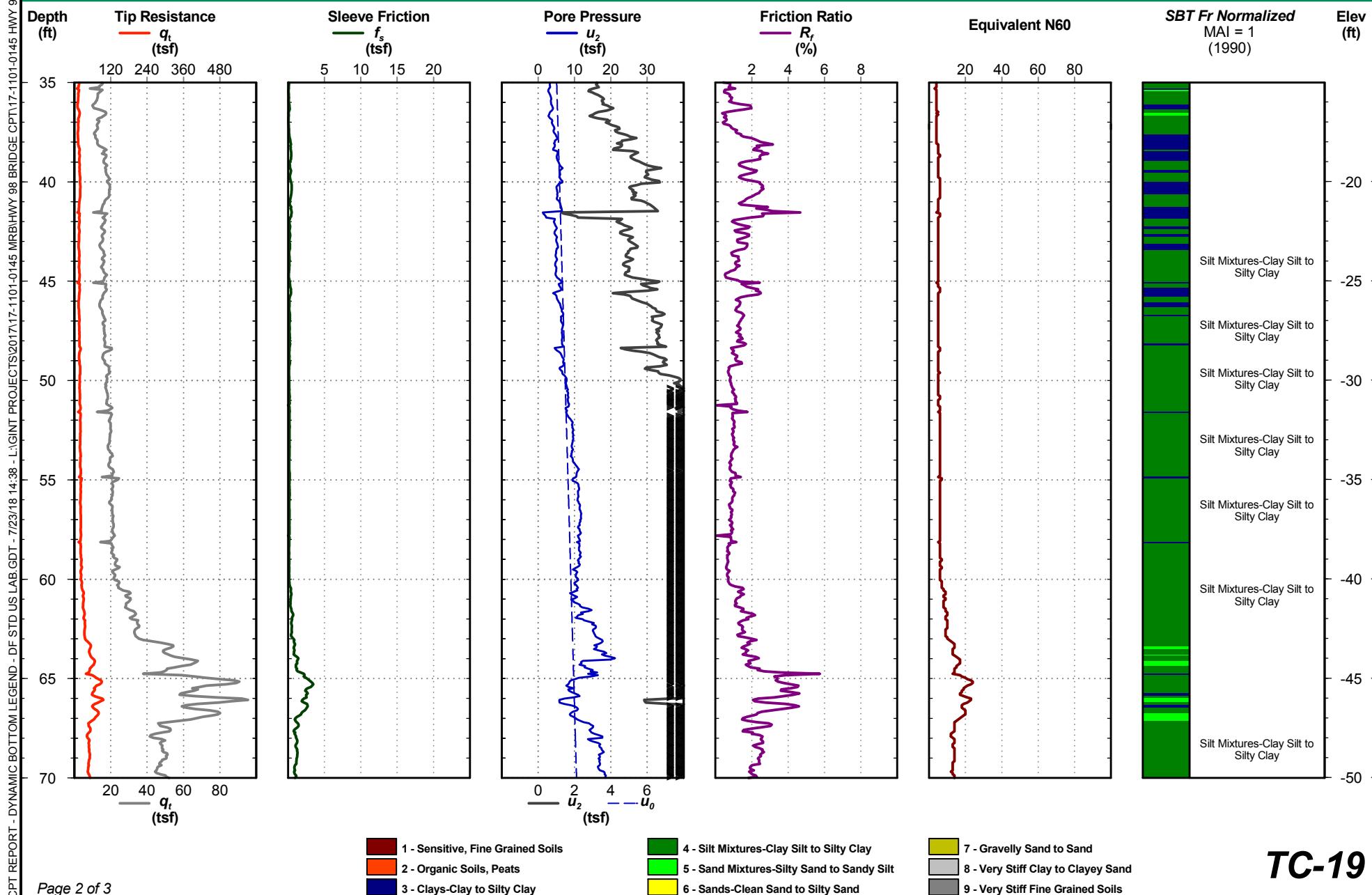
Northing: 238818.6  
Easting: 1839027.3

Elevation: 19.98  
Filename: CPT-2.cpt


Project #: 15-1101-0228  
Date: Jul. 17, 2018

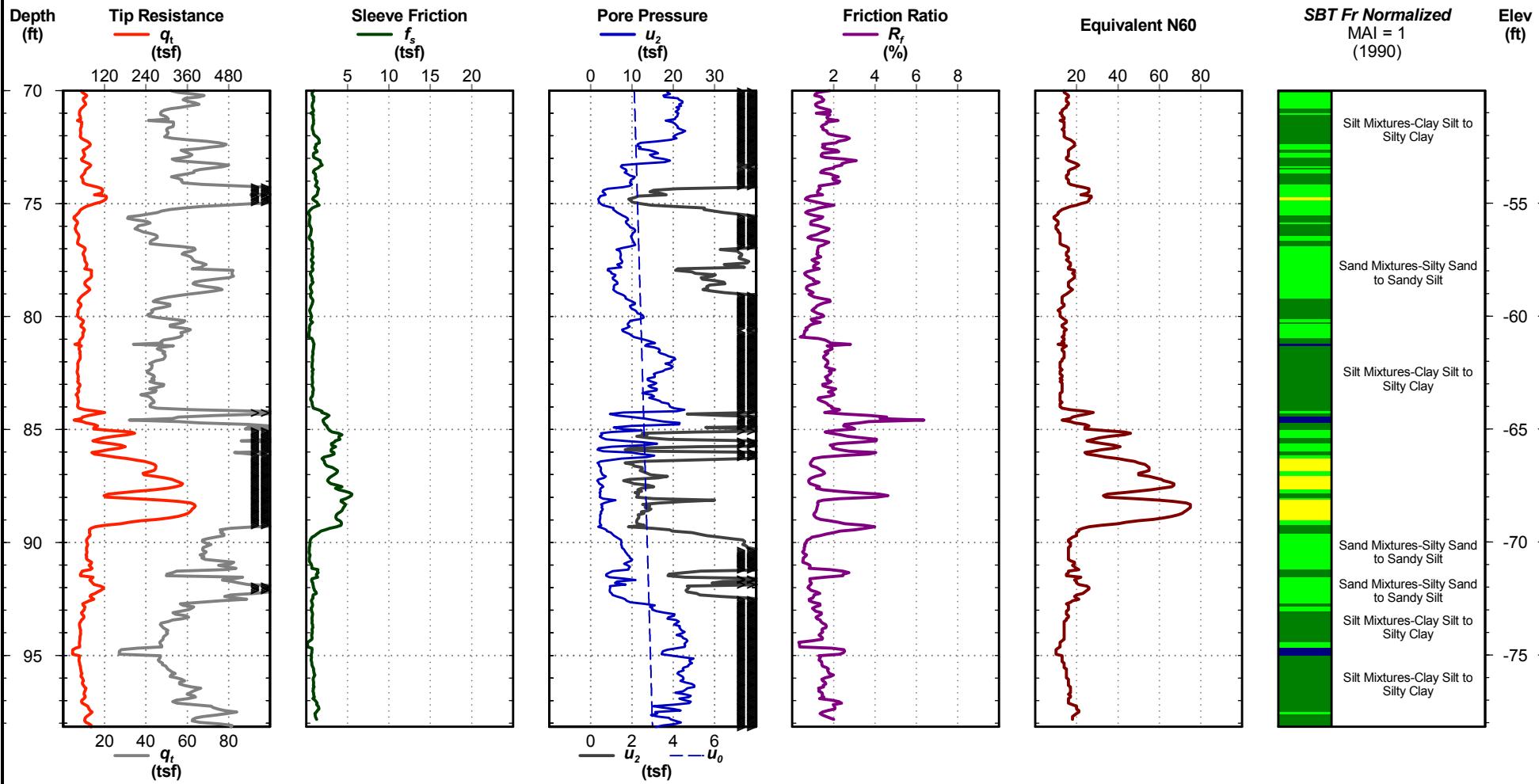
## Cone Penetration Test

TC-19

Northing: 238818.6  
Easting: 1839027.3Elevation: 19.98  
Filename: CPT-2.cpt

**Project #:** 15-1101-0228  
**Date:** Jul. 17, 2018

**Northing:** 238818.6  
**Easting:** 1839027.3

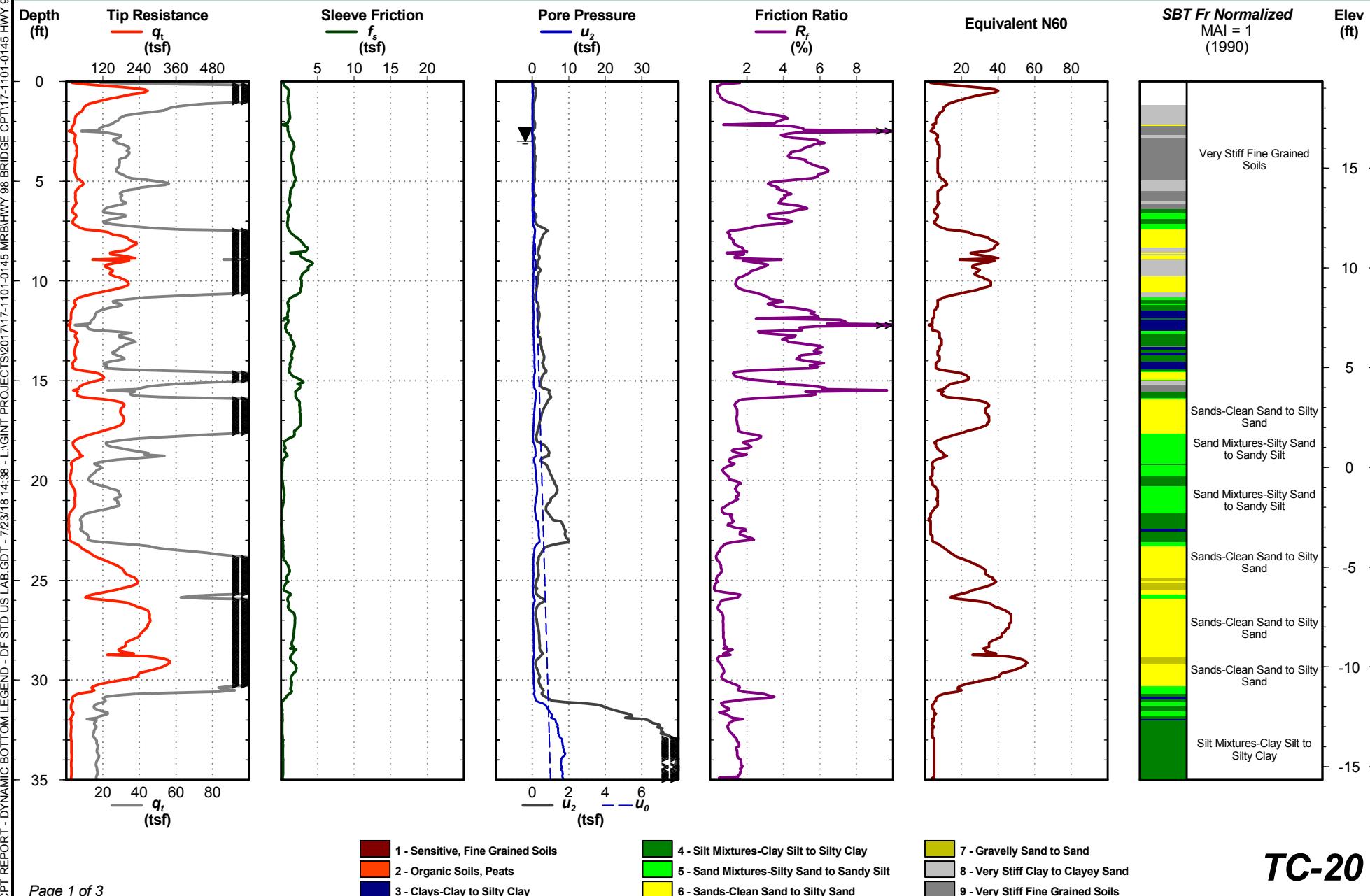
**Elevation:** 19.98  
**Filename:** CPT-2.cpt

1 - Sensitive, Fine Grained Soils  
2 - Organic Soils, Peats  
3 - Clays-Clay to Silty Clay

4 - Silt Mixtures-Clay Silt to Silty Clay  
5 - Sand Mixtures-Silty Sand to Sandy Silt  
6 - Sands-Clean Sand to Silty Sand

7 - Gravelly Sand to Sand  
8 - Very Stiff Clay to Clayey Sand  
9 - Very Stiff Fine Grained Soils

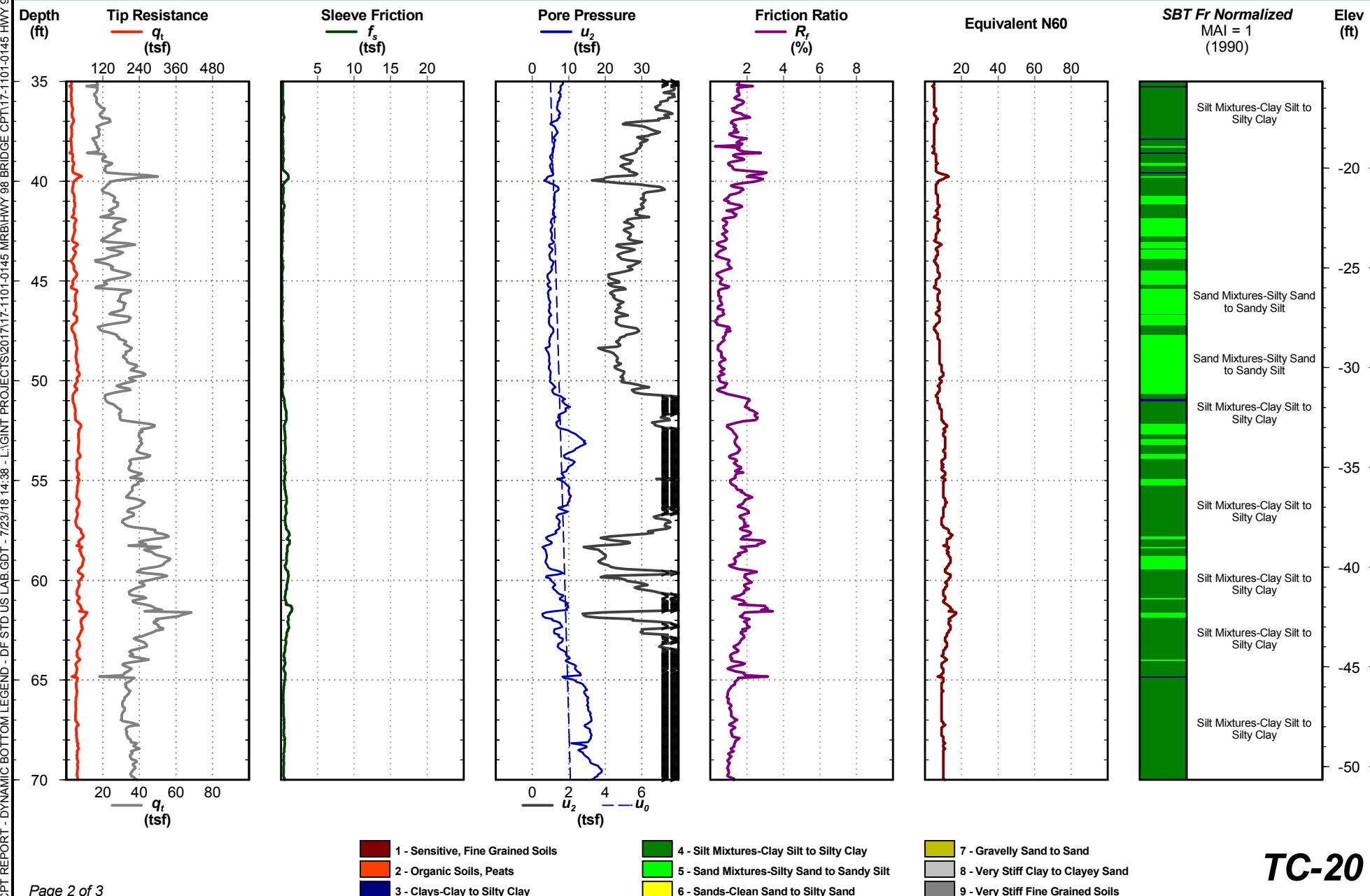
Project #: 15-1101-0228  
Date: Jul. 16, 2018

Northing: 238640.5  
Easting: 1838999.5

Elevation: 19.34  
Filename: CPT-3.cpt


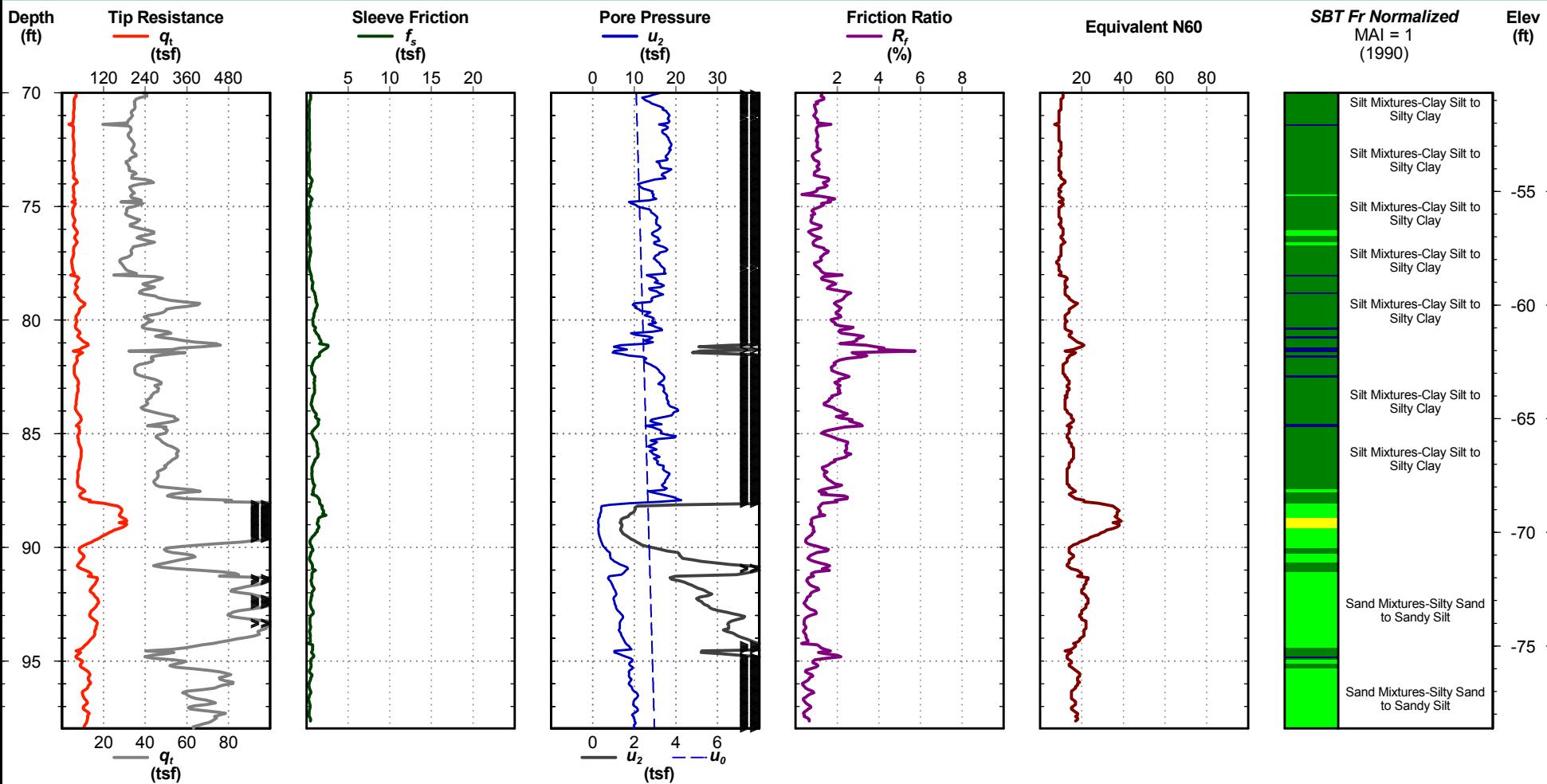
**Project #:** 15-1101-0228  
**Date:** Jul. 16, 2018

**Northing:** 238640.5  
**Easting:** 1838999.5

**Elevation:** 19.34  
**Filename:** CPT-3.cpt


**Project #:** 15-1101-0228  
**Date:** Jul. 16, 2018

**Northing:** 238640.5  
**Easting:** 1838999.5

**Elevation:** 19.34  
**Filename:** CPT-3.cpt

 1 - Sensitive, Fine Grained Soils  
 2 - Organic Soils, Peats  
 3 - Clays-Clay to Silty Clay

 4 - Silt Mixtures-Clay Silt to Silty Clay  
 5 - Sand Mixtures-Silty Sand to Sandy Silt  
 6 - Sands-Clean Sand to Silty Sand

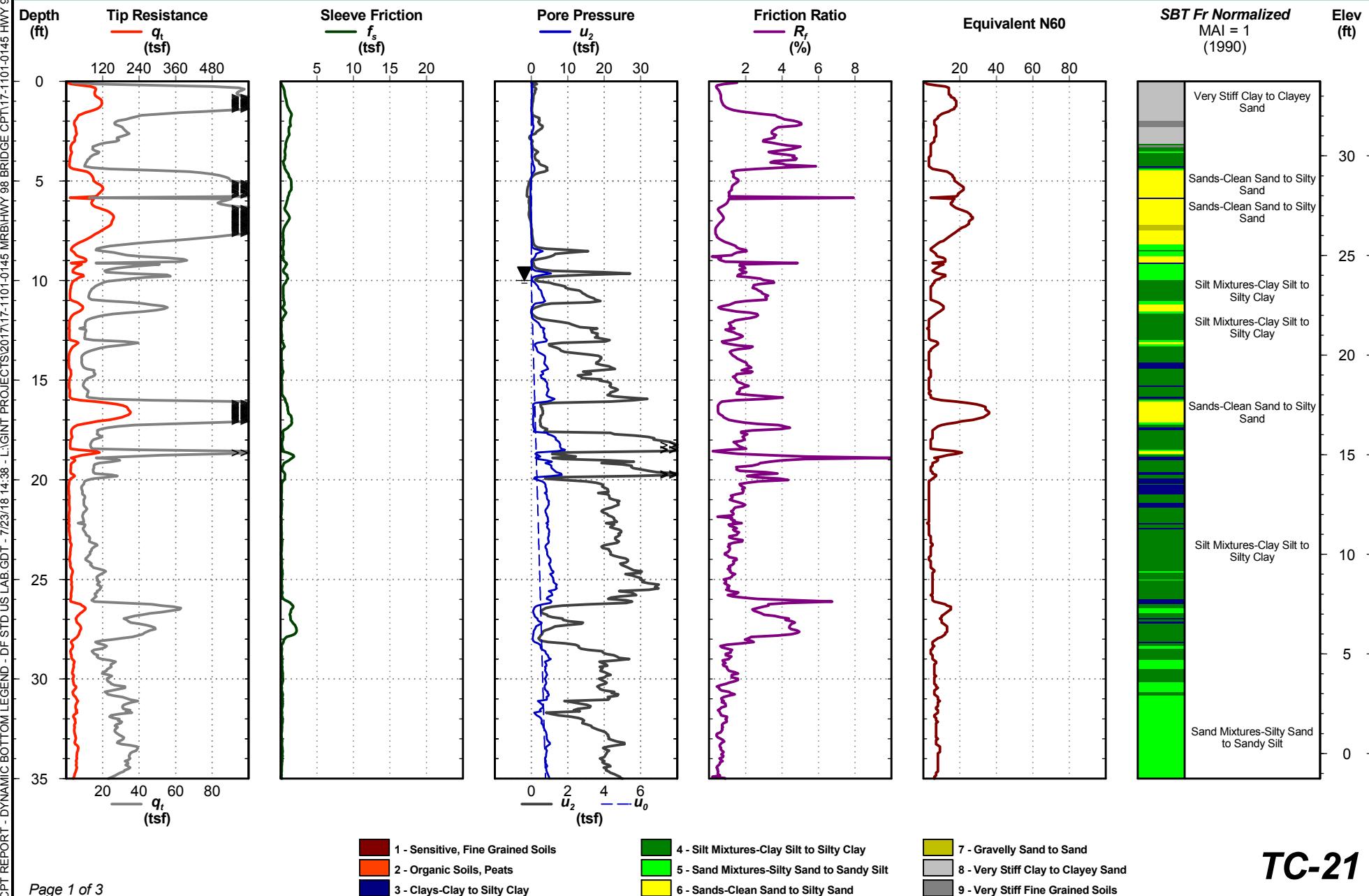
 7 - Gravelly Sand to Sand  
 8 - Very Stiff Clay to Clayey Sand  
 9 - Very Stiff Fine Grained Soils

# Cone Penetration Test

**TC-21**

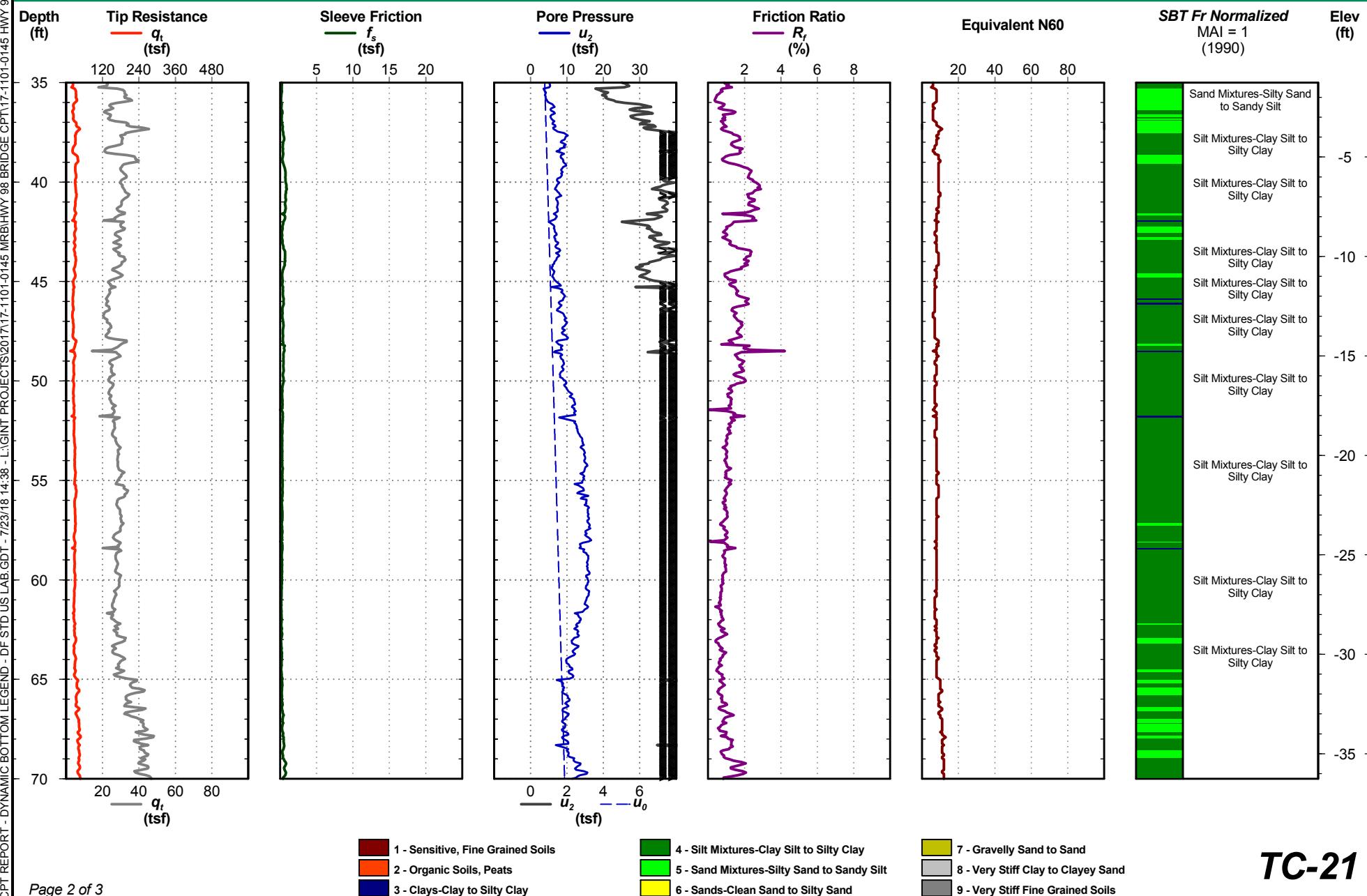
Project #: 15-1101-0228  
Date: Jul. 16, 2018

Northing: 238452.2  
Easting: 1839032.4

Elevation: 33.74  
Filename: CPT-4.cpt


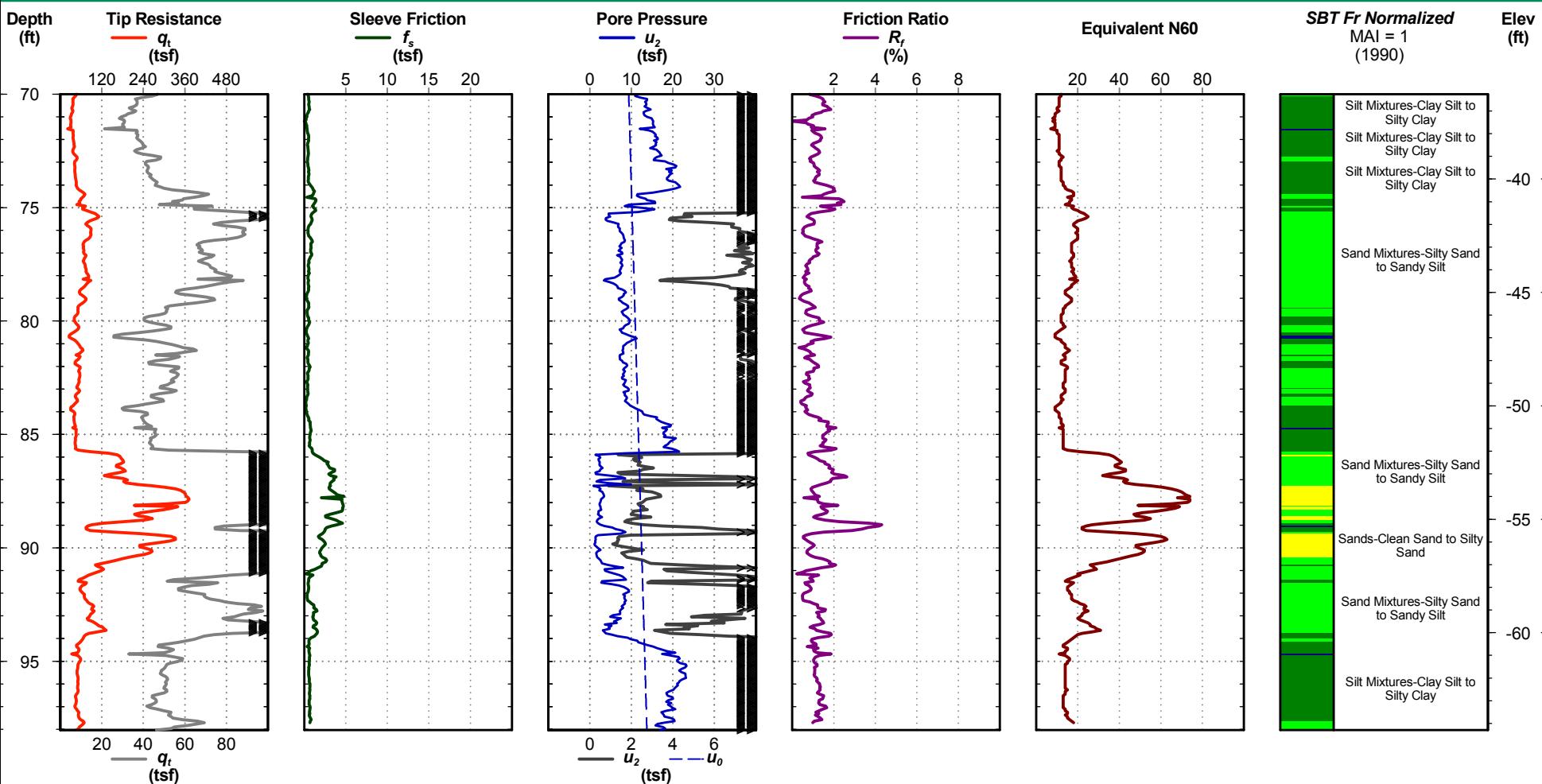
Project #: 15-1101-0228  
Date: Jul. 16, 2018

Northing: 238452.2  
Easting: 1839032.4

Elevation: 33.74  
Filename: CPT-4.cpt


**Project #:** 15-1101-0228  
**Date:** Jul. 16, 2018

**Northing:** 238452.2  
**Easting:** 1839032.4

**Elevation:** 33.74  
**Filename:** CPT-4.cpt

 1 - Sensitive, Fine Grained Soils  
 2 - Organic Soils, Peats  
 3 - Clays-Clay to Silty Clay

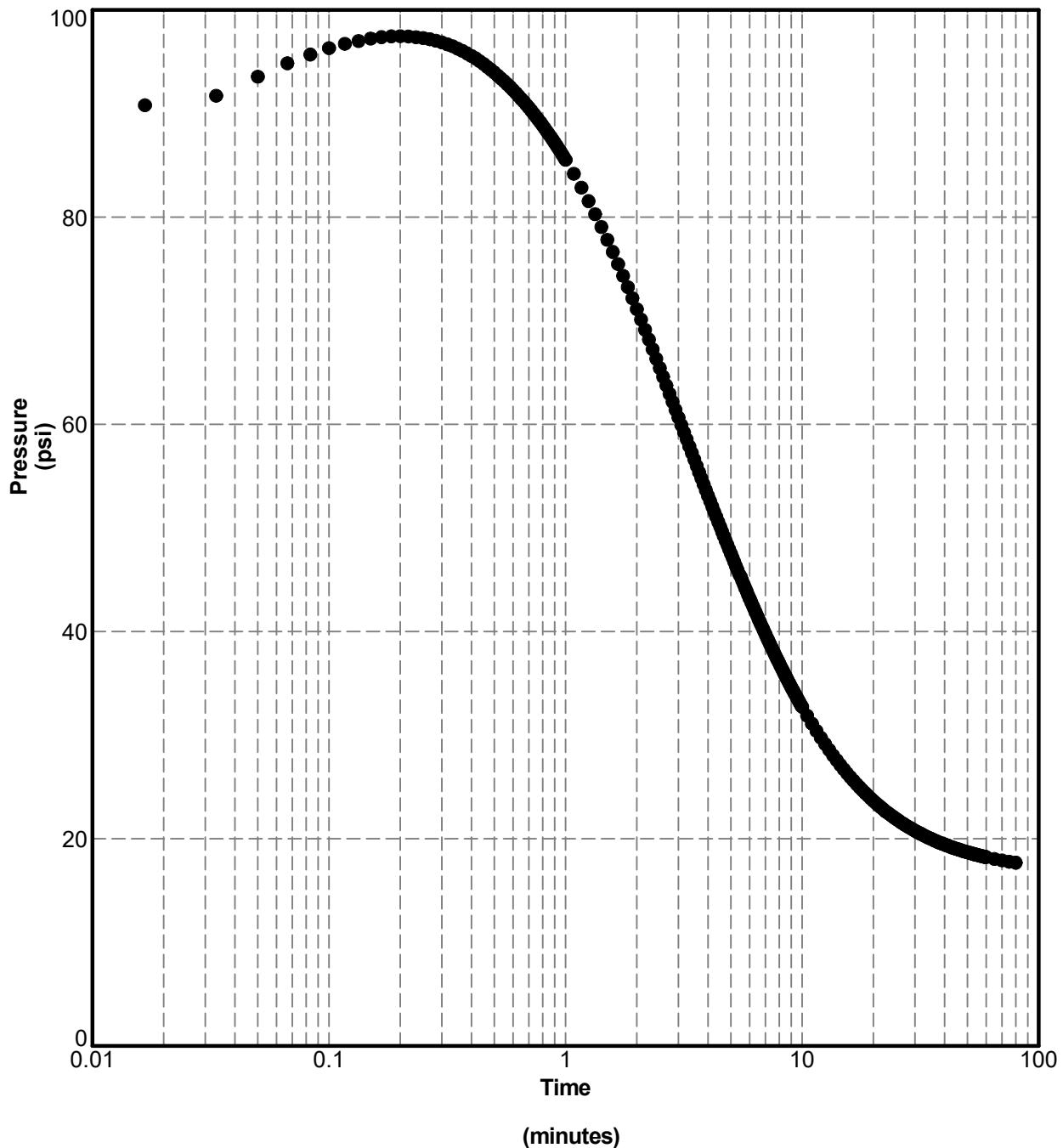
 4 - Silt Mixtures-Clay Silt to Silty Clay  
 5 - Sand Mixtures-Silty Sand to Sandy Silt  
 6 - Sands-Clean Sand to Silty Sand

 7 - Gravelly Sand to Sand  
 8 - Very Stiff Clay to Clayey Sand  
 9 - Very Stiff Fine Grained Soils
**TC-21**

Date: Jul. 17, 2018  
Estimated Water Depth: 2.3 ft  
Rig/Operator: Chris Rea

Northing: 238818.6  
Easting: 1839027.3  
Elevation: 20.0

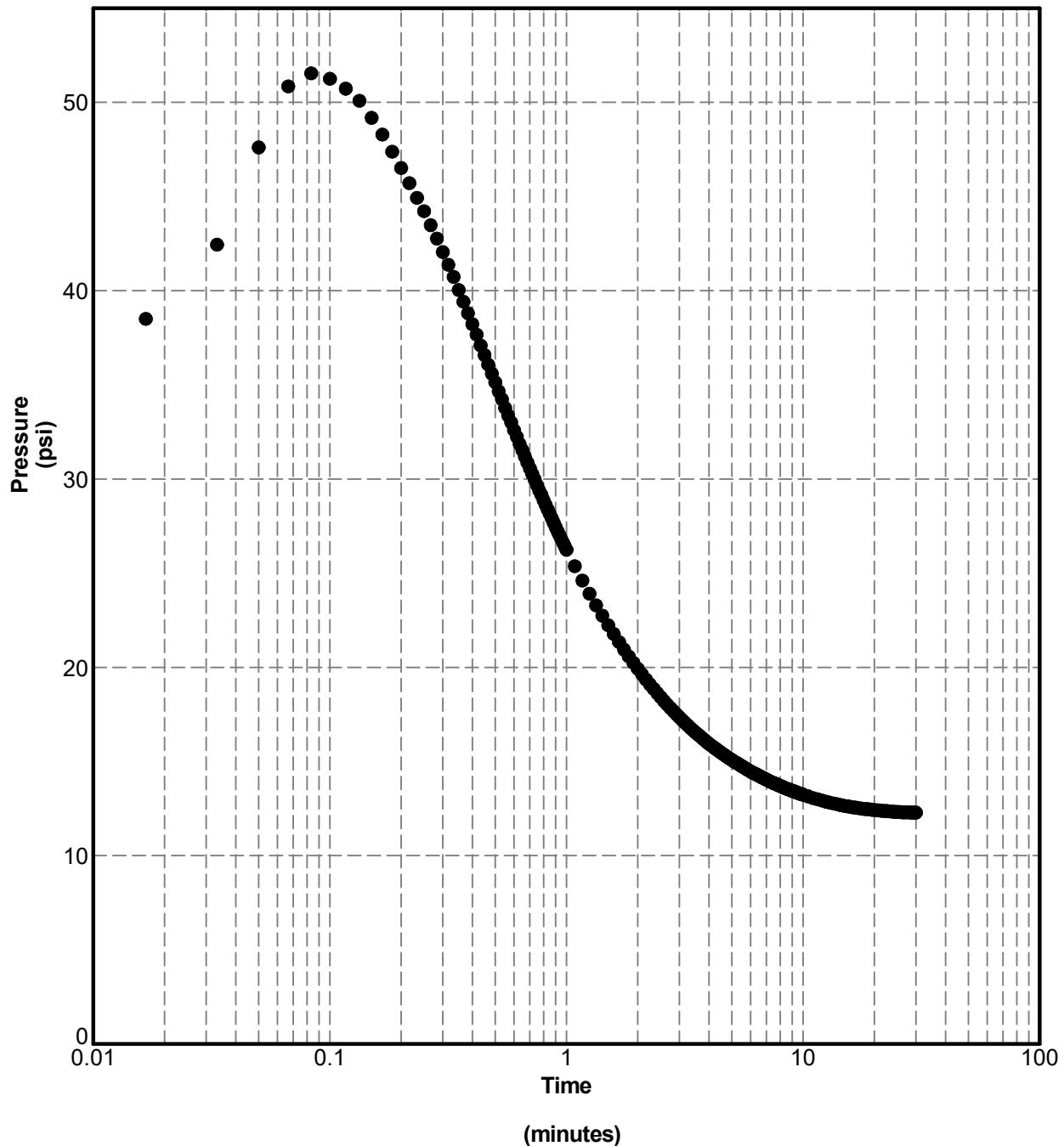
Total Depth: 98.2 ft  
Termination Criteria:  
Test Depth: 41.5 ft



Date: Jul. 16, 2018  
Estimated Water Depth: 10 ft  
Rig/Operator: Chris Rea

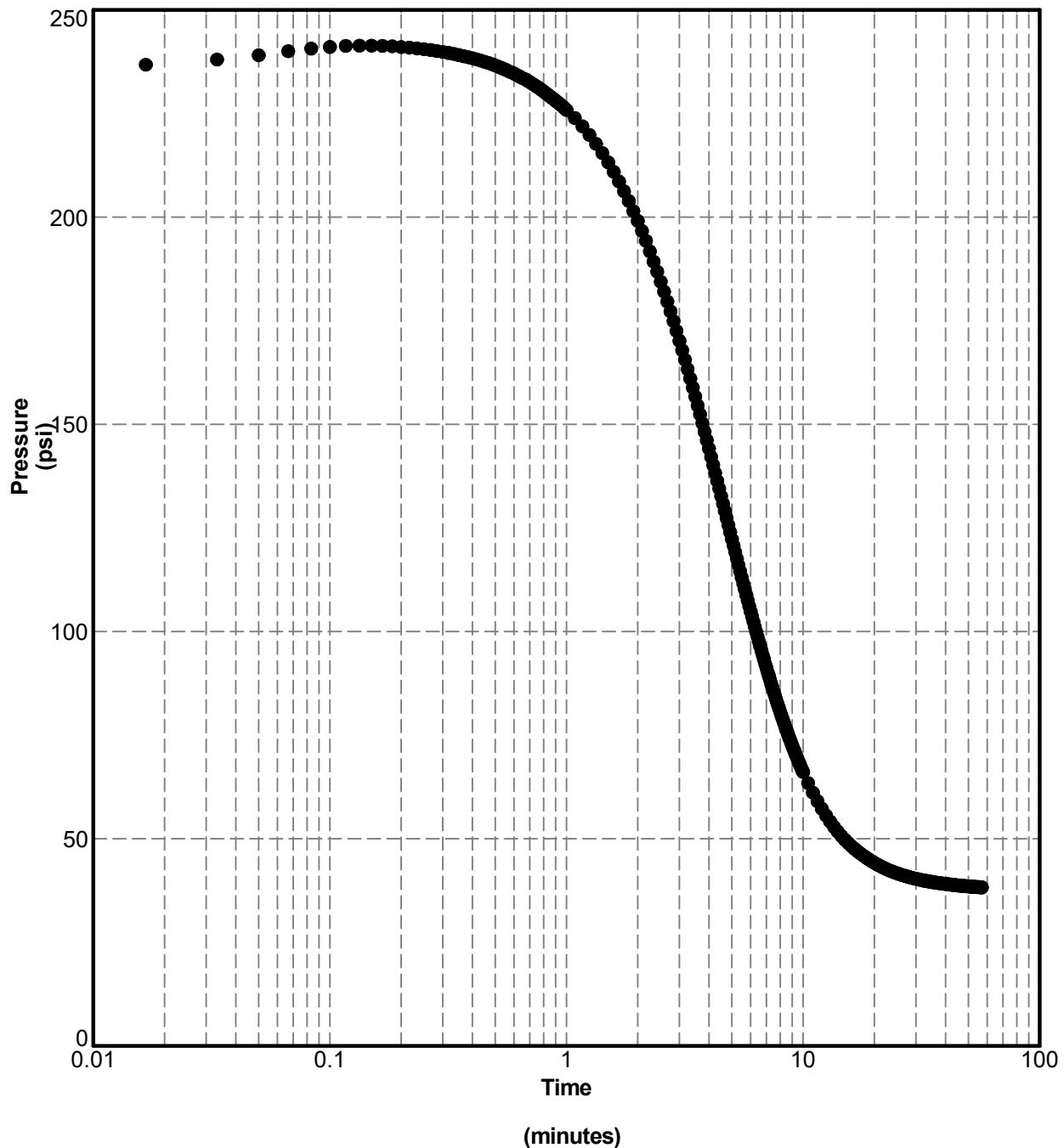
Northing: 238452.2  
Easting: 1839032.4  
Elevation: 33.7

Total Depth: 98.0 ft  
Termination Criteria:  
Test Depth: 31.6 ft



Date: Jul. 16, 2018 Northing: 238452.2  
Estimated Water Depth: 10 ft Easting: 1839032.4  
Rig/Operator: Chris Rea Elevation: 33.7

Total Depth: 98.0 ft  
Termination Criteria:  
Test Depth: 98.0 ft



# KEY TO SYMBOLS



Thompson Engineering, Inc

PROJECT NAME I-10 Mobile River Bridge and Bayway

CLIENT ALDOT

ALDOT PROJECT NO: DPI-0030(005)

TE PROJECT NO: 15-1101-0228

PROJECT LOCATION Baldwin, Baldwin

## LITHOLOGIC SYMBOLS



ASPHALT: Asphalt



AUGER



CH: USCS High Plasticity Clay



CL: USCS Low Plasticity Clay



CL-ML: USCS Low Plasticity Silty Clay



CONCRETE: Concrete



GM: USCS Silty Gravel



GP: USCS Poorly-graded Gravel



GP-GM: USCS Poorly-graded Gravel with Silt



GW: USCS Well-graded Gravel



MH: USCS Elastic Silt



ML: USCS Silt



SC: USCS Clayey Sand



SC-SM: USCS Clayey Sand



SM: USCS Silty Sand



SP: USCS Poorly-graded Sand

## SAMPLER TYPE

SS - Split Spoon

T - Shelby Tube

DCP - Dynamic Cone Penetrometer

AC - Auger Cuttings

GB - Grab Bag

NQ - Rock Core

## GROUNDWATER LEGEND

▽ Delayed Groundwater Level

▼ Groundwater Level at TOB (Time of Boring). Water levels at the time of boring may have not been obtained due to mud rotary drilling techniques.

N.E. - Not Encountered

N.O. - Not Obtained

## ABBREVIATIONS

LL	- LIQUID LIMIT (%)
PL	- PLASTIC LIMIT (%)
PI	- PLASTIC INDEX (%)
NMC	- MOISTURE CONTENT (%)
DD	- DRY DENSITY (PCF)
NP	- NON PLASTIC

%#200	- PERCENT PASSING NO. 200 SIEVE
PP	- POCKET PENETROMETER (TSF)
TV	- TORVANE
UC	- UNCONFINED COMPRESSION

## **APPENDIX C**

- **Laboratory Summary**
- **BMT-5's**
- **Consolidated Undrained (C.U.) Triaxial Shear Tests**
- **Unconsolidated Undrained (U.U.) Triaxial Shear Test Results**
- **Direct Shear Test Results**
- **One Dimensional Consolidation Tests**

Station & Offset	Boring No.	Sample ID	Depth (ft)	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	% Pass 200 % Silt      % Clay	D50 (mm)	USCS	AASHTO
26+47.0 RT 98.9	TH-28	SS-1	0.0	12.2	NP	NP	NP	0.0	77.7	22.3	0.2002	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-2	1.5	17.9	35	13	22	0.0	45.0	55.0		CL	A-6(8)
26+47.0 RT 98.9	TH-28	SS-3	3.0	23.5	22	12	10	2.3	61.6	36.1	0.1612	SC	A-4(0)
26+47.0 RT 98.9	TH-28	SS-4	4.5	38.0	36	13	23	3.2	51.4	45.4	0.0971	SC	A-6(6)
26+47.0 RT 98.9	TH-28	T-1	8.0	21.1	44	20	24	4.5	41.4	22.7      31.4	0.0523	CL	A-7-6(10)
26+47.0 RT 98.9	TH-28	SS-7	18.5	24.2	NP	NP	NP	0.2	69.8	30.0	0.1001	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-10	33.5	25.4	NP	NP	NP	0.0	88.9	11.1	0.1654	SP-SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-12	43.5	22.6	NP	NP	NP	0.0	87.4	12.6	0.2412	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-13	48.5	24.4	NP	NP	NP	0.0	68.3	31.7	0.0978	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-15	58.5	35.2	NP	NP	NP	0.0	70.2	29.8	0.1146	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-18	73.5	26.8	NP	NP	NP	0.0	93.1	6.9	0.2238	SP-SM	A-3(0)
26+47.0 RT 98.9	TH-28	SS-20	83.5	26.2	26	18	8	0.0	56.4	43.6	0.0817	SC	A-4(1)
26+47.0 RT 98.9	TH-28	SS-23	98.5	22.1	28	17	11	0.0	51.2	48.8	0.0768	SC	A-6(2)
26+47.0 RT 98.9	TH-28	SS-27	118.5	25.4	35	21	14	0.0	19.8	80.2		CL	A-6(10)
26+47.0 RT 98.9	TH-28	SS-28	123.5	28.1	NP	NP	NP	0.0	64.8	35.2	0.1005	SM	A-2-4(0)
26+47.0 RT 98.9	TH-28	SS-30	133.5	23.6	35	18	17	0.0	35.9	64.1		CL	A-6(9)
26+47.0 RT 98.9	TH-28	SS-32	143.5	25.6	NP	NP	NP	0.0	53.9	46.1	0.0803	SM	A-4(0)
21+12.1 RT 4.5	TH-29	SS-2	1.5	13.5	21	12	9	0.0	74.4	25.6	0.2121	SC	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-3	3.0	28.6	55	17	38	1.9	16.3	81.8		CH	A-7-6(32)
21+12.1 RT 4.5	TH-29	SS-4	4.5	45.9	37	13	24	28.6	34.9	36.5	0.2182	SC	A-6(3)
21+12.1 RT 4.5	TH-29	T-1	8.5	37.8	44	16	28	1.9	10.3	51.1      36.7	0.0197	CL	A-7-6(25)
21+12.1 RT 4.5	TH-29	SS-7	18.5	26.4	NP	NP	NP	0.0	89.3	10.7	0.1801	SP-SM	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-9	28.5	27.6	25	18	7	0.0	66.8	33.2	0.0951	SC-SM	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-11	38.5	28.4	43	16	27	0.0	29.3	70.7		CL	A-7-6(17)
21+12.1 RT 4.5	TH-29	SS-13	48.5	26.5	29	16	13	0.0	56.9	43.1	0.0841	SC	A-6(2)
21+12.1 RT 4.5	TH-29	SS-15	58.5	26.3	32	14	18	0.0	55.5	44.5	0.0837	SC	A-6(4)
21+12.1 RT 4.5	TH-29	SS-17	68.5	23.0	31	16	15	0.0	59.3	40.7	0.0918	SC	A-6(2)
21+12.1 RT 4.5	TH-29	SS-19	78.5	24.9	26	19	7	0.0	70.8	29.2	0.1099	SC-SM	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-21	88.5	32.2	NP	NP	NP	0.0	68.3	31.7	0.1483	SM	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-23	98.5	27.4	32	14	18	0.0	46.0	54.0		CL	A-6(6)

Station & Offset	Boring No.	Sample ID	Depth (ft)	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	% Pass 200 % Silt      % Clay	D50 (mm)	USCS	AASHTO
21+12.1 RT 4.5	TH-29	SS-26	113.5	26.6	25	18	7	0.0	66.9	33.1	0.1061	SC-SM	A-2-4(0)
21+12.1 RT 4.5	TH-29	SS-27	118.5	25.5	26	19	7	0.0	50.4	49.6	0.0755	SC-SM	A-4(1)
21+12.1 RT 4.5	TH-29	SS-30	133.5	24.3	40	21	19	0.0	34.1	65.9		CL	A-6(11)
21+12.1 RT 4.5	TH-29	SS-33	148.5	26.8	NP	NP	NP	0.0	74.7	25.3	0.1060	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-1	0.0	14.2	NP	NP	NP	0.3	70.0	29.7	0.1736	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-2	1.5	10.2	21	11	10	6.2	62.3	31.5	0.1974	SC	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-3	3.0	21.5	26	12	14	0.0	50.4	49.6	0.0767	SC	A-6(3)
19+60.0 LT 132.7	TH-30	SS-4	4.5	27.4	28	13	15	1.8	47.1	51.2		CL	A-6(4)
19+60.0 LT 132.7	TH-30	SS-6	8.5	29.0	46	14	32	0.0	17.2	82.8		CL	A-7-6(26)
19+60.0 LT 132.7	TH-30	T-1	13.5	55.5	57	19	38	0.0	12.3	43.8      43.9	0.0080	CH	A-7-6(36)
19+60.0 LT 132.7	TH-30	SS-7	18.5	19.9	NP	NP	NP	0.0	94.1	5.9	0.2657	SP-SM	A-3(0)
19+60.0 LT 132.7	TH-30	SS-8	23.5	24.9	20	15	5	0.3	82.6	17.1	0.2041	SC-SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-9	28.5	25.7	NP	NP	NP	0.0	71.4	28.6	0.0984	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	T-2	33.5	29.1	25	21	4	0.0	67.0	19.8      13.3	0.0913	SC-SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-10	38.5	26.9	51	17	34	0.0	32.3	67.7		CH	A-7-6(21)
19+60.0 LT 132.7	TH-30	SS-11	43.5	27.4	33	21	12	0.0	46.7	53.3		CL	A-6(4)
19+60.0 LT 132.7	TH-30	SS-12	48.5	27.3	31	20	11	0.0	40.2	59.8		CL	A-6(4)
19+60.0 LT 132.7	TH-30	SS-14	58.5	23.7	30	16	14	0.0	49.1	50.9		CL	A-6(4)
19+60.0 LT 132.7	TH-30	SS-17	73.5	28.8	34	22	12	0.0	42.3	57.7		CL	A-6(5)
19+60.0 LT 132.7	TH-30	SS-18	78.5	31.1	NP	NP	NP	0.0	77.0	23.0	0.1180	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-20	88.5	23.0	NP	NP	NP	0.0	83.3	16.7	0.2132	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-23	103.5	22.9	NP	NP	NP	0.0	57.4	42.6	0.0843	SM	A-4(0)
19+60.0 LT 132.7	TH-30	SS-25	113.5	28.2	NP	NP	NP	0.0	75.4	24.6	0.1179	SM	A-2-4(0)
19+60.0 LT 132.7	TH-30	SS-27	123.5	37.9	27	22	5	0.0	51.5	48.5	0.0796	SM	A-4(0)
19+60.0 LT 132.7	TH-30	SS-29	133.5	29.7	34	23	11	0.0	6.2	93.8		CL	A-6(11)
19+60.0 LT 132.7	TH-30	SS-31	143.5	26.6	35	20	15	0.0	29.7	70.3		CL	A-6(9)
19+26.0 RT 3.0	TH-31	SS-1	0.0	9.5	29	13	16	23.8	50.4	25.9	0.2919	SC	A-2-6(1)
19+26.0 RT 3.0	TH-31	SS-3	3.0	17.6	NP	NP	NP	0.4	84.6	15.0	0.3076	SM	A-2-4(0)
19+26.0 RT 3.0	TH-31	T-1	8.5	26.1	59	17	42	0.0	2.9	42.3      54.8	0.0036	CH	A-7-6(45)
19+26.0 RT 3.0	TH-31	SS-6	13.5	34.7	31	13	18	0.0	10.8	89.2		CL	A-6(14)

#### Soil Classification Summary

Alabama Department of Transportation  
 ALDOT Project No.: DPI-0030(005)  
 Project Name: I-10 Mobile River Bridge and Bayway  
 Location: Mobile, Alabama

Station & Offset	Boring No.	Sample ID	Depth (ft)	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	% Pass 200 % Silt	% Clay	D50 (mm)	USCS	AASHTO
19+26.0 RT 3.0	TH-31	T-2	23.5	35.5	NP	NP	NP	0.0	57.6	28.5	13.8	0.0834	SM	A-4(0)
19+26.0 RT 3.0	TH-31	SS-9	33.5	28.5	NP	NP	NP	0.0	70.3	29.7		0.0940	SM	A-2-4(0)
19+26.0 RT 3.0	TH-31	T-3	38.0	21.6	NP	NP	NP	0.0	50.4	35.6	14.0	0.0755	SM	A-4(0)
19+26.0 RT 3.0	TH-31	SS-11	48.5	27.6	28	19	9	0.0	61.2	38.8		0.0916	SC	A-4(0)
19+26.0 RT 3.0	TH-31	SS-15	68.5	24.6	NP	NP	NP	0.0	59.4	40.6		0.0912	SM	A-4(0)
19+26.0 RT 3.0	TH-31	SS-18	83.5	29.1	32	18	14	0.0	18.1	81.9			CL	A-6(10)
19+26.0 RT 3.0	TH-31	SS-19	88.5	29.9	NP	NP	NP	0.0	83.3	16.7		0.1829	SM	A-2-4(0)
19+26.0 RT 3.0	TH-31	SS-21	98.5	22.5	37	15	22	0.0	26.1	73.9			CL	A-6(14)
19+26.0 RT 3.0	TH-31	SS-23	108.5	23.5	NP	NP	NP	0.0	63.2	36.8		0.0958	SM	A-4(0)
19+26.0 RT 3.0	TH-31	SS-27	128.5	31.0	37	24	13	0.0	10.6	89.4			CL	A-6(12)
19+26.0 RT 3.0	TH-31	SS-30	143.5	26.1	NP	NP	NP	0.0	68.2	31.8		0.0943	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-1	0.0	5.8	25	15	10	0.8	59.2	40.0		0.1201	SC	A-4(1)
17+55.7 RT 76.7	TH-32	SS-3	3.0	24.1	48	14	34	1.3	36.5	62.3			CL	A-7-6(18)
17+55.7 RT 76.7	TH-32	SS-4	4.5	48.6	37	12	25	2.4	31.4	66.2			CL	A-6(13)
17+55.7 RT 76.7	TH-32	SS-5	6.0	21.2	26	15	11	0.1	42.7	57.2			CL	A-6(3)
17+55.7 RT 76.7	TH-32	SS-8	18.5	15.2	NP	NP	NP	0.2	53.9	45.8		0.0934	SM	A-4(0)
17+55.7 RT 76.7	TH-32	T-1	23.0	14.0	NP	NP	NP	0.7	71.9	19.1	8.3	0.2118	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-9	28.5	21.4	NP	NP	NP	0.2	92.4	7.4		0.3393	SP-SM	A-3(0)
17+55.7 RT 76.7	TH-32	T-2	38.5	25.8	NP	NP	NP	0.0	71.0	12.2	16.8	0.0992	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-12	49.0	27.9	NP	NP	NP	0.0	68.3	31.7		0.0935	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-14	59.0	25.6	30	21	9	0.0	51.9	48.1		0.0771	SC	A-4(2)
17+55.7 RT 76.7	TH-32	SS-18	78.0	24.1	NP	NP	NP	0.0	56.9	43.1		0.0886	SM	A-4(0)
17+55.7 RT 76.7	TH-32	SS-19	83.0	22.8	NP	NP	NP	0.0	65.5	34.5		0.1036	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-21	93.0	31.0	NP	NP	NP	0.0	76.9	23.1		0.1123	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-24	108.0	25.0	34	17	17	0.0	44.8	55.2			CL	A-6(6)
17+55.7 RT 76.7	TH-32	SS-27	123.0	28.1	NP	NP	NP	0.0	73.3	26.7		0.1146	SM	A-2-4(0)
17+55.7 RT 76.7	TH-32	SS-29	133.0	25.8	30	21	9	0.0	53.4	46.6		0.0810	SC	A-4(1)
17+55.7 RT 76.7	TH-32	SS-32	148.0	34.0	41	19	22	0.0	17.6	82.4			CL	A-7-6(18)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-28	TH-28	TH-28	TH-28	TH-28	TH-28
Station	26+47.0	26+47.0	26+47.0	26+47.0	26+47.0	26+47.0
Offset	RT 98.9					
Sample ID	SS-1	SS-2	SS-3	SS-4	T-1	SS-7
Depth (ft)	0.0	1.5	3.0	4.5	8.0	18.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	96.8	100.0
#4 SIEVE (4.75mm)	100.0	100.0	97.7	96.8	95.5	99.8
#10 SIEVE (2.00mm)	99.7	99.4	94.8	94.4	91.9	99.7
#20 SIEVE (0.85mm)	98.7	98.5	90.6	91.8	89.0	99.5
#40" SIEVE (425um)	89.4	94.7	80.6	85.5	85.5	99.3
#60 SIEVE (250um)	62.8	81.9	63.3	72.9	77.6	99.0
#100 SIEVE (150um)	33.3	68.6	47.8	57.7	69.5	92.3
#140 SIEVE (106um)	26.2	62.4	41.8	51.6	62.2	54.0
#200 SIEVE (75um)	22.3	55.0	36.1	45.4	54.1	30.0

Clay					31.4	
Silt					22.7	
Total Sand	77.7	45.0	61.6	51.4	41.4	69.8
Total Gravel	0.0	0.0	2.3	3.2	4.5	0.2

**ATTERBERG LIMITS**

Liquid Limit	NP	35	22	36	44	NP
Plastic Limit	NP	13	12	13	20	NP
Plasticity Index	NP	22	10	23	24	NP

USCS	SM	CL	SC	SC	CL	SM
AASHTO	A-2-4(0)	A-6(8)	A-4(0)	A-6(6)	A-7-6(10)	A-2-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-28	TH-28	TH-28	TH-28	TH-28	TH-28
Station	26+47.0	26+47.0	26+47.0	26+47.0	26+47.0	26+47.0
Offset	RT 98.9					
Sample ID	SS-10	SS-12	SS-13	SS-15	SS-18	SS-20
Depth (ft)	33.5	43.5	48.5	58.5	73.5	83.5
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	99.7	100.0	99.2	100.0	100.0
#20 SIEVE (0.85mm)	99.9	97.9	100.0	97.1	99.9	100.0
#40" SIEVE (425um)	97.5	85.0	99.8	94.9	99.4	99.9
#60 SIEVE (250um)	85.4	52.2	94.2	91.9	60.7	99.2
#100 SIEVE (150um)	41.6	20.6	83.6	68.6	11.4	91.6
#140 SIEVE (106um)	18.1	15.6	55.6	44.6	8.1	69.4
#200 SIEVE (75um)	11.1	12.6	31.7	29.8	6.9	43.6

Clay						
Silt						
Total Sand	88.9	87.4	68.3	70.2	93.1	56.4
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

ATTERBERG LIMITS						
Liquid Limit	NP	NP	NP	NP	NP	26
Plastic Limit	NP	NP	NP	NP	NP	18
Plasticity Index	NP	NP	NP	NP	NP	8
USCS	SP-SM	SM	SM	SM	SP-SM	SC
AASHTO	A-2-4(0)	A-2-4(0)	A-2-4(0)	A-2-4(0)	A-3(0)	A-4(1)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-28	TH-28	TH-28	TH-28	TH-28	TH-29
Station	26+47.0	26+47.0	26+47.0	26+47.0	26+47.0	21+12.1
Offset	RT 98.9	RT 4.5				
Sample ID	SS-23	SS-27	SS-28	SS-30	SS-32	SS-2
Depth (ft)	98.5	118.5	123.5	133.5	143.5	1.5
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	100.0	100.0	100.0	100.0	99.8
#20 SIEVE (0.85mm)	99.9	100.0	99.5	99.3	99.9	98.2
#40" SIEVE (425um)	99.7	99.8	98.7	98.2	98.9	84.6
#60 SIEVE (250um)	98.3	99.3	95.3	96.2	95.3	57.0
#100 SIEVE (150um)	86.3	96.5	75.4	88.6	82.4	35.1
#140 SIEVE (106um)	65.6	90.9	52.7	78.7	66.0	28.9
#200 SIEVE (75um)	48.8	80.2	35.2	64.1	46.1	25.6

Clay						
Silt						
Total Sand	51.2	19.8	64.8	35.9	53.9	74.4
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

ATTERBERG LIMITS						
Liquid Limit	28	35	NP	35	NP	21
Plastic Limit	17	21	NP	18	NP	12
Plasticity Index	11	14	NP	17	NP	9

USCS	SC	CL	SM	CL	SM	SC
AASHTO	A-6(2)	A-6(10)	A-2-4(0)	A-6(9)	A-4(0)	A-2-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-29	TH-29	TH-29	TH-29	TH-29	TH-29
Station	21+12.1	21+12.1	21+12.1	21+12.1	21+12.1	21+12.1
Offset	RT 4.5					
Sample ID	SS-3	SS-4	T-1	SS-7	SS-9	SS-11
Depth (ft)	3.0	4.5	8.5	18.5	28.5	38.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	92.3	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	84.1	98.5	100.0	100.0	100.0
#4 SIEVE (4.75mm)	98.1	71.4	98.1	100.0	100.0	100.0
#10 SIEVE (2.00mm)	97.3	68.8	97.7	99.9	99.6	100.0
#20 SIEVE (0.85mm)	96.7	67.6	96.8	99.8	99.3	100.0
#40" SIEVE (425um)	95.3	62.7	96.3	99.7	99.0	99.9
#60 SIEVE (250um)	91.8	52.5	95.9	94.2	95.8	99.2
#100 SIEVE (150um)	88.4	43.0	95.2	25.4	83.0	95.2
#140 SIEVE (106um)	86.6	39.6	94.5	14.6	57.7	85.9
#200 SIEVE (75um)	81.8	36.5	87.8	10.7	33.2	70.7

Clay		36.7				
Silt		51.1				
Total Sand	16.3	34.9	10.3	89.3	66.8	29.3
Total Gravel	1.9	28.6	1.9	0.0	0.0	0.0

**ATTERBERG LIMITS**

Liquid Limit	55	37	44	NP	25	43
Plastic Limit	17	13	16	NP	18	16
Plasticity Index	38	24	28	NP	7	27

USCS	CH	SC	CL	SP-SM	SC-SM	CL
AASHTO	A-7-6(32)	A-6(3)	A-7-6(25)	A-2-4(0)	A-2-4(0)	A-7-6(17)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-29	TH-29	TH-29	TH-29	TH-29	TH-29
Station	21+12.1	21+12.1	21+12.1	21+12.1	21+12.1	21+12.1
Offset	RT 4.5					
Sample ID	SS-13	SS-15	SS-17	SS-19	SS-21	SS-23
Depth (ft)	48.5	58.5	68.5	78.5	88.5	98.5
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	100.0	100.0	100.0	100.0	100.0
#20 SIEVE (0.85mm)	100.0	100.0	100.0	100.0	99.9	99.8
#40" SIEVE (425um)	99.9	99.9	99.9	99.8	92.4	98.8
#60 SIEVE (250um)	98.6	98.2	98.2	97.3	76.4	96.1
#100 SIEVE (150um)	87.5	85.6	82.9	79.4	50.4	86.6
#140 SIEVE (106um)	63.9	61.8	56.6	46.6	36.9	72.2
#200 SIEVE (75um)	43.1	44.5	40.7	29.2	31.7	54.0

Clay						
Silt						
Total Sand	56.9	55.5	59.3	70.8	68.3	46.0
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

ATTERBERG LIMITS						
Liquid Limit	29	32	31	26	NP	32
Plastic Limit	16	14	16	19	NP	14
Plasticity Index	13	18	15	7	NP	18
USCS	SC	SC	SC	SC-SM	SM	CL
AASHTO	A-6(2)	A-6(4)	A-6(2)	A-2-4(0)	A-2-4(0)	A-6(6)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-29	TH-29	TH-29	TH-29	TH-30	TH-30
Station	21+12.1	21+12.1	21+12.1	21+12.1	19+60.0	19+60.0
Offset	RT 4.5	RT 4.5	RT 4.5	RT 4.5	LT 132.7	LT 132.7
Sample ID	SS-26	SS-27	SS-30	SS-33	SS-1	SS-2
Depth (ft)	113.5	118.5	133.5	148.5	0.0	1.5
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	95.3
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	95.3
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	99.7	93.8
#10 SIEVE (2.00mm)	100.0	100.0	100.0	100.0	98.4	92.1
#20 SIEVE (0.85mm)	99.9	100.0	99.7	99.9	96.6	89.4
#40" SIEVE (425um)	98.7	98.0	95.5	99.3	87.1	76.6
#60 SIEVE (250um)	94.4	94.6	94.1	98.7	65.4	57.0
#100 SIEVE (150um)	73.7	83.7	90.7	86.9	43.8	41.9
#140 SIEVE (106um)	49.9	67.0	74.9	50.0	35.2	36.0
#200 SIEVE (75um)	33.1	49.6	65.9	25.3	29.7	31.5

Clay						
Silt						
Total Sand	66.9	50.4	34.1	74.7	70.0	62.3
Total Gravel	0.0	0.0	0.0	0.0	0.3	6.2

ATTERBERG LIMITS						
Liquid Limit	25	26	40	NP	NP	21
Plastic Limit	18	19	21	NP	NP	11
Plasticity Index	7	7	19	NP	NP	10

USCS	SC-SM	SC-SM	CL	SM	SM	SC
AASHTO	A-2-4(0)	A-4(1)	A-6(11)	A-2-4(0)	A-2-4(0)	A-2-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-30	TH-30	TH-30	TH-30	TH-30	TH-30
Station	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0
Offset	LT 132.7					
Sample ID	SS-3	SS-4	SS-6	T-1	SS-7	SS-8
Depth (ft)	3.0	4.5	8.5	13.5	18.5	23.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	98.2	100.0	100.0	100.0	99.7
#10 SIEVE (2.00mm)	99.2	96.3	100.0	100.0	99.7	99.2
#20 SIEVE (0.85mm)	97.5	94.4	100.0	99.3	97.8	97.1
#40" SIEVE (425um)	89.9	87.0	99.9	97.4	75.9	84.8
#60 SIEVE (250um)	75.5	73.4	99.6	95.1	46.6	64.4
#100 SIEVE (150um)	62.0	62.0	98.0	93.3	14.8	28.1
#140 SIEVE (106um)	55.4	56.5	93.0	91.4	7.9	20.4
#200 SIEVE (75um)	49.6	51.2	82.8	87.7	5.9	17.1

Clay				43.9		
Silt				43.8		
Total Sand	50.4	47.1	17.2	12.3	94.1	82.6
Total Gravel	0.0	1.8	0.0	0.0	0.0	0.3

**ATTERBERG LIMITS**

Liquid Limit	26	28	46	57	NP	20
Plastic Limit	12	13	14	19	NP	15
Plasticity Index	14	15	32	38	NP	5

USCS	SC	CL	CL	CH	SP-SM	SC-SM
AASHTO	A-6(3)	A-6(4)	A-7-6(26)	A-7-6(36)	A-3(0)	A-2-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-30	TH-30	TH-30	TH-30	TH-30	TH-30
Station	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0
Offset	LT 132.7					
Sample ID	SS-9	T-2	SS-10	SS-11	SS-12	SS-14
Depth (ft)	28.5	33.5	38.5	43.5	48.5	58.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	100.0	100.0	99.9	100.0	99.9
#20 SIEVE (0.85mm)	100.0	100.0	99.9	99.8	100.0	99.6
#40" SIEVE (425um)	99.9	99.7	99.8	99.5	100.0	99.2
#60 SIEVE (250um)	98.4	98.6	99.2	98.7	99.2	97.4
#100 SIEVE (150um)	85.0	86.8	94.3	92.6	92.3	85.7
#140 SIEVE (106um)	55.9	62.9	83.1	73.9	76.6	64.8
#200 SIEVE (75um)	28.6	33.0	67.7	53.3	59.8	50.9

Clay	13.3					
Silt	19.8					
Total Sand	71.4	67.0	32.3	46.7	40.2	49.1
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

**ATTERBERG LIMITS**

Liquid Limit	NP	25	51	33	31	30
Plastic Limit	NP	21	17	21	20	16
Plasticity Index	NP	4	34	12	11	14

USCS	SM	SC-SM	CH	CL	CL	CL
AASHTO	A-2-4(0)	A-2-4(0)	A-7-6(21)	A-6(4)	A-6(4)	A-6(4)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-30	TH-30	TH-30	TH-30	TH-30	TH-30
Station	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0	19+60.0
Offset	LT 132.7					
Sample ID	SS-17	SS-18	SS-20	SS-23	SS-25	SS-27
Depth (ft)	73.5	78.5	88.5	103.5	113.5	123.5
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	99.9	99.9	100.0	100.0	100.0
#20 SIEVE (0.85mm)	99.3	99.8	99.8	99.9	99.8	97.0
#40" SIEVE (425um)	92.2	99.1	94.3	99.3	98.2	83.0
#60 SIEVE (250um)	88.6	94.5	61.3	96.4	92.8	78.1
#100 SIEVE (150um)	80.2	73.7	25.0	83.6	68.9	68.5
#140 SIEVE (106um)	67.5	39.4	19.0	64.4	41.7	57.0
#200 SIEVE (75um)	57.7	23.0	16.7	42.6	24.6	48.5

Clay						
Silt						
Total Sand	42.3	77.0	83.3	57.4	75.4	51.5
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

ATTERBERG LIMITS						
Liquid Limit	34	NP	NP	NP	NP	27
Plastic Limit	22	NP	NP	NP	NP	22
Plasticity Index	12	NP	NP	NP	NP	5
USCS	CL	SM	SM	SM	SM	SM
AASHTO	A-6(5)	A-2-4(0)	A-2-4(0)	A-4(0)	A-2-4(0)	A-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-30	TH-30	TH-31	TH-31	TH-31	TH-31
Station	19+60.0	19+60.0	19+26.0	19+26.0	19+26.0	19+26.0
Offset	LT 132.7	LT 132.7	RT 3.0	RT 3.0	RT 3.0	RT 3.0
Sample ID	SS-29	SS-31	SS-1	SS-3	T-1	SS-6
Depth (ft)	133.5	143.5	0.0	3.0	8.5	13.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	83.8	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	83.8	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	82.7	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	76.2	99.6	100.0	100.0
#10 SIEVE (2.00mm)	99.9	99.9	72.6	99.0	100.0	100.0
#20 SIEVE (0.85mm)	98.8	98.2	68.7	95.7	99.4	99.8
#40" SIEVE (425um)	97.5	97.3	59.1	69.5	99.0	99.7
#60 SIEVE (250um)	96.9	96.7	46.2	37.5	98.7	99.6
#100 SIEVE (150um)	96.3	94.7	34.9	21.6	98.3	98.2
#140 SIEVE (106um)	95.6	87.3	29.9	17.5	97.8	94.3
#200 SIEVE (75um)	93.8	70.3	25.9	15.0	97.1	89.2

Clay					54.8	
Silt					42.3	
Total Sand	6.2	29.7	50.4	84.6	2.9	10.8
Total Gravel	0.0	0.0	23.8	0.4	0.0	0.0

**ATTERBERG LIMITS**

Liquid Limit	34	35	29	NP	59	31
Plastic Limit	23	20	13	NP	17	13
Plasticity Index	11	15	16	NP	42	18

USCS	CL	CL	SC	SM	CH	CL
AASHTO	A-6(11)	A-6(9)	A-2-6(1)	A-2-4(0)	A-7-6(45)	A-6(14)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-31	TH-31	TH-31	TH-31	TH-31	TH-31
Station	19+26.0	19+26.0	19+26.0	19+26.0	19+26.0	19+26.0
Offset	RT 3.0					
Sample ID	T-2	SS-9	T-3	SS-11	SS-15	SS-18
Depth (ft)	23.5	33.5	38.0	48.5	68.5	83.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	100.0	100.0	100.0	100.0	99.9
#20 SIEVE (0.85mm)	99.1	100.0	100.0	99.9	99.8	99.6
#40" SIEVE (425um)	98.4	99.9	99.9	99.3	99.5	98.6
#60 SIEVE (250um)	96.6	98.8	99.3	97.6	97.2	97.7
#100 SIEVE (150um)	87.1	86.5	91.3	85.2	81.8	93.9
#140 SIEVE (106um)	67.3	60.7	72.5	58.1	57.3	88.4
#200 SIEVE (75um)	42.4	29.7	49.6	38.8	40.6	81.9

Clay	13.8		14.0			
Silt	28.5		35.6			
Total Sand	57.6	70.3	50.4	61.2	59.4	18.1
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

**ATTERBERG LIMITS**

Liquid Limit	NP	NP	NP	28	NP	32
Plastic Limit	NP	NP	NP	19	NP	18
Plasticity Index	NP	NP	NP	9	NP	14

USCS	SM	SM	SM	SC	SM	CL
AASHTO	A-4(0)	A-2-4(0)	A-4(0)	A-4(0)	A-4(0)	A-6(10)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-31	TH-31	TH-31	TH-31	TH-31	TH-32
Station	19+26.0	19+26.0	19+26.0	19+26.0	19+26.0	17+55.7
Offset	RT 3.0	RT 76.7				
Sample ID	SS-19	SS-21	SS-23	SS-27	SS-30	SS-1
Depth (ft)	88.5	98.5	108.5	128.5	143.5	0.0
TOTAL PASSING (%)						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	99.2
#10 SIEVE (2.00mm)	94.9	100.0	100.0	100.0	99.9	98.0
#20 SIEVE (0.85mm)	92.9	99.9	99.9	99.9	99.7	96.4
#40" SIEVE (425um)	89.1	98.0	98.1	97.9	98.8	90.5
#60 SIEVE (250um)	72.0	96.4	92.9	96.8	97.8	76.9
#100 SIEVE (150um)	36.0	91.3	75.4	95.4	90.3	57.3
#140 SIEVE (106um)	21.7	84.3	55.5	93.9	59.3	45.9
#200 SIEVE (75um)	16.7	73.9	36.8	89.4	31.8	40.0

Clay						
Silt						
Total Sand	83.3	26.1	63.2	10.6	68.2	59.2
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.8

ATTERBERG LIMITS						
Liquid Limit	NP	37	NP	37	NP	25
Plastic Limit	NP	15	NP	24	NP	15
Plasticity Index	NP	22	NP	13	NP	10
USCS	SM	CL	SM	CL	SM	SC
AASHTO	A-2-4(0)	A-6(14)	A-4(0)	A-6(12)	A-2-4(0)	A-4(1)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-32	TH-32	TH-32	TH-32	TH-32	TH-32
Station	17+55.7	17+55.7	17+55.7	17+55.7	17+55.7	17+55.7
Offset	RT 76.7					
Sample ID	SS-3	SS-4	SS-5	SS-8	T-1	SS-9
Depth (ft)	3.0	4.5	6.0	18.5	23.0	28.5
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	98.7	97.6	99.9	99.8	99.3	99.8
#10 SIEVE (2.00mm)	97.1	96.0	99.2	98.6	99.2	99.4
#20 SIEVE (0.85mm)	94.7	94.3	98.2	97.0	97.2	96.8
#40" SIEVE (425um)	88.9	90.1	94.8	91.9	84.0	69.0
#60 SIEVE (250um)	79.6	83.5	86.1	79.3	56.0	24.3
#100 SIEVE (150um)	72.7	76.6	71.5	60.7	37.5	10.8
#140 SIEVE (106um)	67.5	71.4	64.4	52.4	31.5	8.5
#200 SIEVE (75um)	62.3	66.2	57.2	45.8	27.4	7.4

Clay					8.3	
Silt					19.1	
Total Sand	36.5	31.4	42.7	53.9	71.9	92.4
Total Gravel	1.3	2.4	0.1	0.2	0.7	0.2

**ATTERBERG LIMITS**

Liquid Limit	48	37	26	NP	NP	NP
Plastic Limit	14	12	15	NP	NP	NP
Plasticity Index	34	25	11	NP	NP	NP

USCS	CL	CL	CL	SM	SM	SP-SM
AASHTO	A-7-6(18)	A-6(13)	A-6(3)	A-4(0)	A-2-4(0)	A-3(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-32	TH-32	TH-32	TH-32	TH-32	TH-32
Station	17+55.7	17+55.7	17+55.7	17+55.7	17+55.7	17+55.7
Offset	RT 76.7					
Sample ID	T-2	SS-12	SS-14	SS-18	SS-19	SS-21
Depth (ft)	38.5	49.0	59.0	78.0	83.0	93.0
<b>TOTAL PASSING (%)</b>						
3" SIEVE (75mm)	100.0	100.0	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	99.9	100.0	100.0	100.0	100.0
#20 SIEVE (0.85mm)	100.0	99.8	99.9	100.0	99.9	100.0
#40" SIEVE (425um)	99.9	99.6	99.3	99.3	98.6	99.7
#60 SIEVE (250um)	98.6	98.1	98.4	95.3	95.6	97.1
#100 SIEVE (150um)	84.4	85.9	92.4	78.5	78.2	80.4
#140 SIEVE (106um)	55.0	60.4	71.7	57.4	51.1	43.9
#200 SIEVE (75um)	29.0	31.7	48.1	43.1	34.5	23.1

Clay	16.8					
Silt	12.2					
Total Sand	71.0	68.3	51.9	56.9	65.5	76.9
Total Gravel	0.0	0.0	0.0	0.0	0.0	0.0

**ATTERBERG LIMITS**

Liquid Limit	NP	NP	30	NP	NP	NP
Plastic Limit	NP	NP	21	NP	NP	NP
Plasticity Index	NP	NP	9	NP	NP	NP

USCS	SM	SM	SC	SM	SM	SM
AASHTO	A-2-4(0)	A-2-4(0)	A-4(2)	A-4(0)	A-2-4(0)	A-2-4(0)

**BMT-5**

Client: ALDOT  
 Project: I-10 Mobile River Bridge and Bayway  
 ALDOT Project No.:15-1101-0228

Project No.: 15-1101-0228  
 Region: Southwest Region  
 Date: 07/20/2018

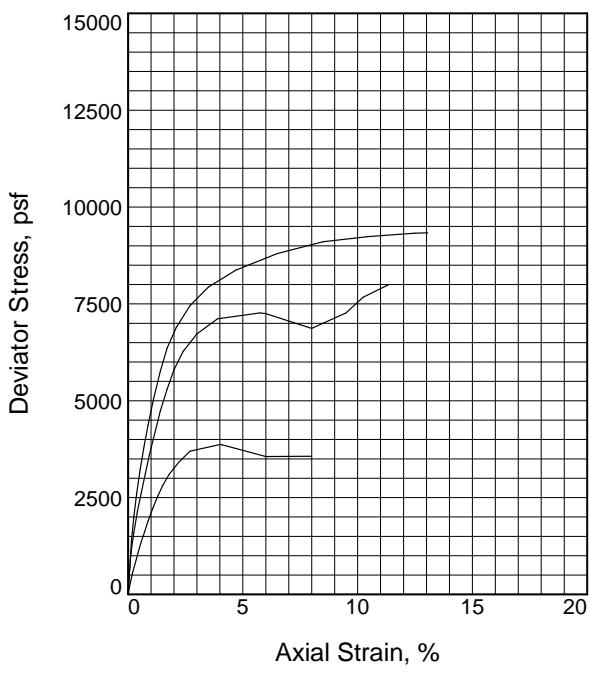
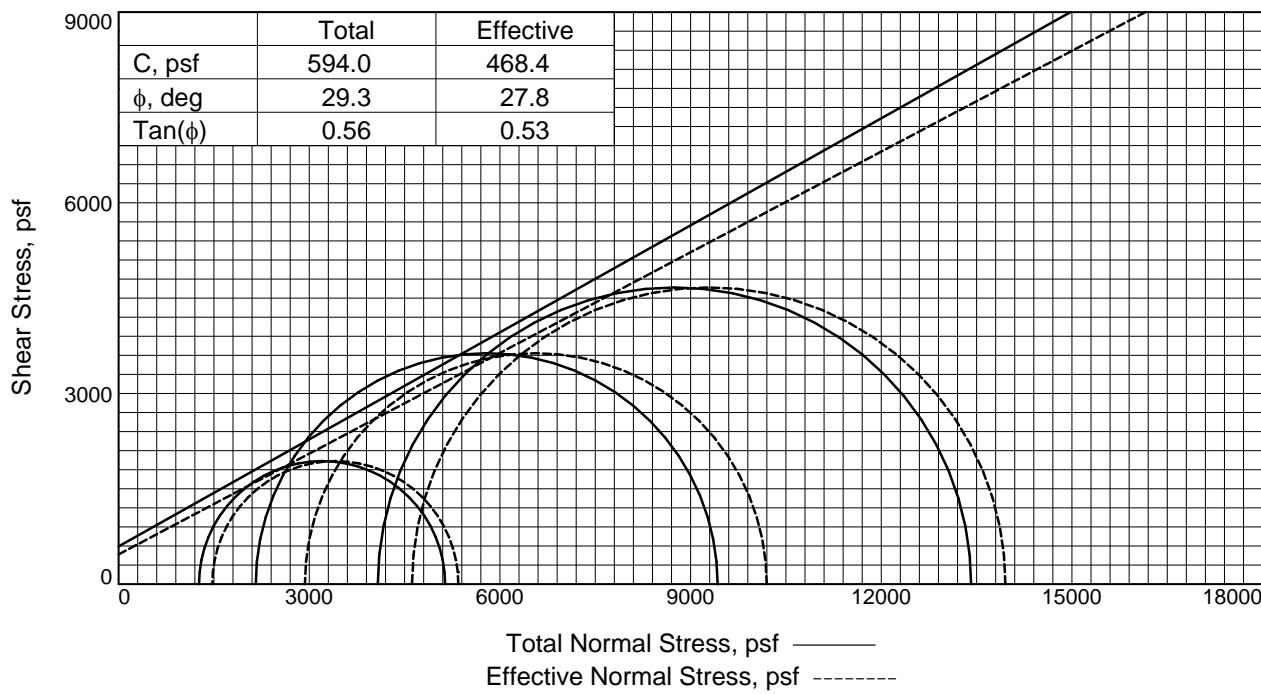
**ALABAMA DEPARTMENT OF TRANSPORTATION**  
**SOILS AND BASE COARSE ANALYSIS**

Boring No.	TH-32	TH-32	TH-32	TH-32
Station	17+55.7	17+55.7	17+55.7	17+55.7
Offset	RT 76.7	RT 76.7	RT 76.7	RT 76.7
Sample ID	SS-24	SS-27	SS-29	SS-32
Depth (ft)	108.0	123.0	133.0	148.0
TOTAL PASSING (%)				
3" SIEVE (75mm)	100.0	100.0	100.0	100.0
2 1/2" SIEVE (63mm)	100.0	100.0	100.0	100.0
2" SIEVE (50mm)	100.0	100.0	100.0	100.0
1 1/2" SIEVE (37.5mm)	100.0	100.0	100.0	100.0
1" SIEVE (25mm)	100.0	100.0	100.0	100.0
3/4" SIEVE (19mm)	100.0	100.0	100.0	100.0
1/2" SIEVE (12.5mm)	100.0	100.0	100.0	100.0
3/8" SIEVE (9.5mm)	100.0	100.0	100.0	100.0
#4 SIEVE (4.75mm)	100.0	100.0	100.0	100.0
#10 SIEVE (2.00mm)	100.0	100.0	100.0	100.0
#20 SIEVE (0.85mm)	99.6	99.9	99.9	100.0
#40" SIEVE (425um)	97.5	98.4	99.3	98.0
#60 SIEVE (250um)	94.5	92.9	97.4	97.0
#100 SIEVE (150um)	82.1	67.8	80.4	95.5
#140 SIEVE (106um)	70.1	44.8	61.9	92.7
#200 SIEVE (75um)	55.2	26.7	46.6	82.4

Clay				
Silt				
Total Sand	44.8	73.3	53.4	17.6
Total Gravel	0.0	0.0	0.0	0.0

ATTERBERG LIMITS				
Liquid Limit	34	NP	30	41
Plastic Limit	17	NP	21	19
Plasticity Index	17	NP	9	22

USCS	CL	SM	SC	CL
AASHTO	A-6(6)	A-2-4(0)	A-4(1)	A-7-6(18)



	Specimen No.	1	2	3
Initial	Water Content, %	15.8	16.6	16.7
	Dry Density, pcf	111.4	113.9	114.8
	Saturation, %	85.4	96.7	99.7
	Void Ratio	0.4909	0.4578	0.4460
	Diameter, in.	1.447	1.427	1.417
	Height, in.	2.790	2.780	2.780
At Test	Water Content, %	19.7	19.0	18.0
	Dry Density, pcf	111.4	113.9	114.8
	Saturation, %	106.9	110.1	107.2
	Void Ratio	0.4909	0.4578	0.4460
	Diameter, in.	1.447	1.427	1.417
	Height, in.	2.790	2.780	2.780
Strain at peak, %		4.0	5.7	13.1
Eff. Cell Pressure, psf		1265.8	2158.6	4078.1
Fail. Stress, psf		3871.0	7266.0	9335.7
Excess Pore Pr., psf		-208.4	-772.6	-538.7
Strain, %		4.0	5.7	13.1
Ult. Stress, psf		3871.0	7266.0	9335.7
Excess Pore Pr., psf		-208.4	-772.6	-538.7
Strain, %		4.0	5.7	13.1
$\bar{\sigma}_1$ Failure, psf		5345.2	10197.2	13952.5
$\bar{\sigma}_3$ Failure, psf		1474.2	2931.2	4616.8

**Type of Test:**

CU with Pore Pressures

**Sample Type:** 3-in. Shelby Tube

**Description:** SANDY LEAN CLAY (CL, A-7-6(10))

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Asymmetrical  
Shear Plane

**Figure** \_\_\_\_\_

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 8.5'-10.0'

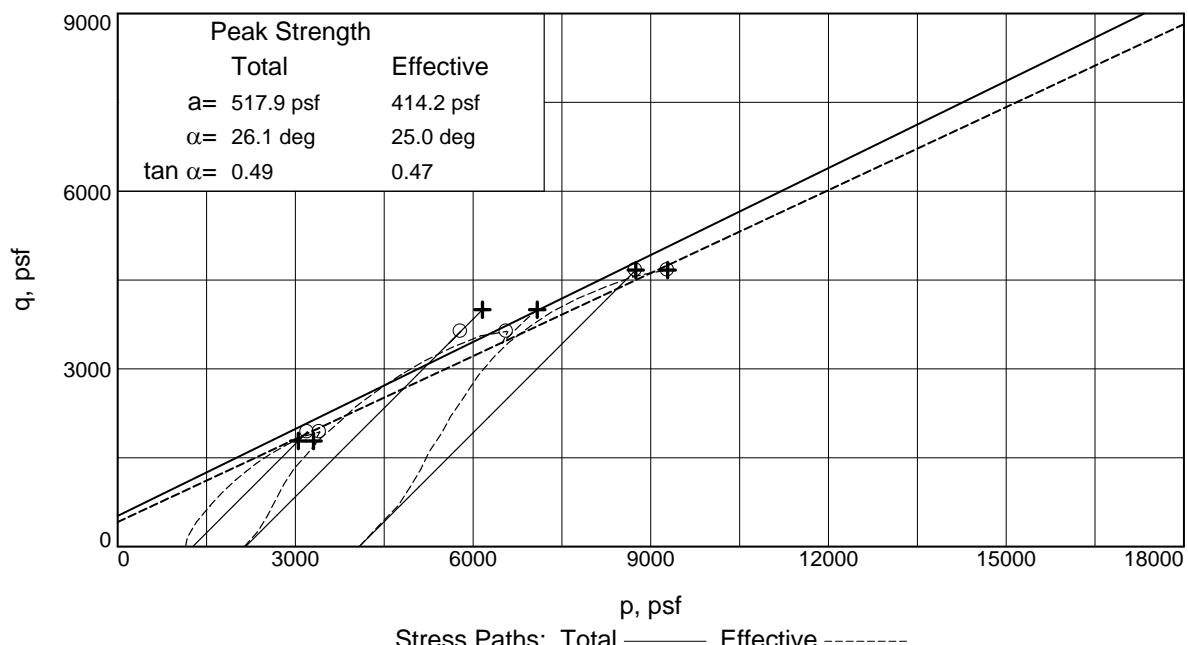
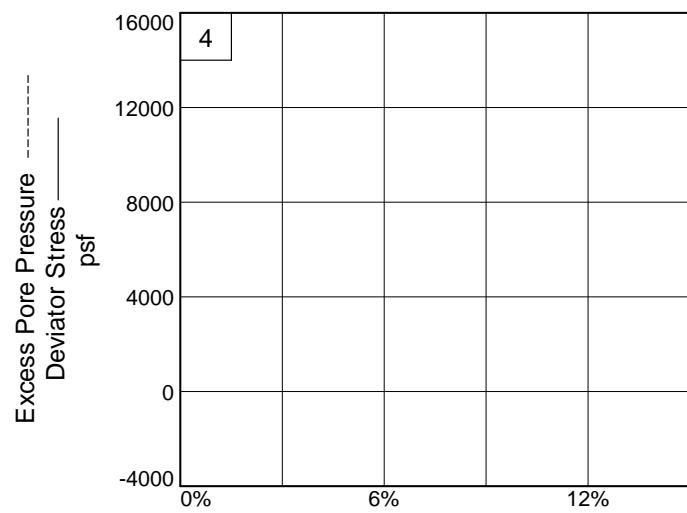
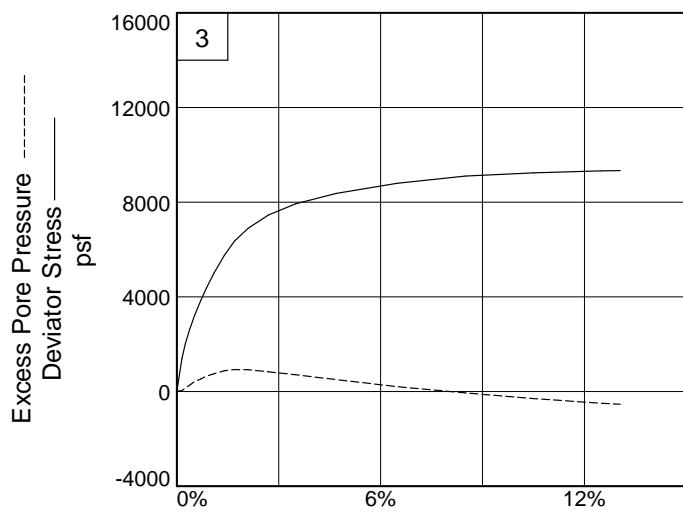
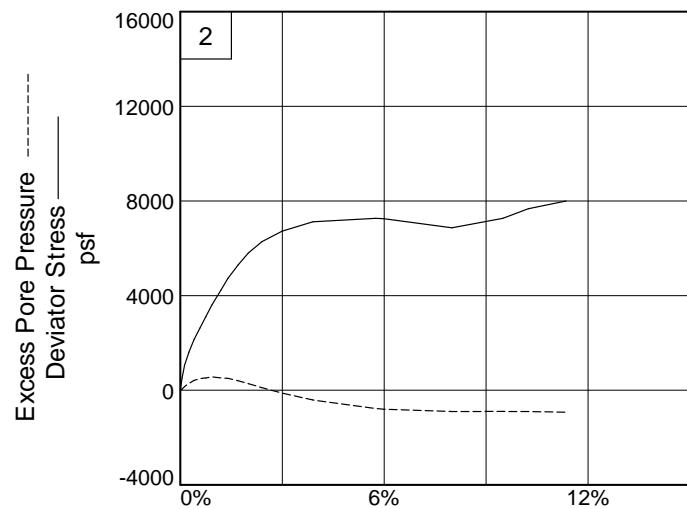
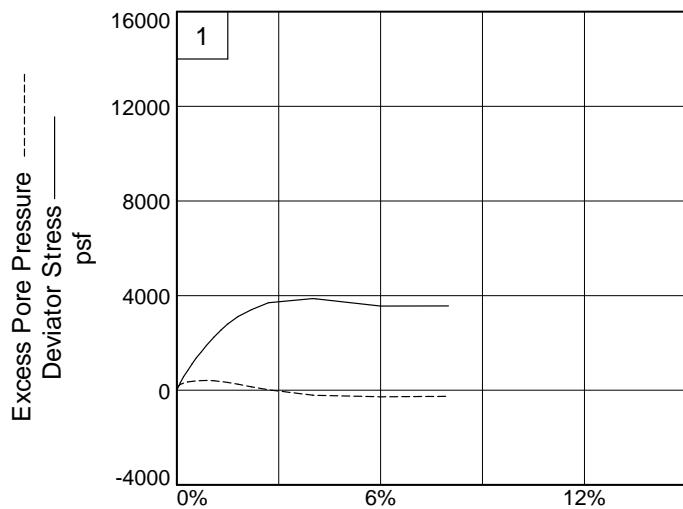
**Sample Number:** TH-28 T-1

**Proj. No.:** 1511010228

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

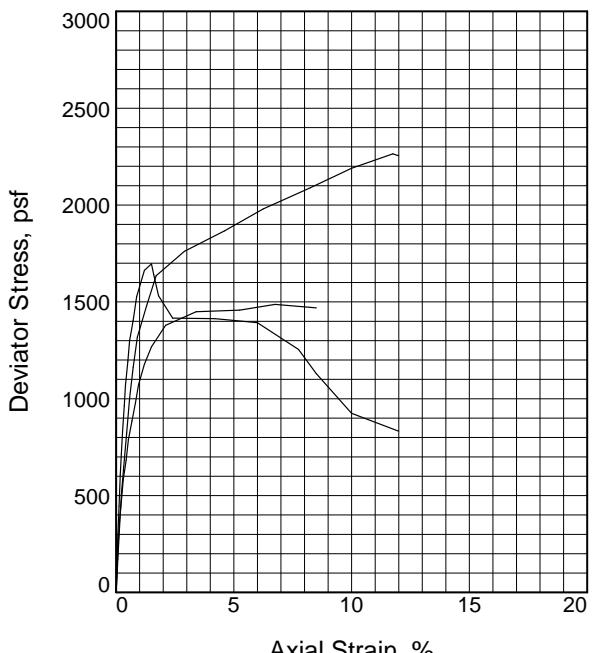
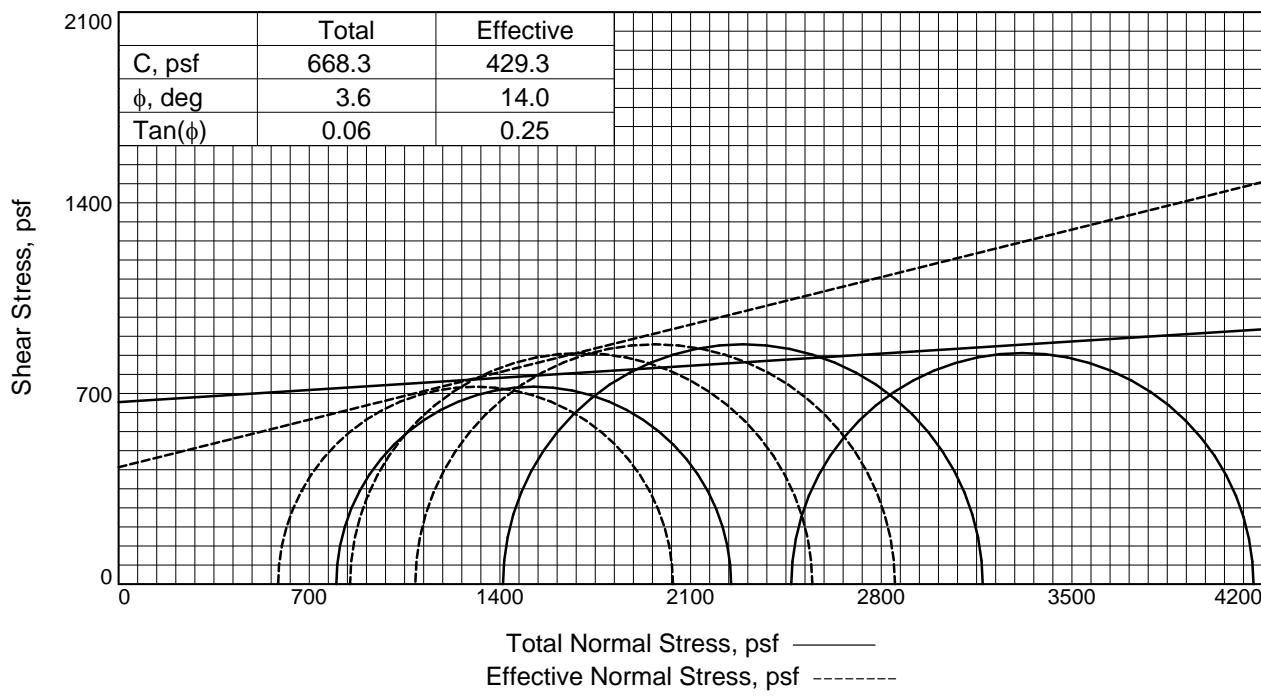
**Depth:** 8.5'-10.0'

**Project No.:** 1511010228

**Sample Number:** TH-28 T-1

**Figure** \_\_\_\_\_

**Thompson Engineering**



	Initial	1	2	3
Water Content, %	29.6	29.4	25.3	
Dry Density, pcf	93.6	94.2	100.1	
Saturation, %	101.7	102.7	102.3	
Void Ratio	0.7733	0.7621	0.6588	
Diameter, in.	1.416	1.422	1.414	
Height, in.	2.790	2.790	2.790	
	At Test	1	2	3
Water Content, %	2.0	29.9	25.6	
Dry Density, pcf	93.6	94.2	100.1	
Saturation, %	6.8	104.2	103.4	
Void Ratio	0.7733	0.7621	0.6588	
Diameter, in.	1.416	1.422	1.414	
Height, in.	2.790	2.790	2.790	
Strain at peak, %		3.4	2.9	1.5
Eff. Cell Pressure, psf		799.2	1411.2	2469.6
Fail. Stress, psf		1449.5	1761.0	1696.7
Excess Pore Pr., psf		213.6	322.0	1619.7
Strain, %		3.4	2.9	1.5
Ult. Stress, psf		1449.5	1761.0	
Excess Pore Pr., psf		213.6	322.0	
Strain, %		3.4	2.9	
$\bar{\sigma}_1$ Failure, psf		2035.0	2850.2	2546.6
$\bar{\sigma}_3$ Failure, psf		585.6	1089.2	849.9

**Type of Test:**

CU with Pore Pressures

**Sample Type:** 3-in. Shelby Tube

**Description:** LEAN CLAY (CL, A-7-6(25))

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Symmetrical  
Bulge

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8210

**Depth:** 8.5'-10.0'

**Sample Number:** TH-29 T-1

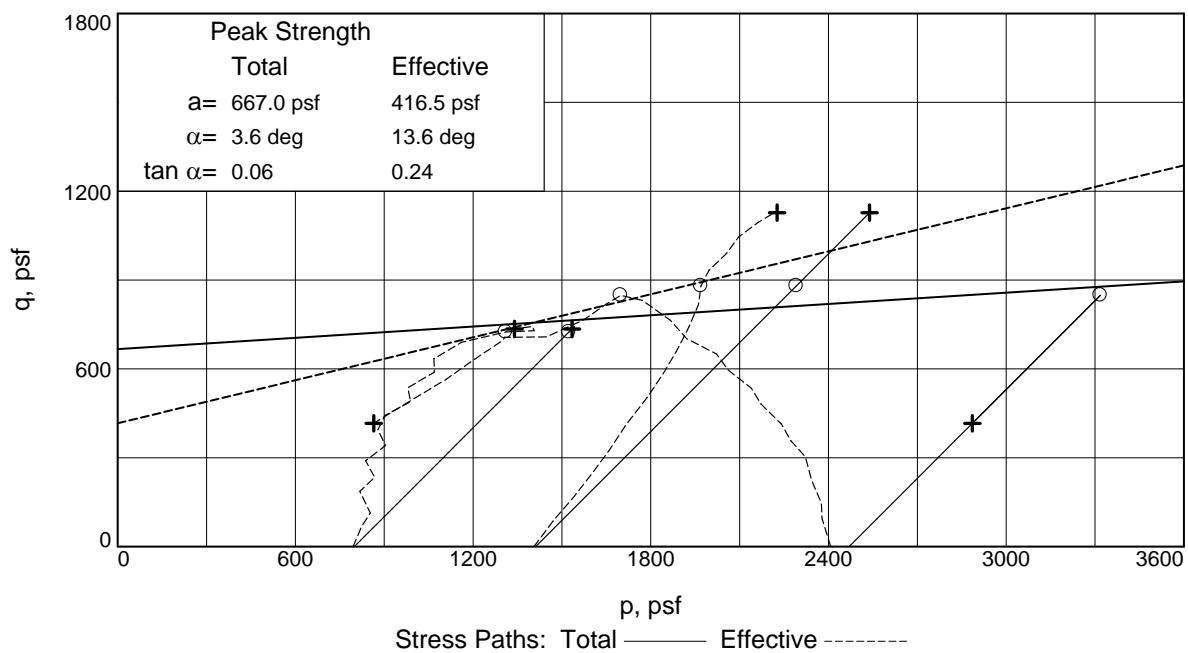
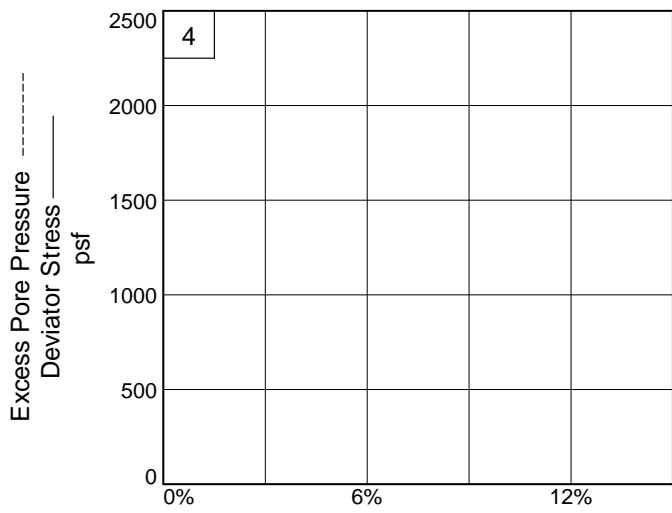
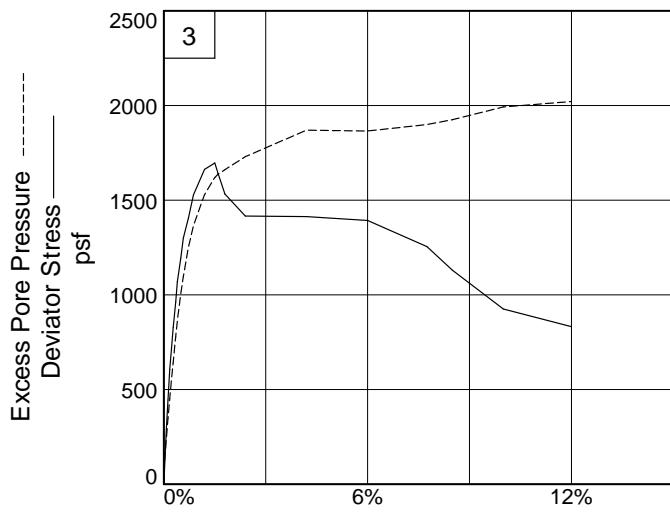
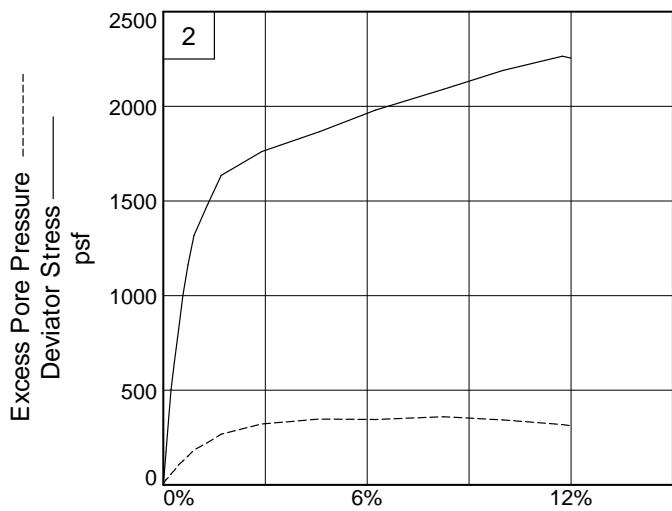
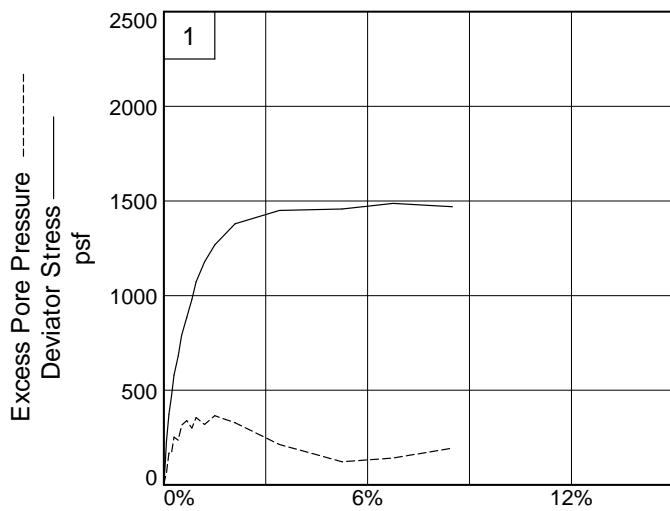
**Proj. No.:** 1511010228

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

 Thompson Engineering  
Mobile, Alabama

**Figure** \_\_\_\_\_



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8210

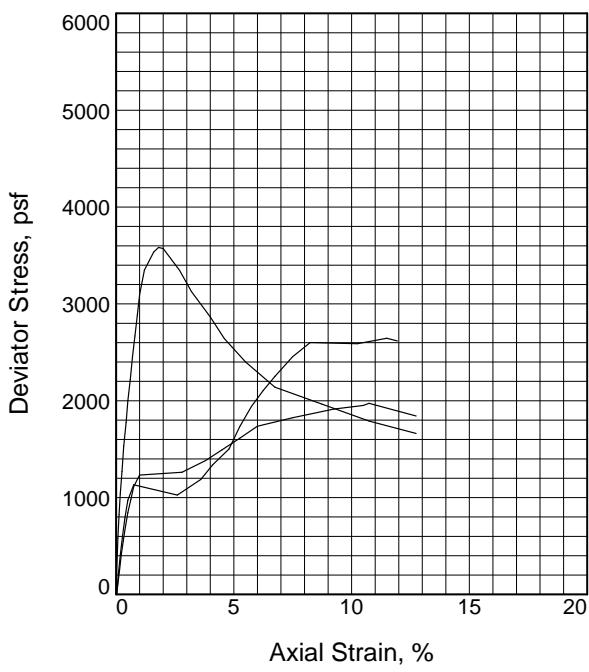
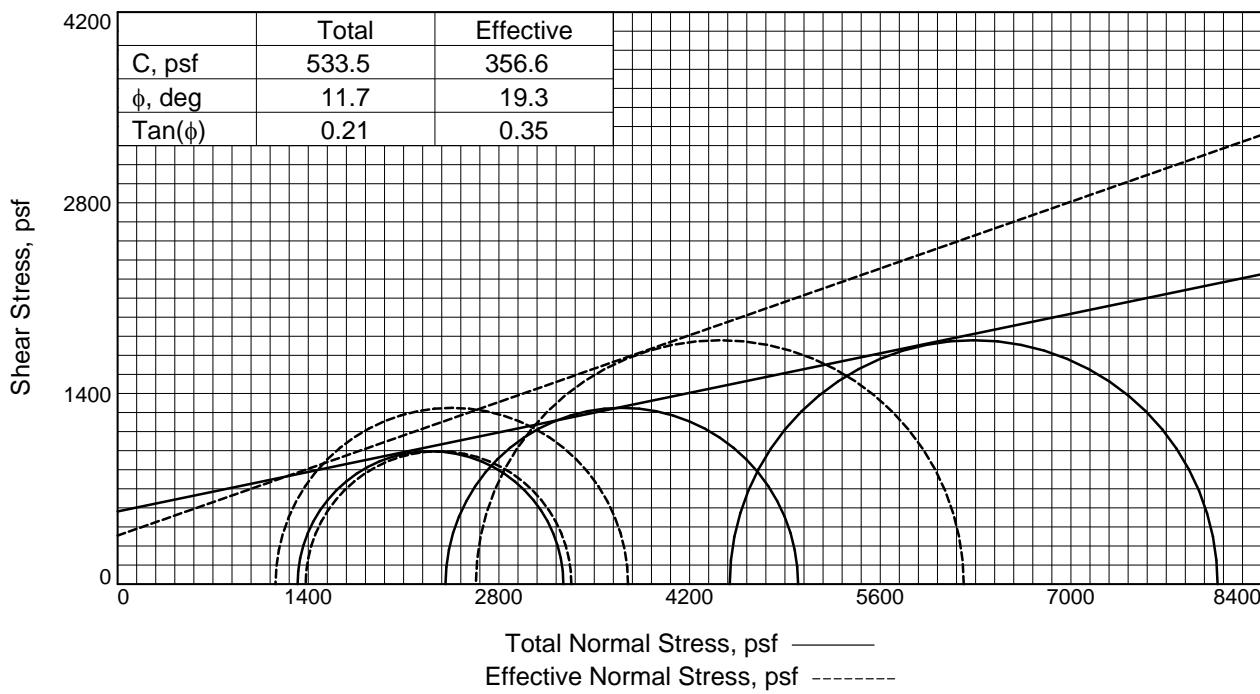
**Project No.:** 1511010228

**Depth:** 8.5'-10.0'

**Figure** \_\_\_\_\_

**Sample Number:** TH-29 T-1

**Thompson Engineering**



	Specimen No.	1	2	3
Initial	Water Content, %	22.5	23.1	21.1
	Dry Density, pcf	104.9	102.6	106.9
	Saturation, %	102.8	99.4	101.5
	Void Ratio	0.5824	0.6190	0.5536
	Diameter, in.	1.420	1.424	1.417
	Height, in.	2.780	2.780	2.780
At Test	Water Content, %	23.5	24.5	22.3
	Dry Density, pcf	104.9	102.6	106.9
	Saturation, %	107.5	105.3	107.0
	Void Ratio	0.5824	0.6190	0.5536
	Diameter, in.	1.420	1.424	1.417
	Height, in.	2.780	2.780	2.780
Strain at peak, %		10.5	10.2	1.8
Eff. Cell Pressure, psf		1321.9	2407.7	4494.2
Fail. Stress, psf		1951.1	2588.6	3582.2
Excess Pore Pr., psf		-58.8	1248.3	1863.6
Strain, %		10.5	10.2	1.8
Ult. Stress, psf		1951.1	2588.6	3582.2
Excess Pore Pr., psf		-58.8	1248.3	1863.6
Strain, %		10.5	10.2	1.8
$\bar{\sigma}_1$ Failure, psf		3331.9	3747.9	6212.8
$\bar{\sigma}_3$ Failure, psf		1380.7	1159.4	2630.6

**Type of Test:**

CU with Pore Pressures

**Sample Type:** 3-in. Shelby Tube

**Description:** FAT CLAY (CH, A-7-6(45)) Specimen was very soft and wanted to sluff off during setup.

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Asymmetrical Shear Plane

**Figure** \_\_\_\_\_

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 8.5'-10.5'

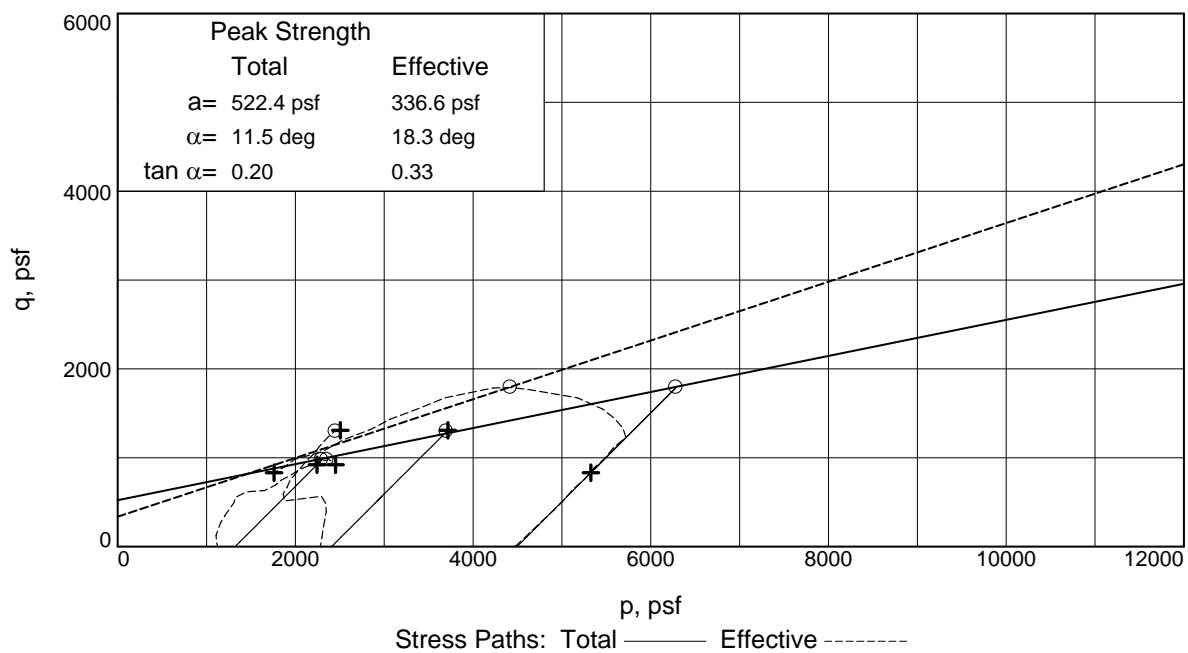
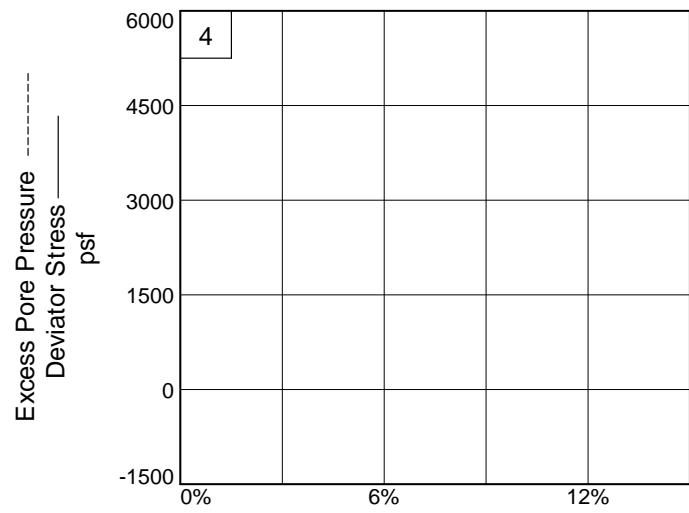
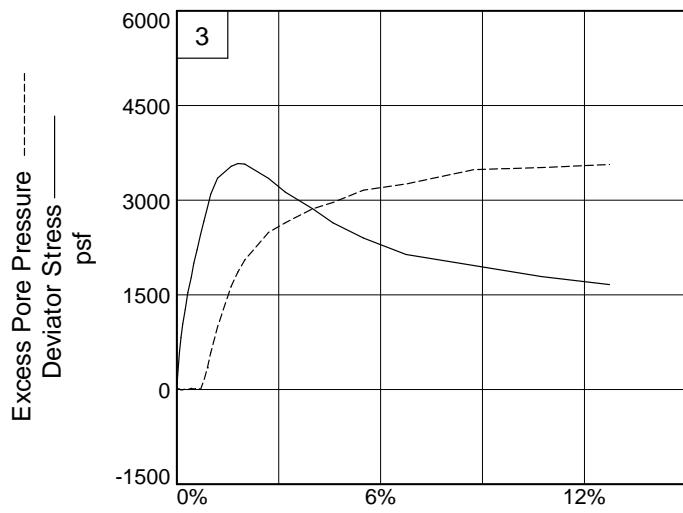
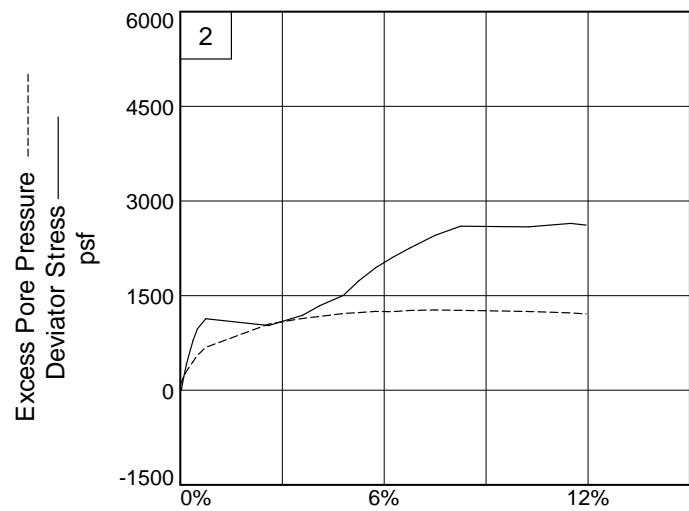
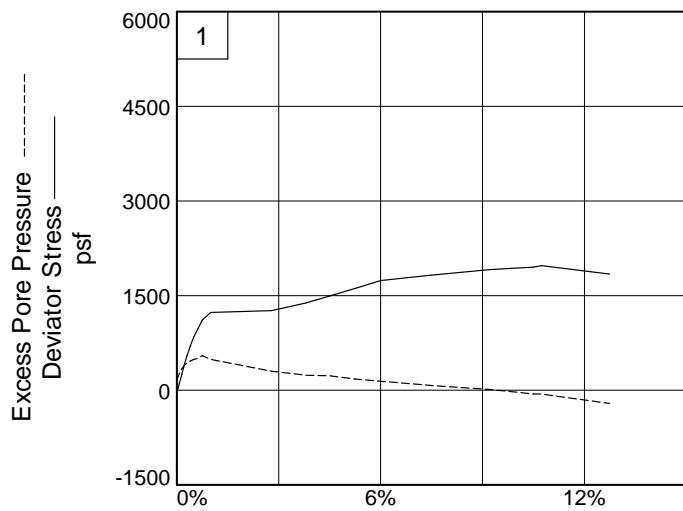
**Sample Number:** TH-31 T-1

**Proj. No.:** 1511010228

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

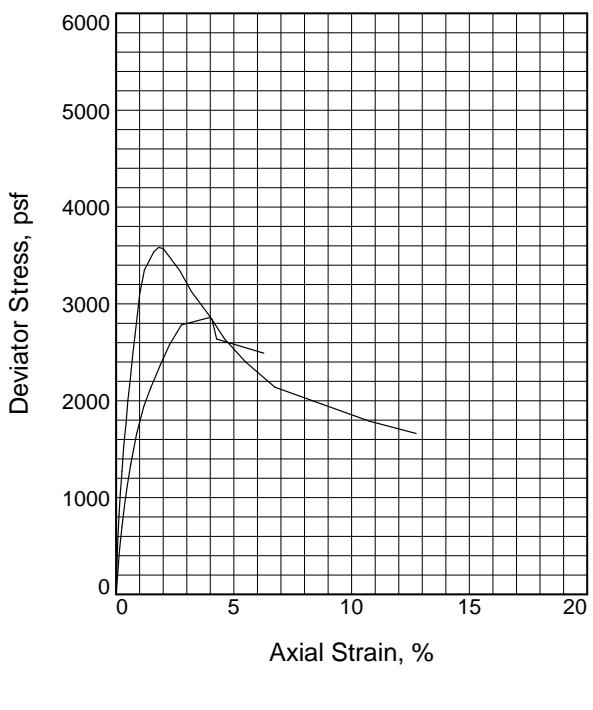
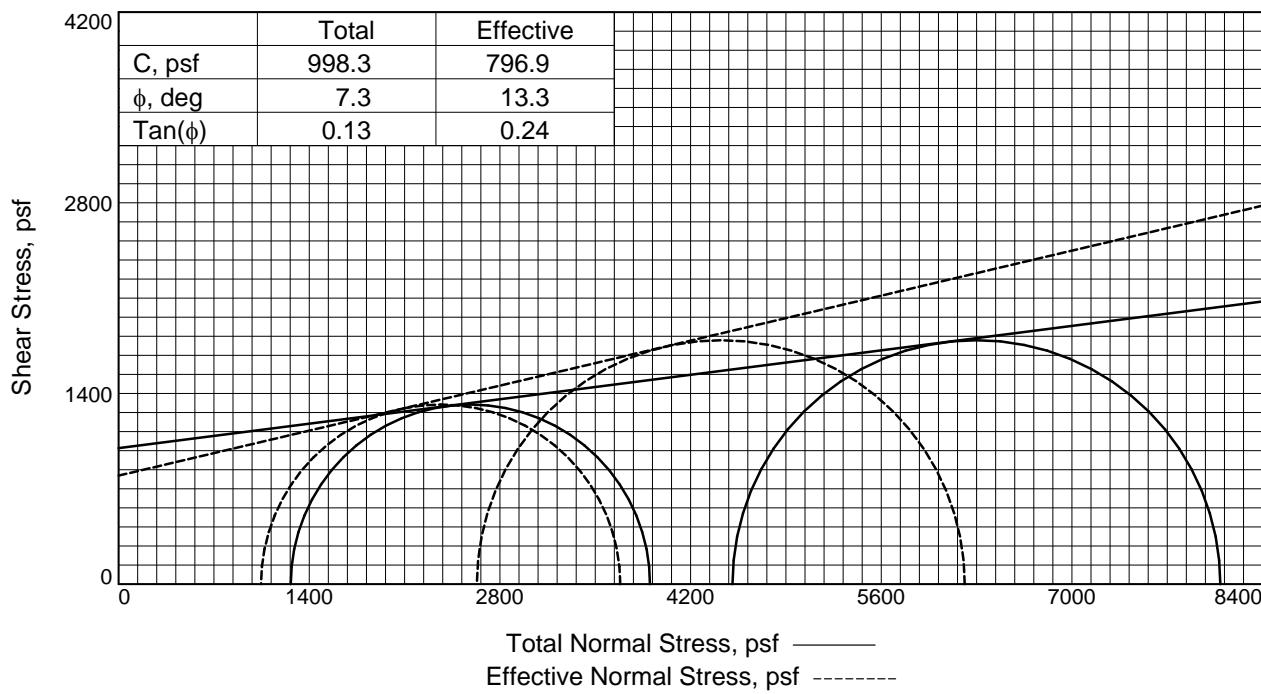
**Depth:** 8.5'-10.5'

**Project No.:** 1511010228

**Figure** \_\_\_\_\_

**Sample Number:** TH-31 T-1

**Thompson Engineering**


**Type of Test:**

CU with Pore Pressures

**Sample Type:** 3-in. Shelby Tube

**Description:** SILTY SAND (SM, A-4(0))

Sample was sandy compared to other CU test specimens, only able to test 2 points.

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Asymmetrical Shear Plane

**Figure** \_\_\_\_\_

	Specimen No.	
	1	2
Initial	Water Content, %	31.6
	Dry Density, pcf	85.4
	Saturation, %	88.9
	Void Ratio	0.9442
	Diameter, in.	1.427
	Height, in.	2.780
At Test	Water Content, %	36.9
	Dry Density, pcf	85.4
	Saturation, %	104.1
	Void Ratio	0.9442
	Diameter, in.	1.427
	Height, in.	2.780
Strain at peak, %		
Eff. Cell Pressure, psf		
Fail. Stress, psf		
Excess Pore Pr., psf		
Strain, %		
Ult. Stress, psf		
Excess Pore Pr., psf		
Strain, %		
$\bar{\sigma}_1$ Failure, psf	3683.4	6212.8
$\bar{\sigma}_3$ Failure, psf	1046.0	2630.6

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 23.5'-25.5'

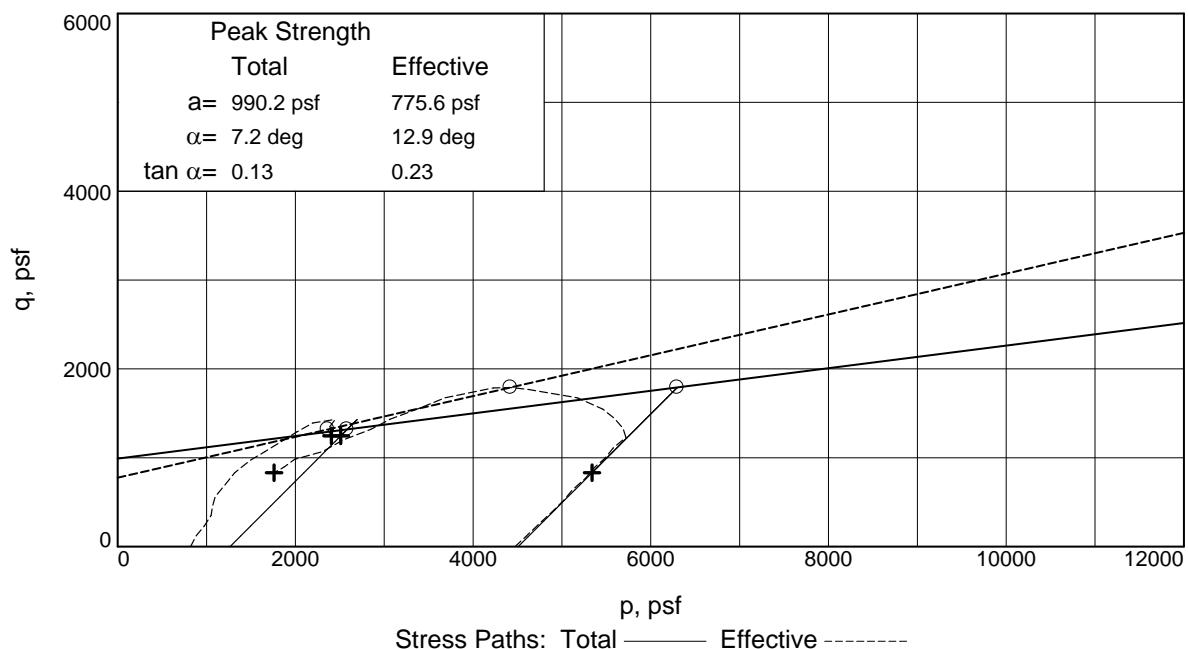
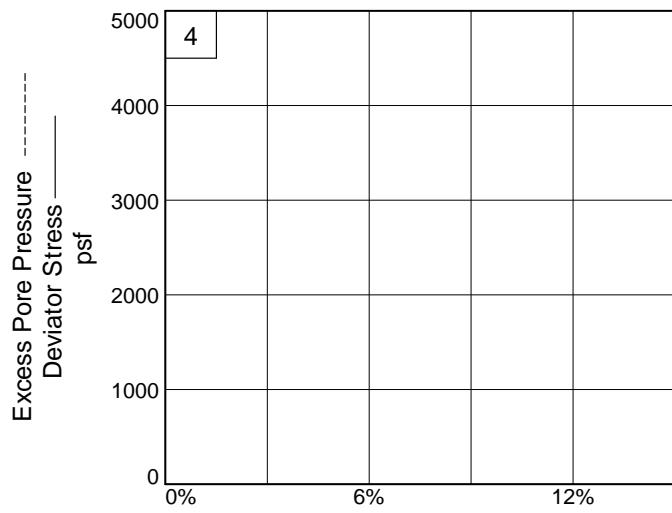
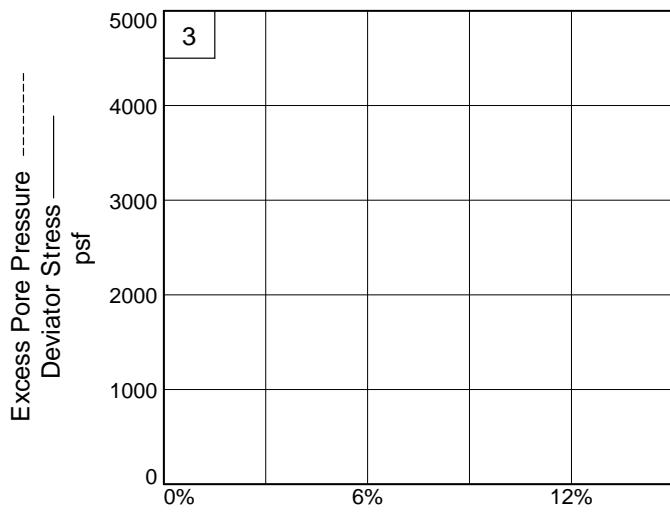
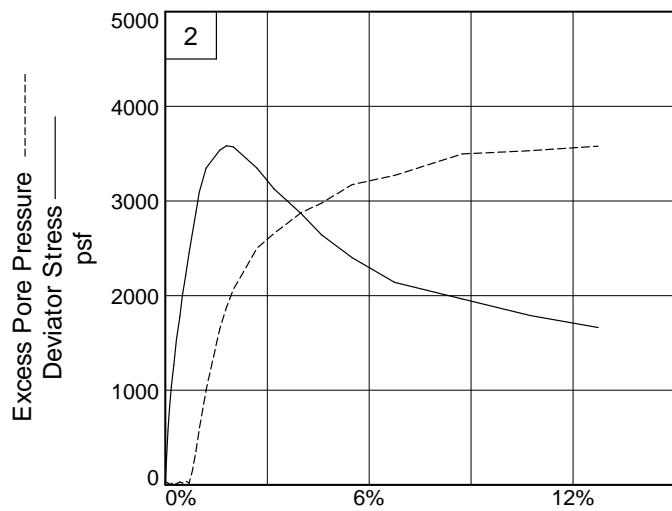
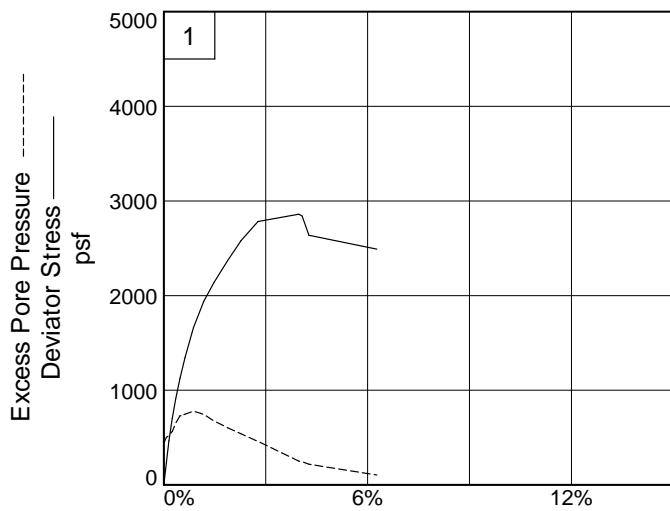
**Sample Number:** TH-31 T-2

**Proj. No.:** 1511010228

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

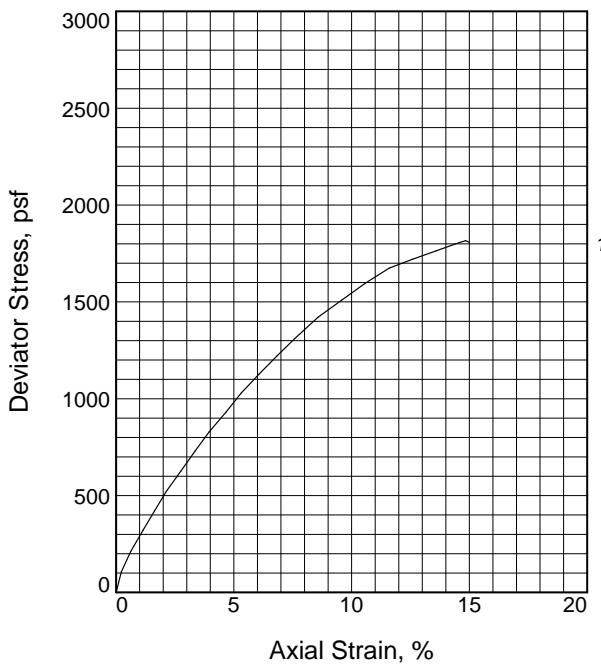
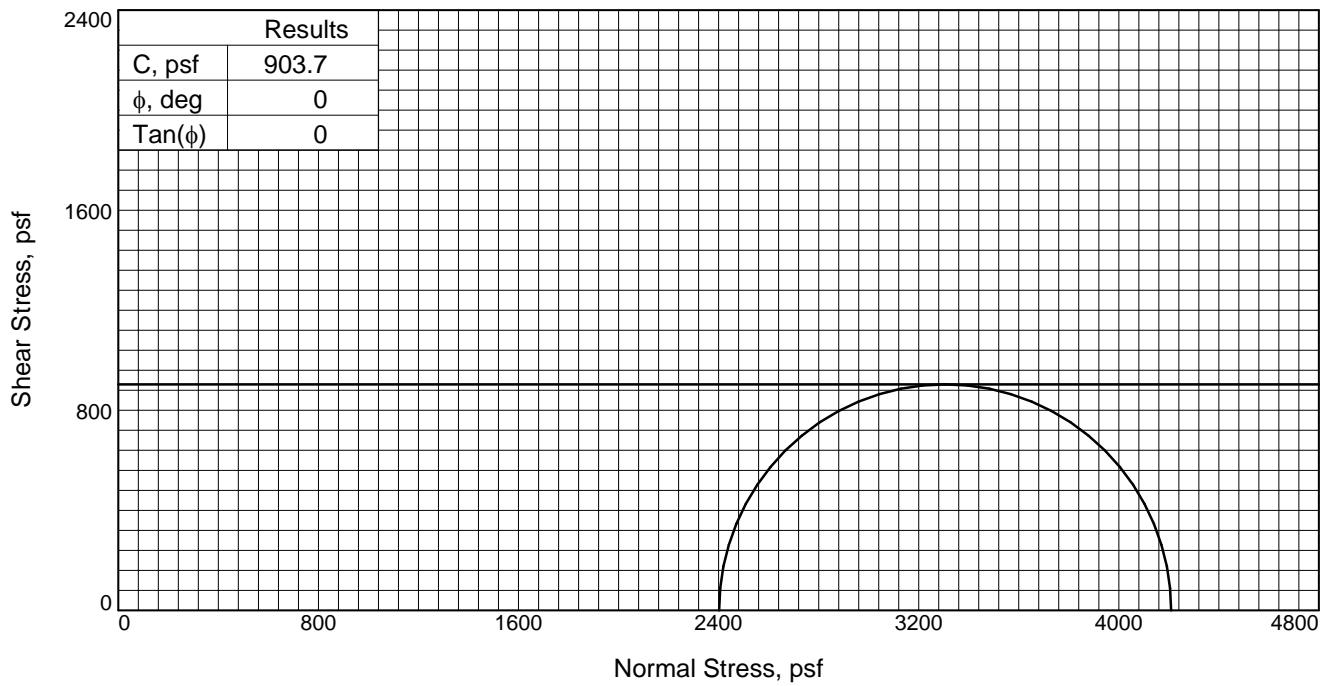
**Project No.:** 1511010228

**Depth:** 23.5'-25.5'

**Figure** \_\_\_\_\_

**Sample Number:** TH-31 T-2

**Thompson Engineering**



Specimen No.		1
Initial	Water Content, %	27.7
	Dry Density, pcf	99.1
	Saturation, %	109.0
	Void Ratio	0.6756
	Diameter, in.	2.824
	Height, in.	5.497
At Test	Water Content, %	26.4
	Dry Density, pcf	99.1
	Saturation, %	104.1
	Void Ratio	0.6756
	Diameter, in.	2.824
	Height, in.	5.497
Strain at peak, %		15.0
Back Pressure, psf		0.0
Cell Pressure, psf		2401.9
Fail. Stress, psf		1807.5
Strain, %		15.0
Ult. Stress, psf		1807.5
Strain, %		15.0
$\sigma_1$ Failure, psf		4209.4
$\sigma_3$ Failure, psf		2401.9

**Type of Test:**

Unconsolidated Undrained

**Sample Type:** 3-in. Shelby Tube

**Description:** SILTY, CLAYEY SAND (SC-SM, A-2-4(0))

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Symmetrical Bulge

**Figure** \_\_\_\_\_

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8210

**Depth:** 33.5'-35.5'

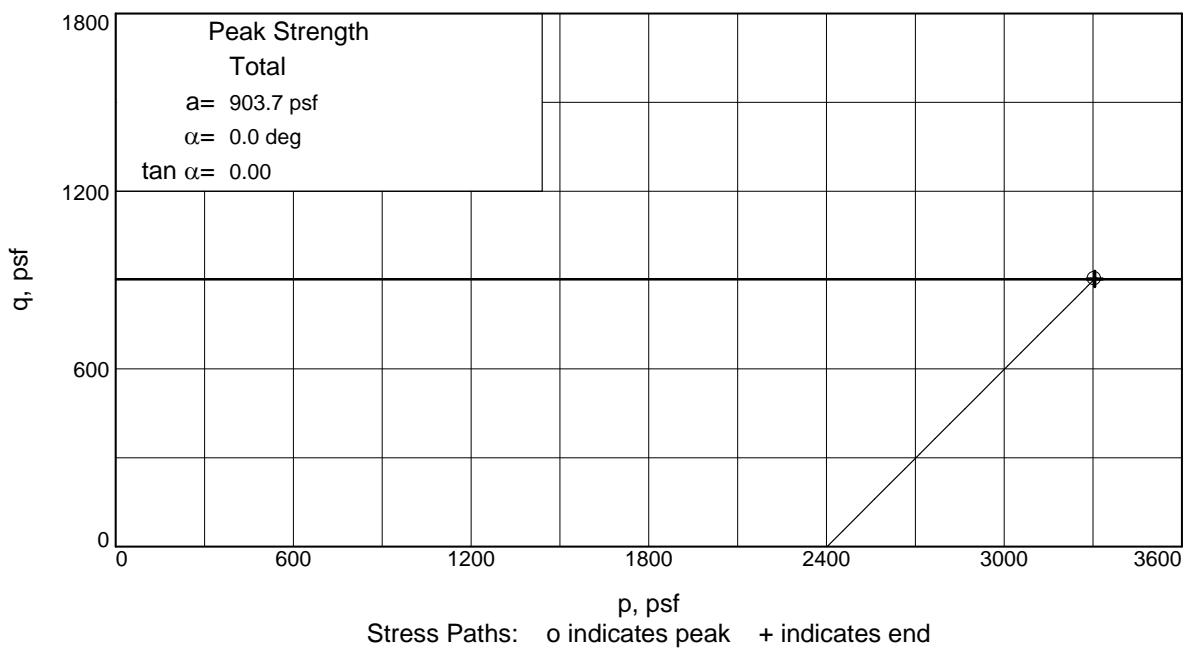
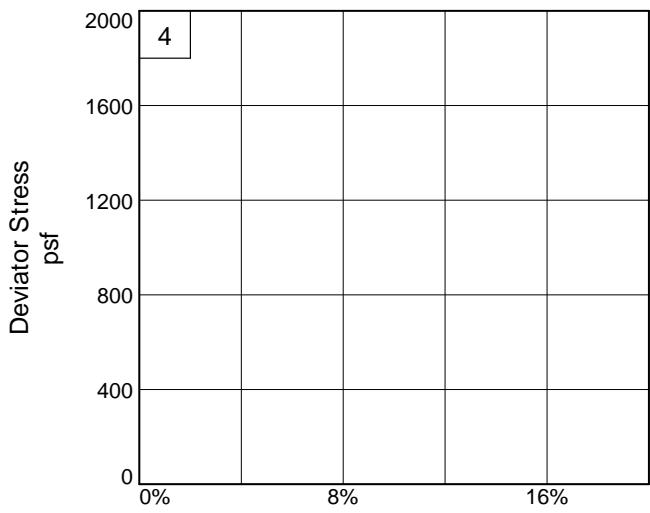
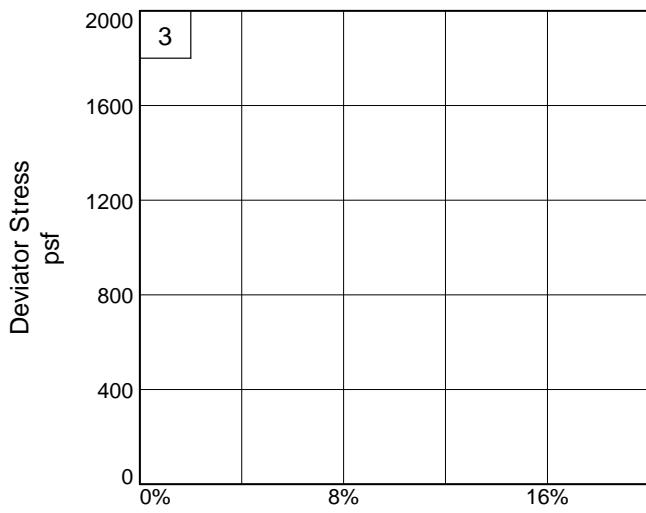
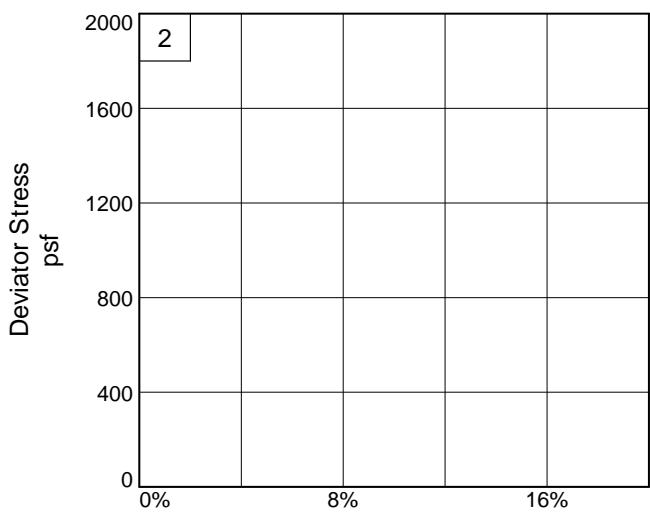
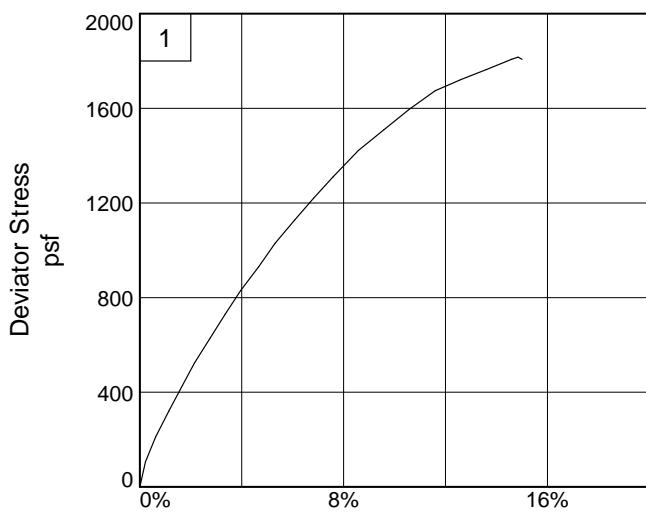
**Sample Number:** TH-30 T-2

**Proj. No.:** 1511010228

**Date Sampled:**

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 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8210

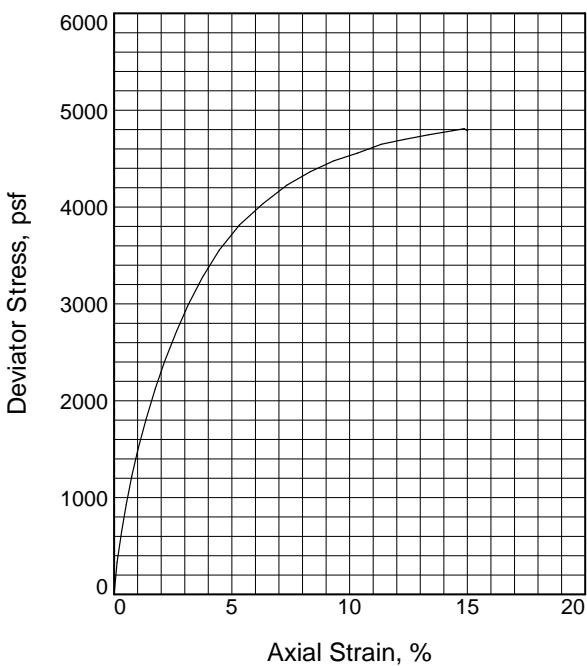
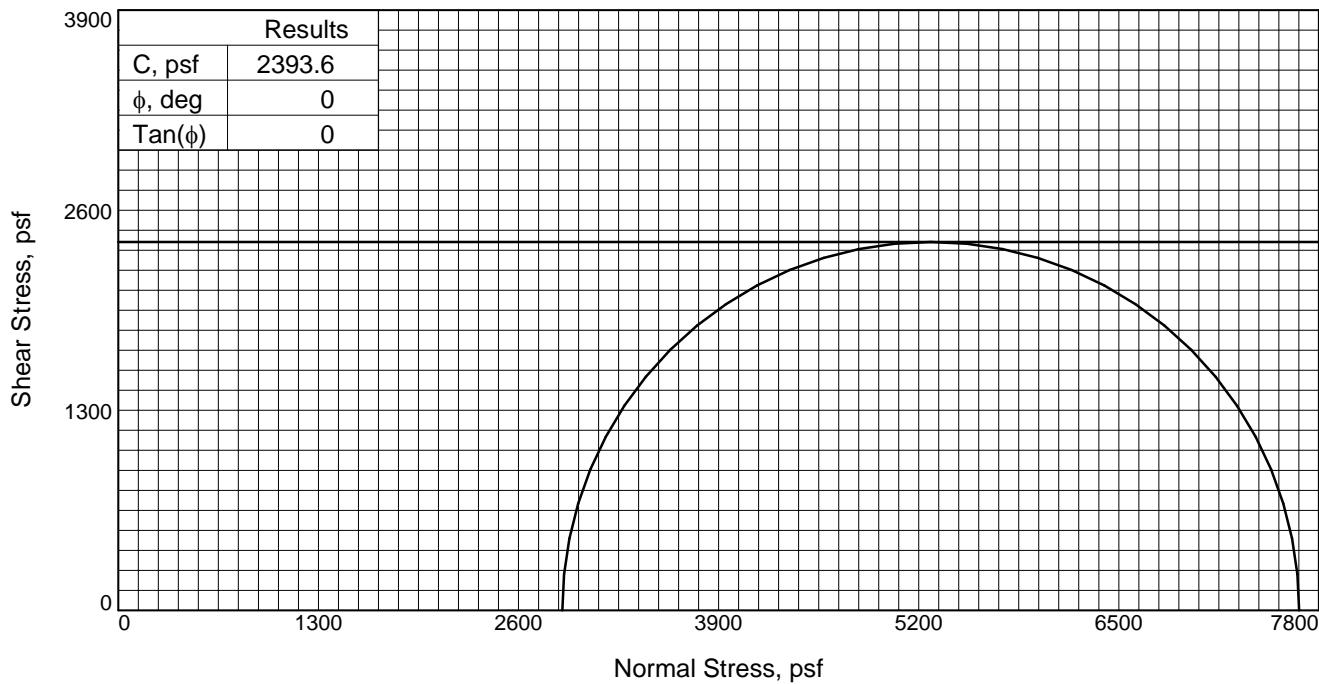
**Project No.:** 1511010228

**Depth:** 33.5'-35.5'

**Figure** \_\_\_\_\_

**Sample Number:** TH-30 T-2

**Thompson Engineering**


**Type of Test:**

Unconsolidated Undrained

**Sample Type:** 3-in. Shelby Tube

**Description:** SILTY SAND (SM, A-4(0))

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Symmetrical  
Bulge

**Figure** \_\_\_\_\_

	Specimen No.	1
Initial	Water Content, %	21.5
	Dry Density, pcf	103.9
	Saturation, %	95.4
	Void Ratio	0.5990
	Diameter, in.	2.869
	Height, in.	5.766
At Test	Water Content, %	23.0
	Dry Density, pcf	103.9
	Saturation, %	102.0
	Void Ratio	0.5990
	Diameter, in.	2.869
	Height, in.	5.766
Strain at peak, %		
Back Pressure, psf		
Cell Pressure, psf		
Fail. Stress, psf		
Strain, %		
Ult. Stress, psf		
Strain, %		
$\sigma_1$ Failure, psf		
$\sigma_3$ Failure, psf		

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 38.0'-40.0'

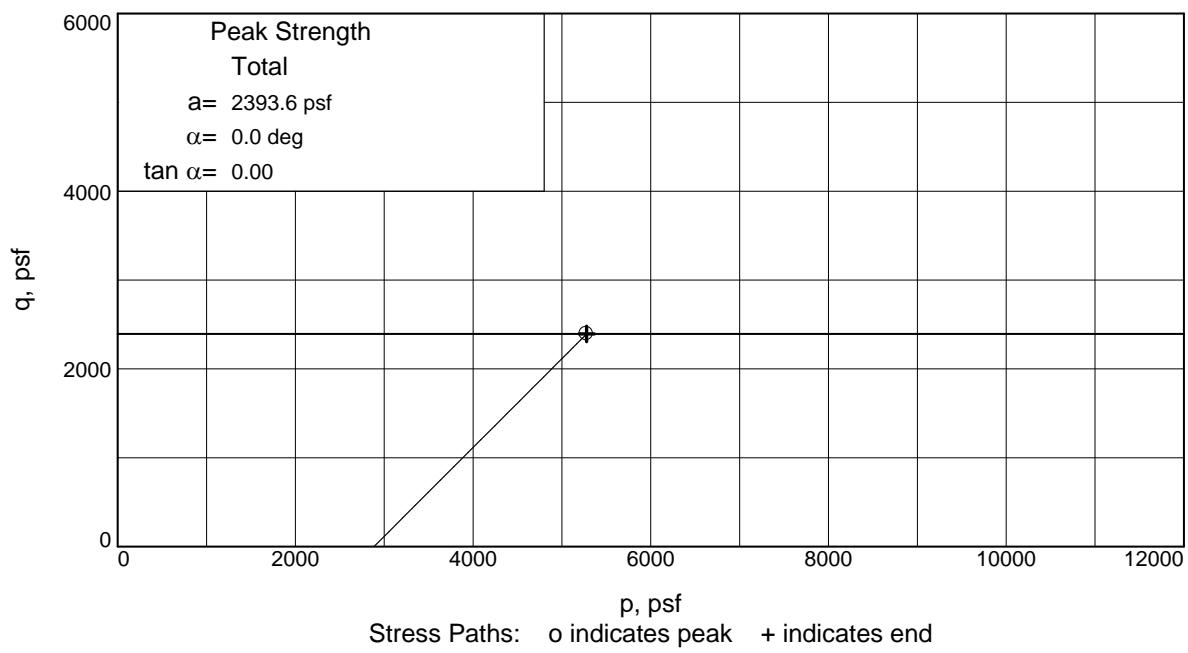
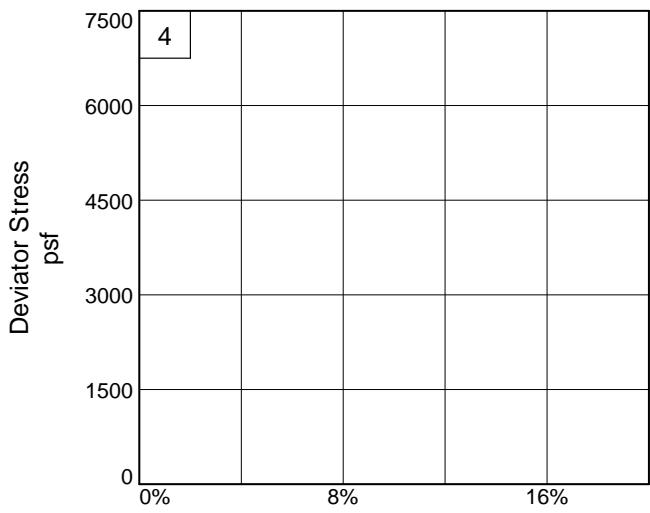
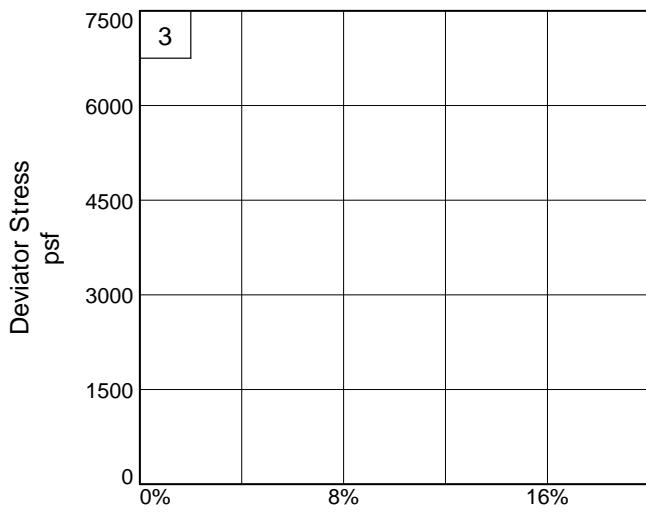
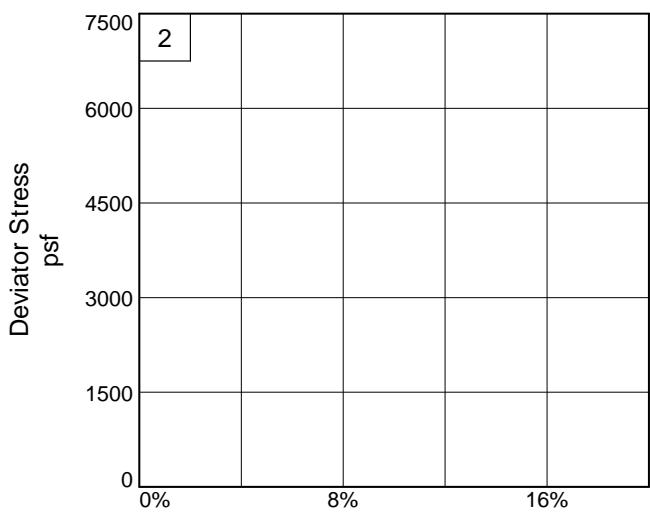
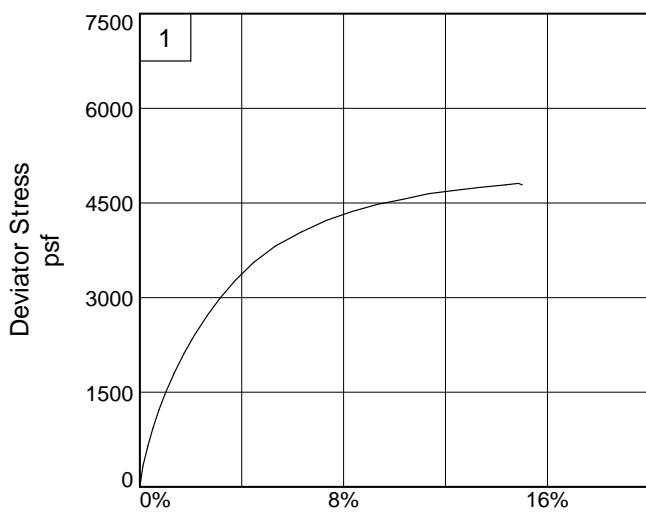
**Sample Number:** TH-31 T-3

**Proj. No.:** 1511010228

**Date Sampled:**

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 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

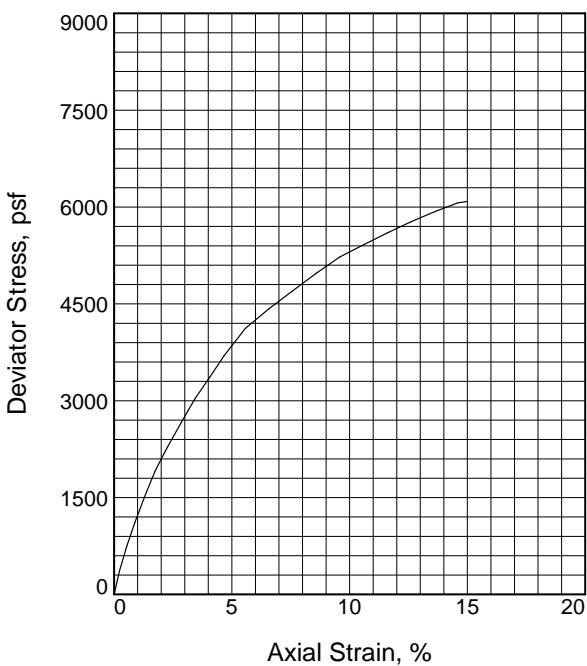
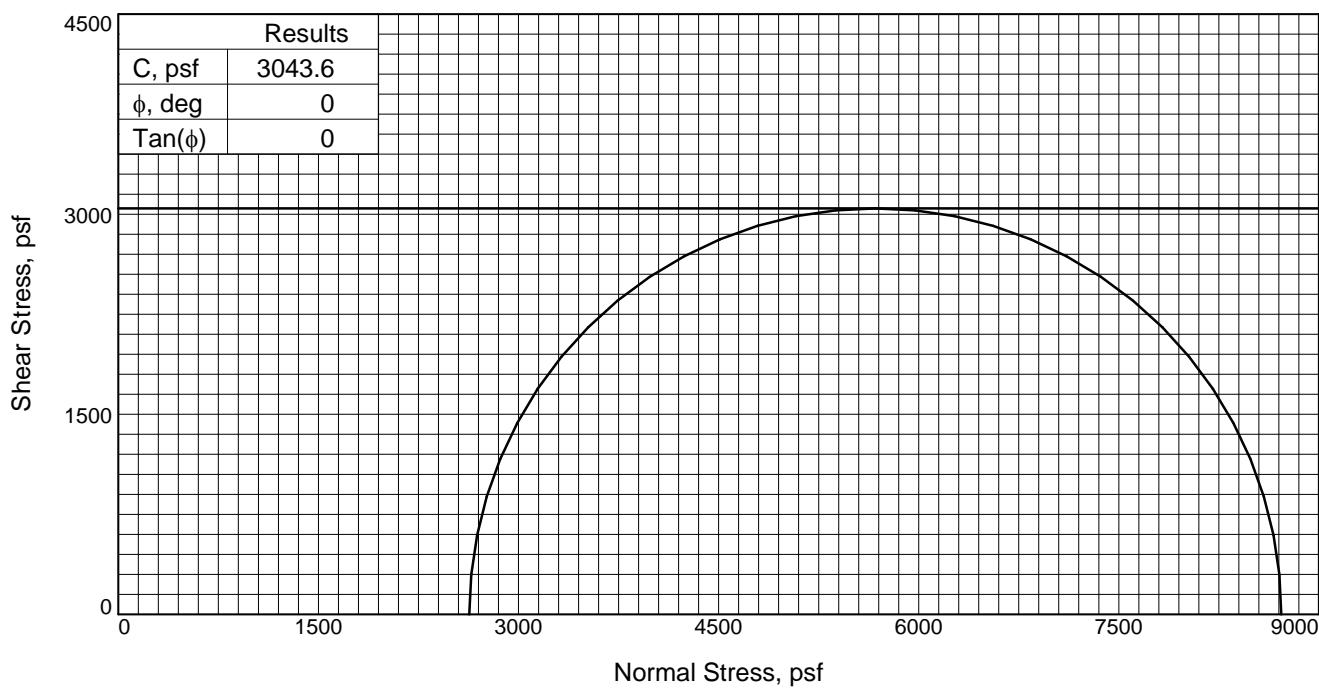
**Depth:** 38.0'-40.0'

**Project No.:** 1511010228

**Figure** \_\_\_\_\_

**Sample Number:** TH-31 T-3

**Thompson Engineering**


**Type of Test:**

Unconsolidated Undrained

**Sample Type:** 3-in. Shelby Tube

**Description:** SILTY SAND (SM, A-2-4(0))

**Specific Gravity=** 2.66

**Remarks:** Compression Failure Mode: Symmetrical  
Bulge

**Figure** \_\_\_\_\_

	Specimen No.	1
Initial	Water Content, %	13.2
	Dry Density, pcf	124.5
	Saturation, %	104.9
	Void Ratio	0.3335
	Diameter, in.	2.855
	Height, in.	5.556
At Test	Water Content, %	13.0
	Dry Density, pcf	124.5
	Saturation, %	103.8
	Void Ratio	0.3335
	Diameter, in.	2.855
	Height, in.	5.556
Strain at peak, %		15.0
Back Pressure, psf		0.0
Cell Pressure, psf		2630.9
Fail. Stress, psf		6087.3
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
$\sigma_1$ Failure, psf		8718.2
$\sigma_3$ Failure, psf		2630.9

**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 23.0'-25.0'

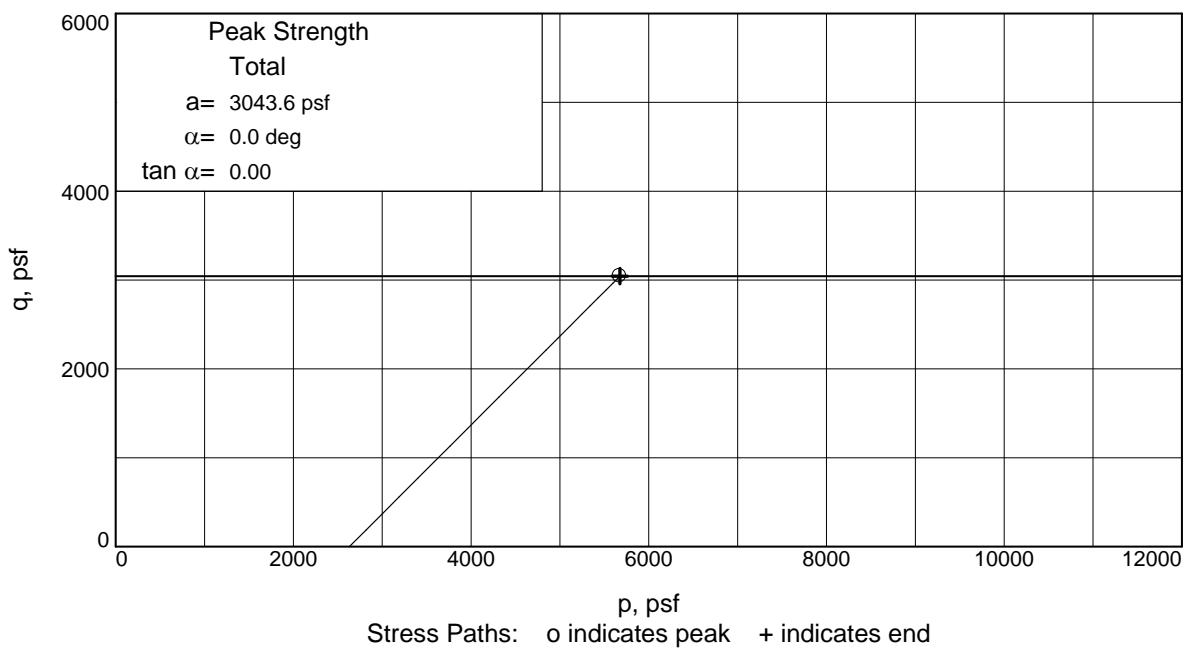
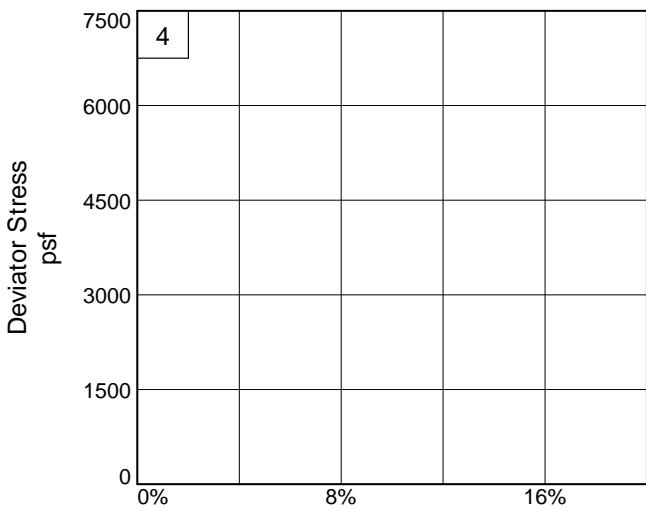
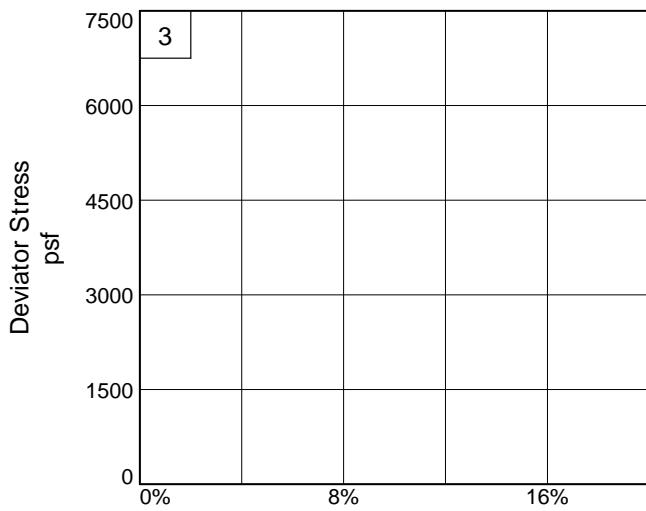
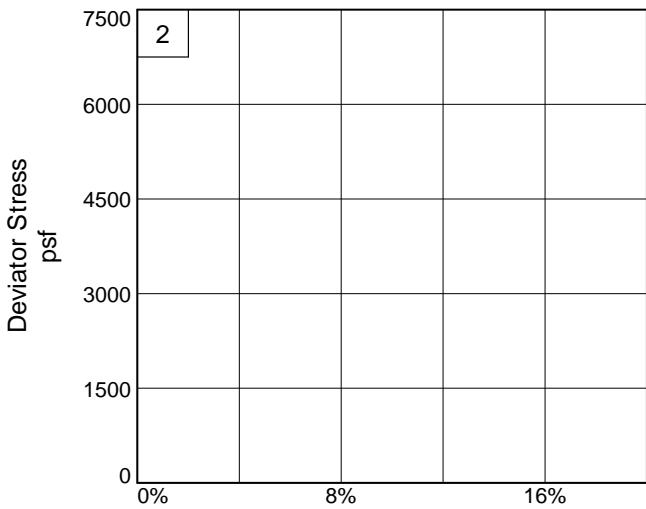
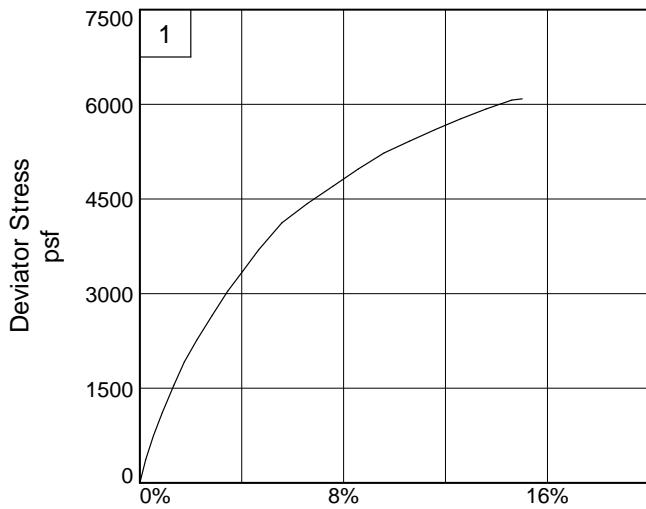
**Sample Number:** TH-32 T-1

**Proj. No.:** 1511010228

**Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

 Thompson Engineering  
Mobile, Alabama



**Client:** ALDOT

**Project:** Mobile River Bridge

**Source of Sample:** Lab #8203

**Depth:** 23.0'-25.0'

**Project No.:** 1511010228

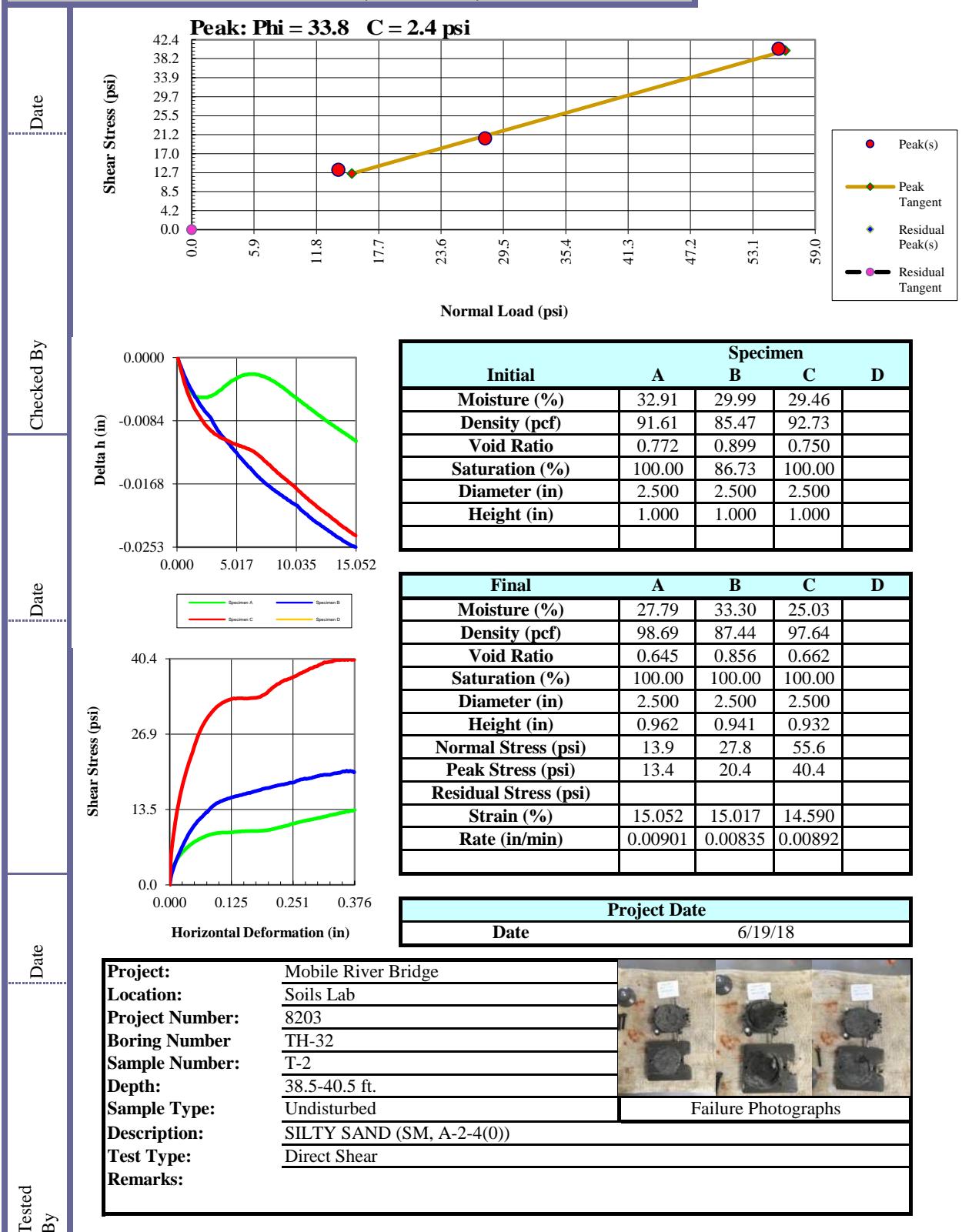
**Sample Number:** TH-32 T-1

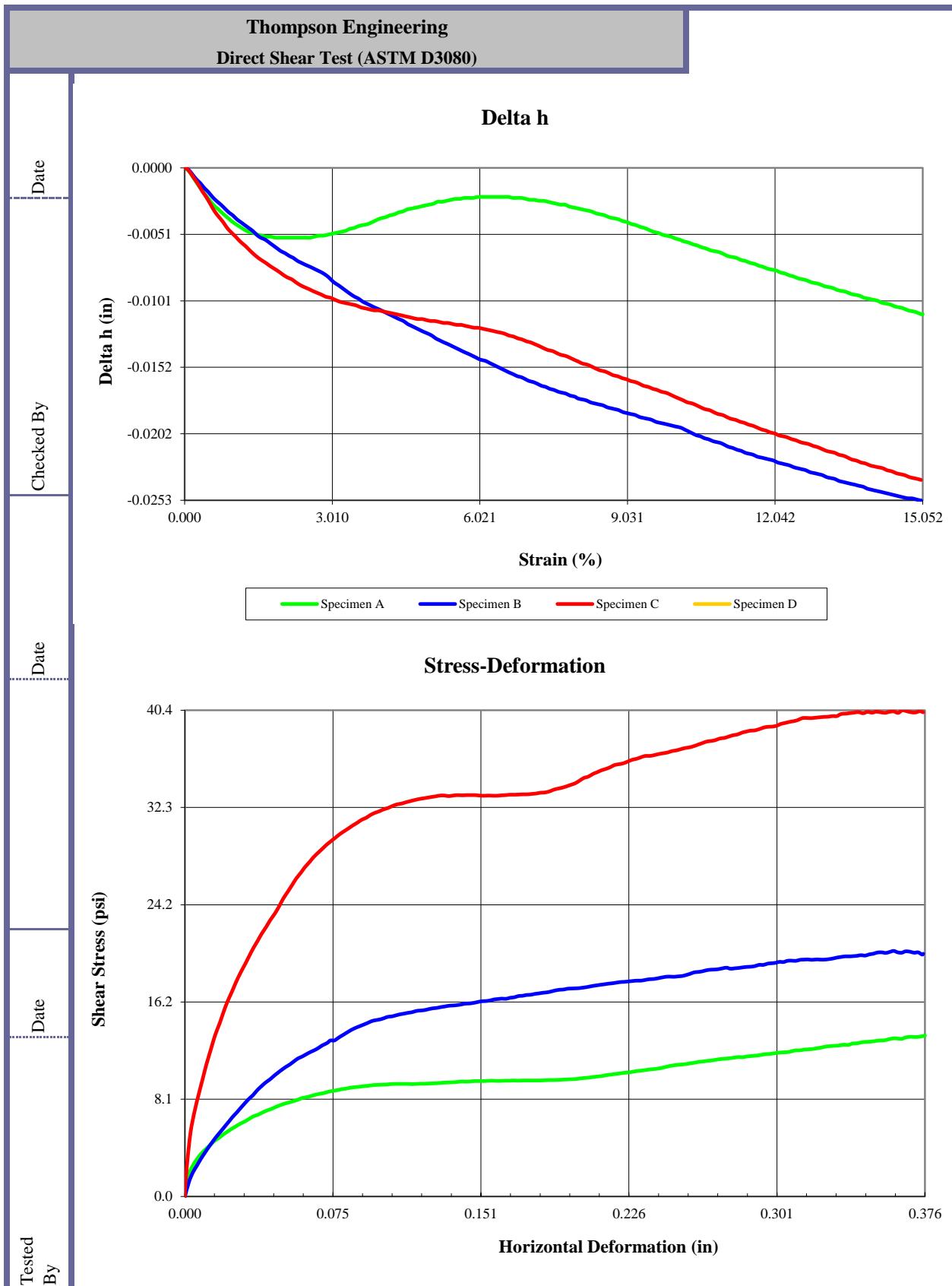
**Figure** \_\_\_\_\_

**Thompson Engineering**

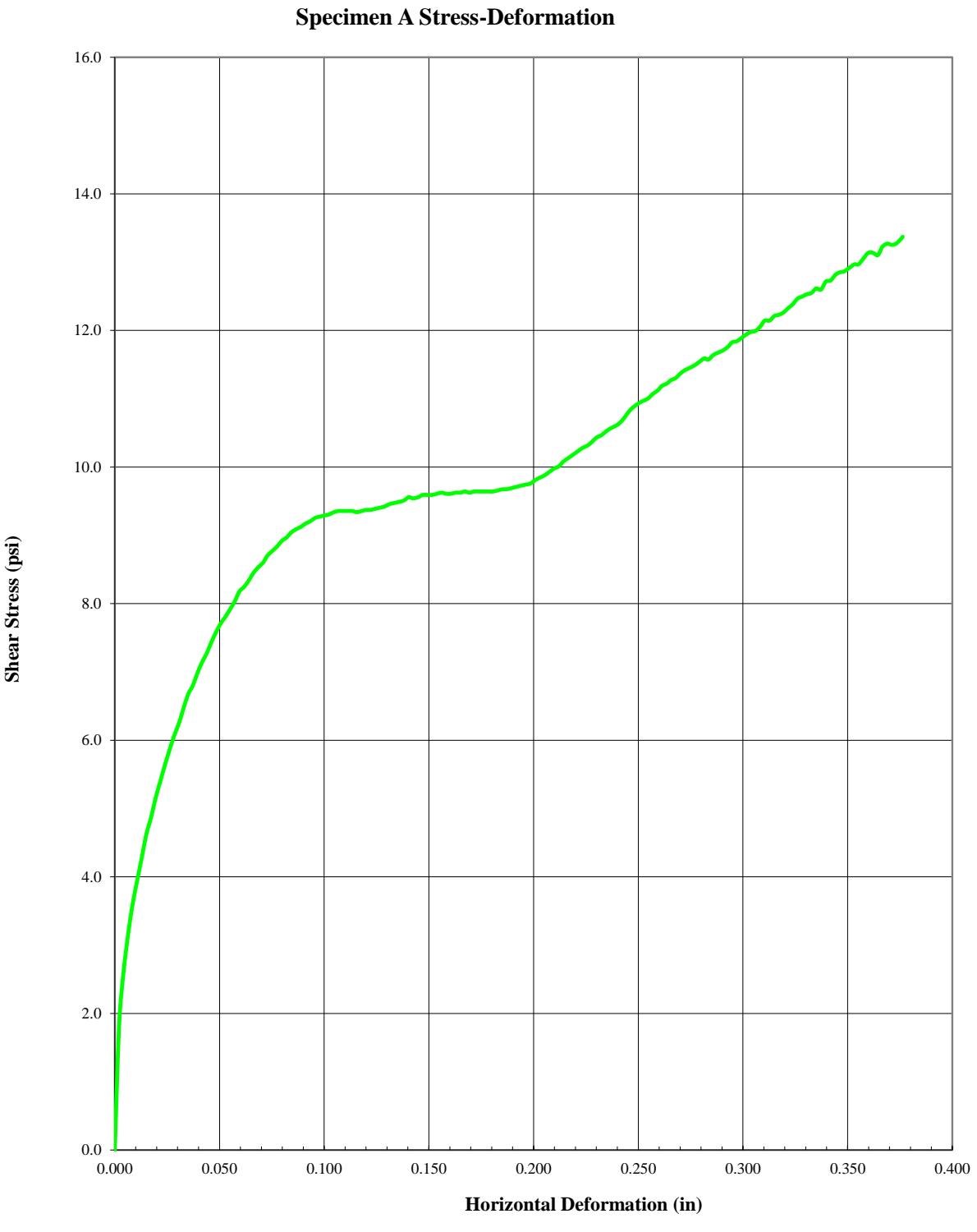
# Thompson Engineering

## Direct Shear Test (ASTM D3080)



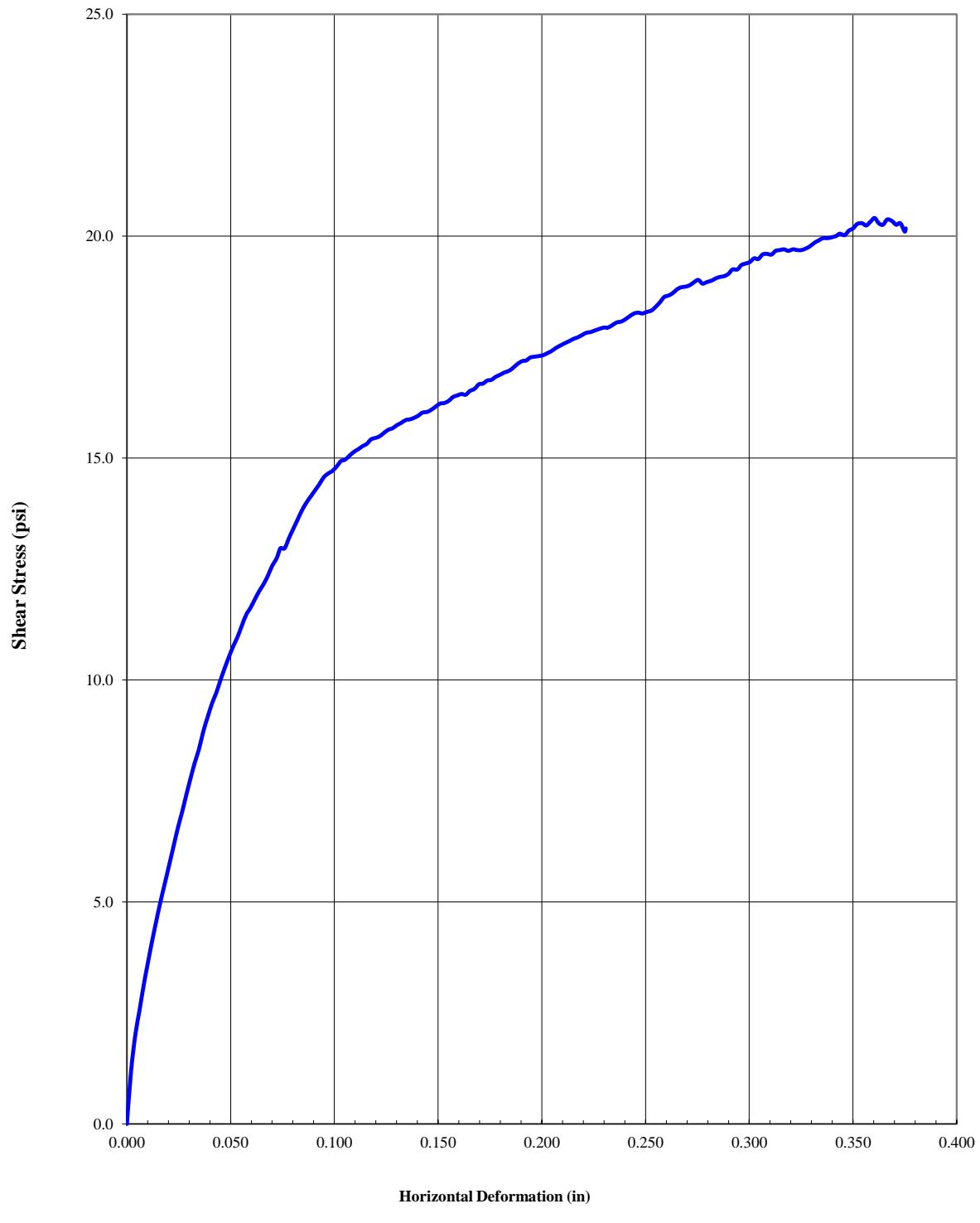


**Thompson Engineering**  
**Direct Shear Test**



**Thompson Engineering**  
**Direct Shear Test**

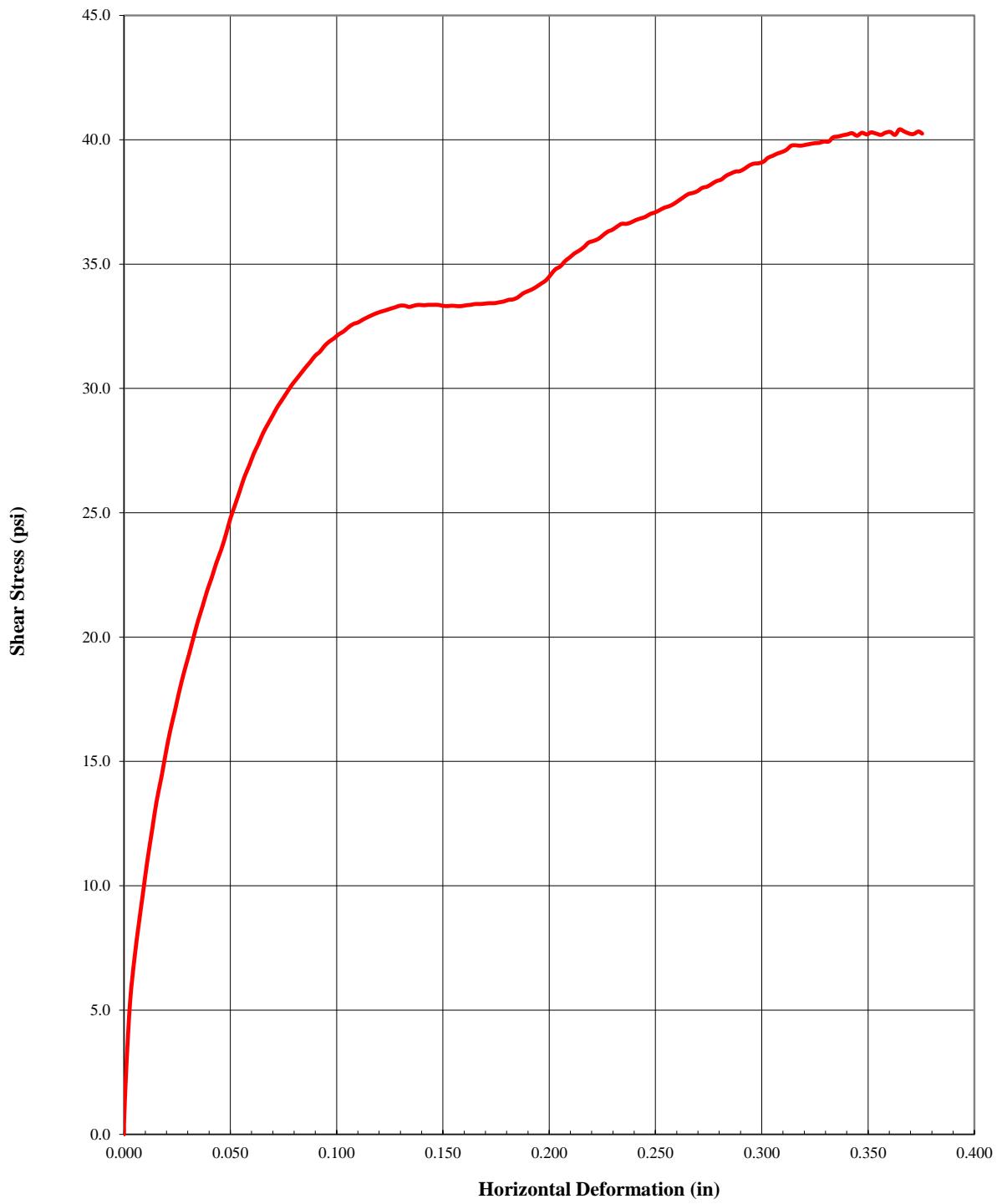
**Specimen B Stress-Deformation**



**Thompson Engineering**

**Direct Shear Test**

**Specimen C Stress-Deformation**



**Specimen Information**  
Direct Shear Test

**Thompson Engineering**

**Project Information**

Project: Mobile River Bridge

Location: Soils Lab

Project Number: 8203

Client: ALDOT

Sample Location: Soils Lab

Sample Number: TH-32

Boring Number: SB-5

Tested By: B. Hak

Reduced By: B. Hak

Checked By: C. Dugger

<b>Sample Description/Remarks</b>	
<b>Specimen A Description</b>	SILTY SAND (SM, A-2-4(0))
<b>Remarks</b>	
<b>Specimen B Description</b>	SILTY SAND (SM, A-2-4(0))
<b>Remarks</b>	
<b>Specimen C Description</b>	SILTY SAND (SM, A-2-4(0))
<b>Remarks</b>	
<b>Specimen D Description</b>	
<b>Remarks</b>	

**Moisture Density Data**

	Specimen A		Specimen B		Specimen C		Specimen D	
	Initial	Final	Initial	Final	Initial	Final	Initial	Final
<b>Height (in)</b>	1.000	0.962	1.000	0.941	1.000	0.932		
<b>Diameter (in)</b>	2.500	2.500	2.500	2.500	2.500	2.500		
<b>Total Wet Weight of Ring &amp; Soil (g)</b>	1196.97	1202.58	1182.16	1189.19	1194.94	1197.57		
<b>Weight of Ring (g)</b>	1040.08	1040.08	1039.00	1039.00	1040.26	1040.26		
<b>Wet Weight of Soil (g)</b>	156.89	162.50	143.16	150.19	154.68	157.31		
<b>Wt of Wet Soil &amp; Dish (g)</b>	-	208.04	-	222.02	-	201.38		
<b>Wt of Dry Soil &amp; Dish (g)</b>	-	190.65	-	198.72	-	185.75		
<b>Wt. Of Dish (g)</b>	-	128.07	-	128.74	-	123.31		

**Consolidation Calculations**

	Specimen A	Specimen B	Specimen C	Specimen D
<b>Initial Ref. Height (in)</b>	0.393	0.397	0.389	
<b>Final Ref. Height (in)</b>	0.355	0.338	0.321	
<b>Height after Consol (in)</b>	0.962	0.941	0.932	

**Calculations**

	Specimen A		Specimen B		Specimen C		Specimen D	
	Initial	Final	Initial	Final	Initial	Final	Initial	Final
<b>Specific Gravity</b>	2.600	2.600	2.600	2.600	2.600	2.600		
<b>Area (in<sup>2</sup>)</b>	4.909	4.909	4.909	4.909	4.909	4.909		
<b>Volume (in<sup>3</sup>)</b>	4.9	4.9	4.9	4.9	4.9	4.9		
<b>Moisture Content (%)</b>	32.910	27.788	29.986	33.295	29.459	25.032		
<b>Wet Density (pcf)</b>	121.757	126.111	111.102	116.558	120.042	122.083		
<b>Dry Density (pcf)</b>	91.609	98.687	85.472	87.443	92.726	97.642		
<b>Saturation (%)</b>	100.000	100.000	86.725	100.000	100.000	100.000		
<b>Void Ratio</b>	0.772	0.645	0.899	0.856	0.750	0.662		
<b>Porosity (%)</b>	43.559	36.821	47.340	42.754	42.871	35.441		

**Specimen A Shear Data**  
**Direct Shear Test**

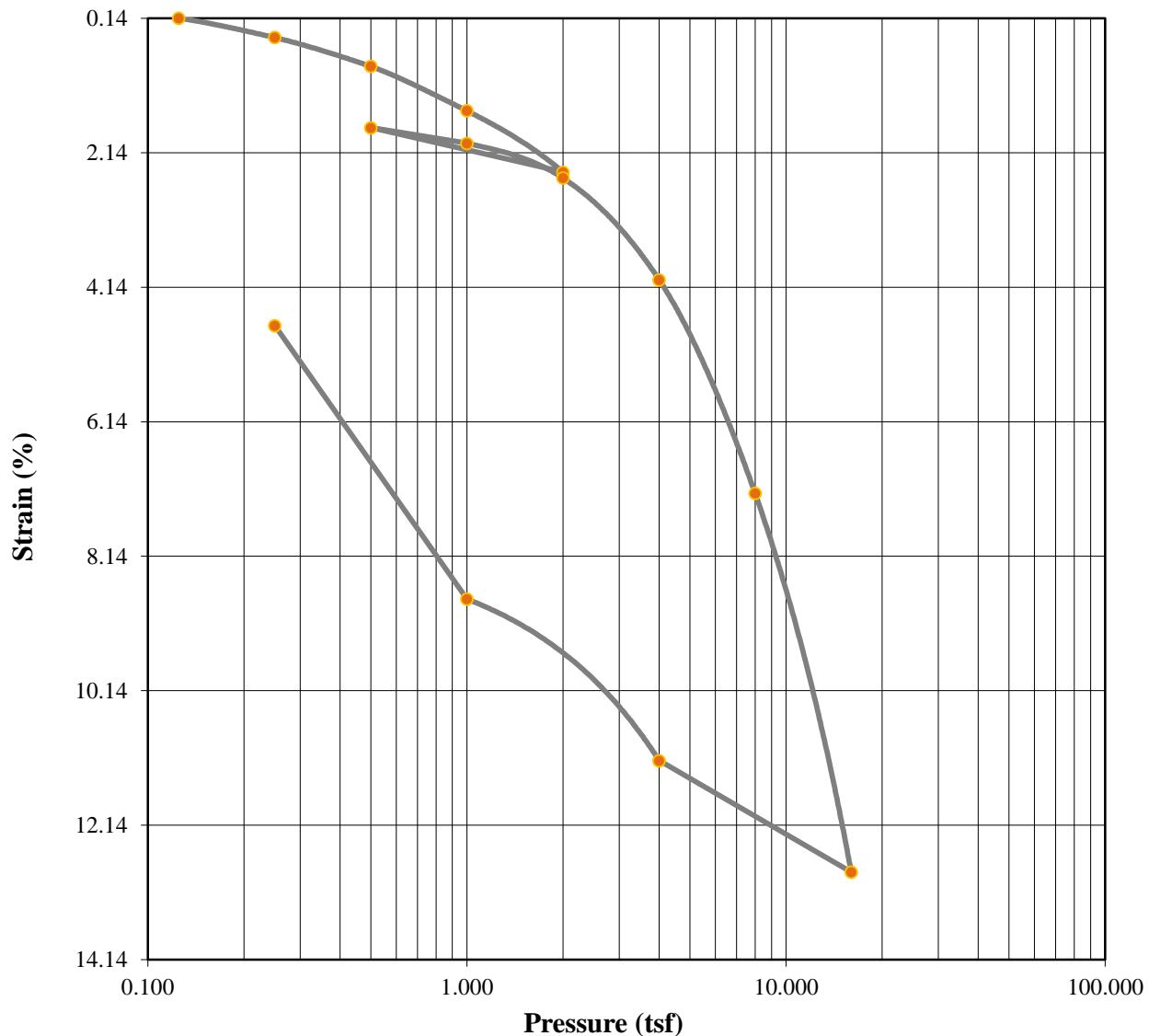
Thompson Engineering

File Location  
DS 17-1101-0145 SB-5 T-2.HSD

**Last Shear Pass**

Reading Number	Time	Shear Force (lbs)	Horizontal Deformation (in)	Vertical Deformation (in)	Axial Strain (%)	Stress (psi)
0	00:00:00	0.0	0.000	0.0000	0.000	0.0
1	00:00:15	8.9	0.002	-0.0002	0.081	1.8
2	00:00:30	12.6	0.004	-0.0007	0.162	2.6
3	00:00:45	15.5	0.006	-0.0012	0.254	3.2
4	00:01:00	17.6	0.008	-0.0016	0.335	3.6
5	00:01:15	19.4	0.011	-0.0021	0.428	3.9
6	00:01:30	21.1	0.013	-0.0025	0.520	4.3
7	00:01:45	22.7	0.015	-0.0029	0.601	4.6
8	00:02:00	23.9	0.017	-0.0032	0.694	4.9
9	00:02:15	25.2	0.019	-0.0035	0.775	5.1
10	00:02:30	26.5	0.022	-0.0038	0.867	5.4
11	00:02:45	27.7	0.024	-0.0040	0.960	5.6
12	00:03:00	28.7	0.026	-0.0043	1.040	5.8
13	00:03:15	29.8	0.028	-0.0045	1.133	6.1
14	00:03:30	30.7	0.031	-0.0047	1.225	6.2
15	00:03:45	31.7	0.033	-0.0049	1.306	6.5
16	00:04:00	32.7	0.035	-0.0049	1.399	6.7
17	00:04:15	33.4	0.037	-0.0051	1.491	6.8
18	00:04:30	34.2	0.039	-0.0052	1.572	7.0
19	00:04:45	35.0	0.042	-0.0052	1.665	7.1
20	00:05:00	35.7	0.044	-0.0052	1.757	7.3
21	00:05:15	36.4	0.046	-0.0053	1.838	7.4
22	00:05:30	37.2	0.048	-0.0053	1.931	7.6
23	00:05:45	37.8	0.051	-0.0053	2.023	7.7
24	00:06:00	38.3	0.053	-0.0053	2.116	7.8
25	00:06:15	38.8	0.055	-0.0053	2.197	7.9
26	00:06:30	39.4	0.057	-0.0053	2.289	8.0
27	00:06:45	40.2	0.060	-0.0053	2.382	8.2
28	00:07:00	40.5	0.062	-0.0053	2.474	8.2
29	00:07:15	41.0	0.064	-0.0053	2.566	8.3
30	00:07:30	41.5	0.066	-0.0052	2.647	8.4
31	00:07:45	41.9	0.068	-0.0052	2.740	8.5
32	00:08:00	42.2	0.071	-0.0052	2.832	8.6
33	00:08:15	42.7	0.073	-0.0051	2.913	8.7
34	00:08:30	43.0	0.075	-0.0050	3.006	8.8
35	00:08:45	43.4	0.077	-0.0049	3.098	8.8
36	00:09:00	43.8	0.080	-0.0049	3.191	8.9
37	00:09:15	44.0	0.082	-0.0048	3.283	9.0
38	00:09:30	44.4	0.084	-0.0046	3.364	9.0
39	00:09:45	44.6	0.086	-0.0046	3.457	9.1
40	00:10:00	44.8	0.089	-0.0044	3.549	9.1
41	00:10:15	45.0	0.091	-0.0043	3.642	9.2
42	00:10:30	45.2	0.093	-0.0043	3.734	9.2
43	00:10:45	45.4	0.096	-0.0041	3.827	9.3
44	00:11:00	45.5	0.098	-0.0040	3.908	9.3
45	00:11:15	45.6	0.100	-0.0038	4.000	9.3

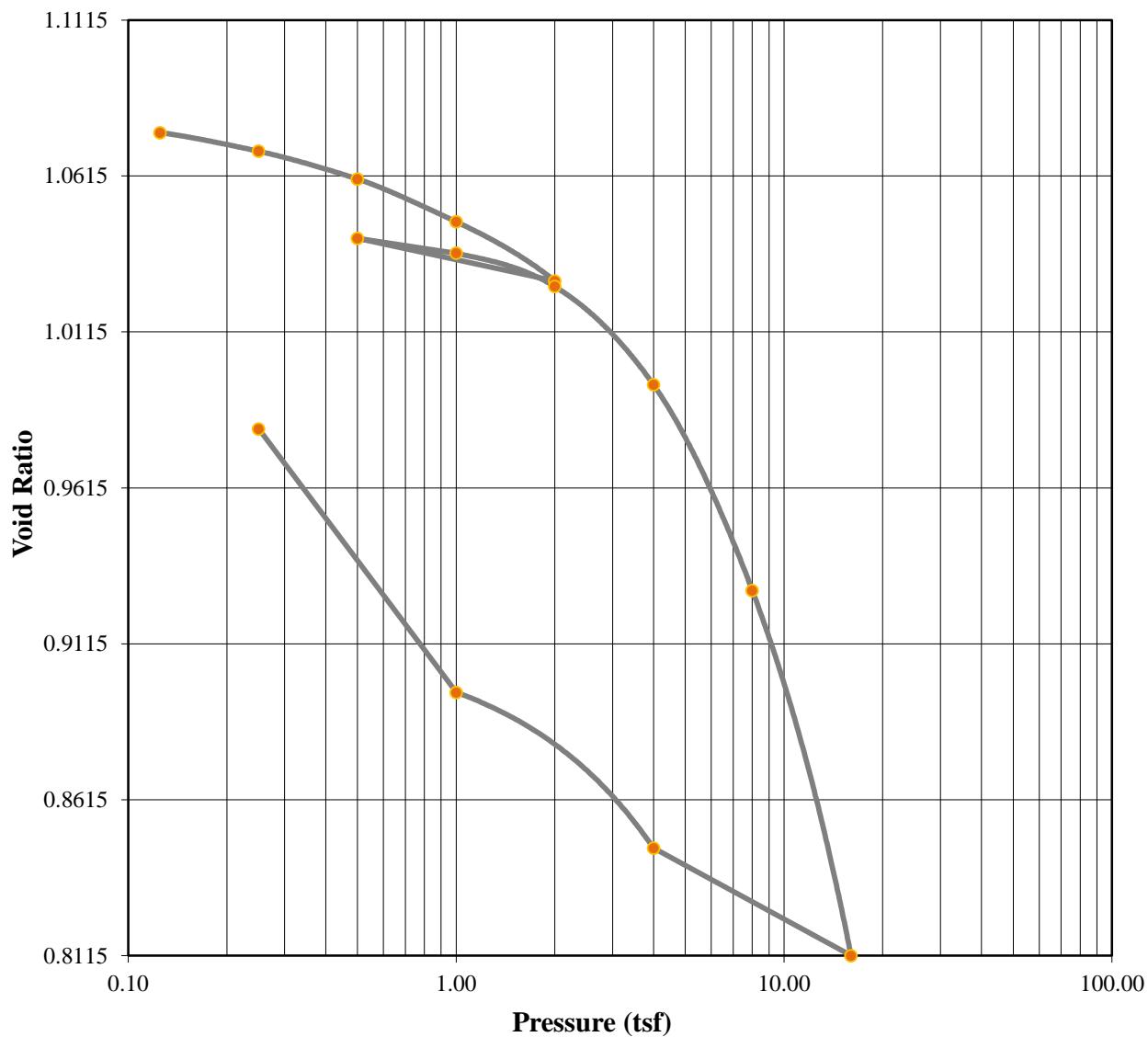
## Consolidation Test Test Results



Moisture (%):	Before	After	Liquid Limits:	0	Test Date:	6/5/18
Dry Density (pcf):	79.76	83.06	Plastic Limits:	0		
Saturation (%):	88.40	94.43	Plasticity Index (%):	0		
Void Ratio:	1.0779	0.9799	Specific Gravity:	2.660	Assumed	
Sample Description:	SILTY SAND (SM, A-4(0))					
Project Number:	8203		Depth:	23.5-25.5 ft.	Remarks:	
Sample Number:	T-2		Boring Number:	TH-31		
Project:	Mobile River Bridge					
Client:	ALDOT					
Location:	Soils Lab					

## Consolidation Test

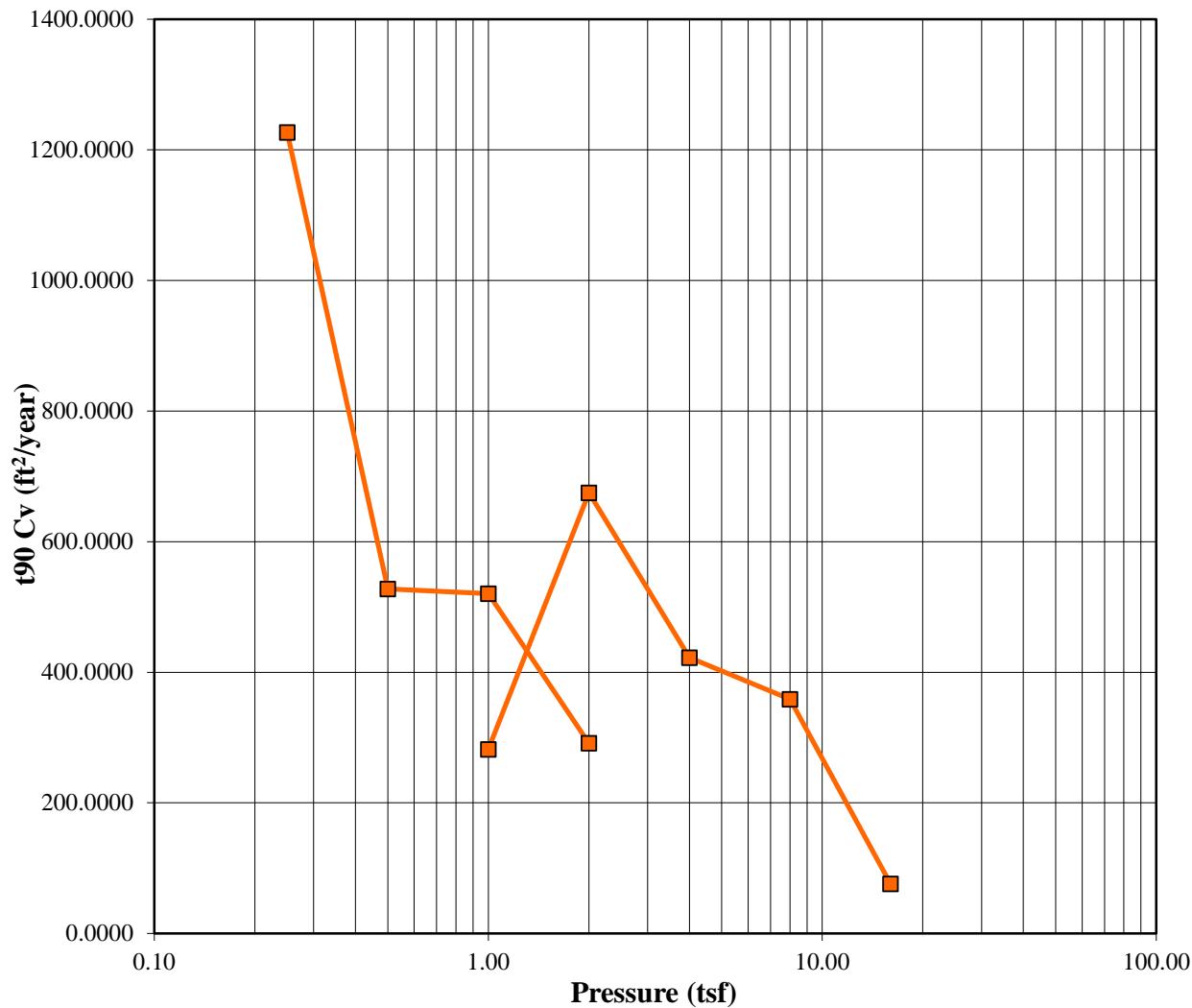
### Test Results



Moisture (%):	Before	After	Liquid Limits:	0	Test Date:	6/5/18
Dry Density (pcf):	79.76	83.06	Plastic Limits:	0		
Saturation (%):	88.40	94.43	Plasticity Index (%):	0		
Void Ratio:	1.0779	0.9799	Specific Gravity:	2.660	Assumed	
Soil Description:	SILTY SAND (SM, A-4(0))					
Project Number:	8203		Depth: 23.5-25.5 ft.		Remarks:	
Sample Number:	T-2		Boring Number: TH-31			
Project:	Mobile River Bridge					
Client:	ALDOT					
Location:	Soils Lab					

## Consolidation Test

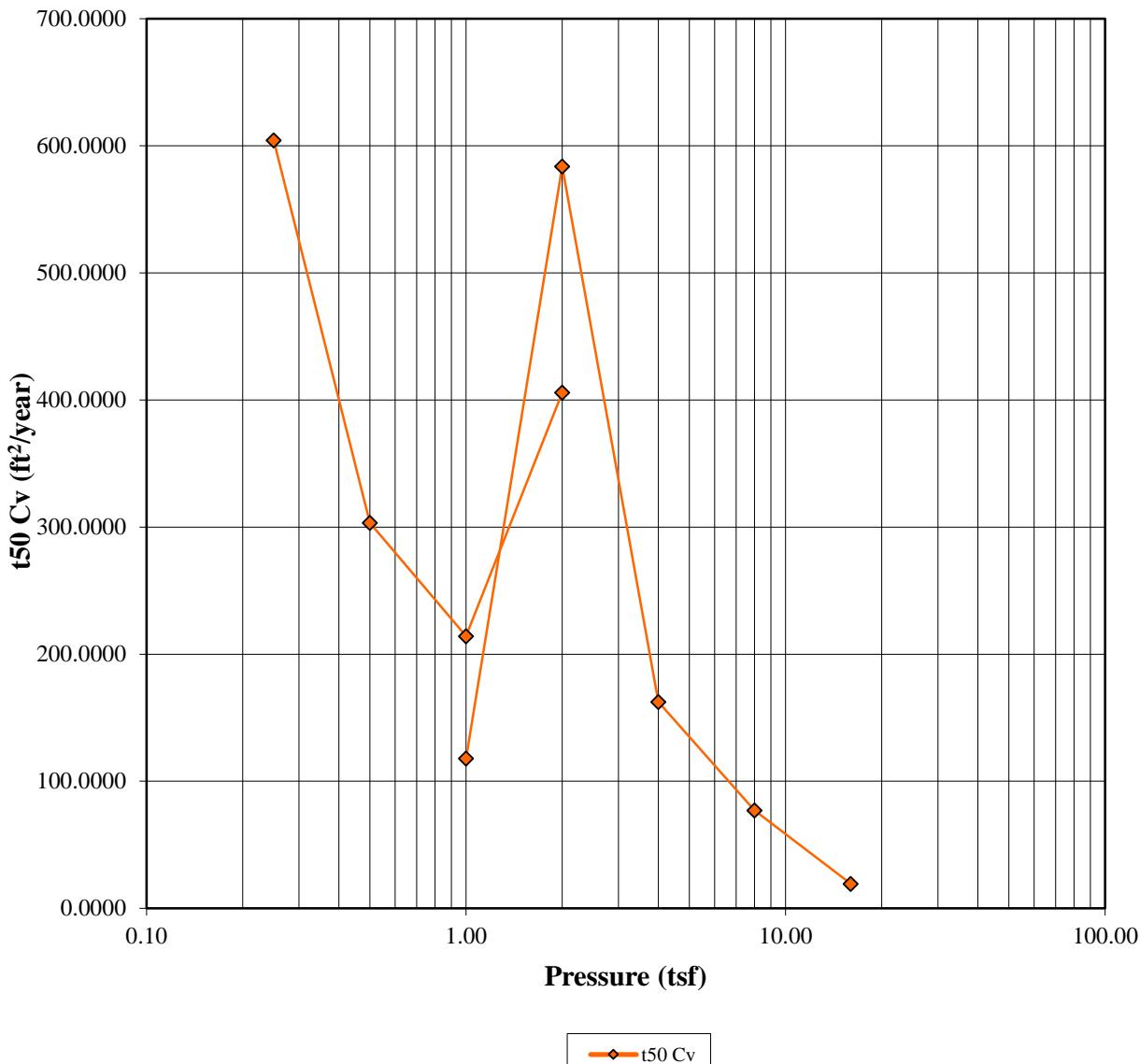
### Test Results



—■—  $t_{90} C_v$

Moisture (%):	Before	After	Liquid Limits:	0	Test Date:	6/5/18	
Dry Density (pcf):	79.76	83.06	Plastic Limits:	0			
Saturation (%):	88.40	94.43	Plasticity Index (%):	0			
Void Ratio:	1.0779	0.9799	Specific Gravity:	2.660	Assumed		
Soil Description:	SILTY SAND (SM, A-4(0))						
Project Number:	8203		Depth: 23.5-25.5 ft.		Remarks:		
Sample Number:	T-2		Boring Number: TH-31				
Project:	Mobile River Bridge						
Client:	ALDOT						
Location:	Soils Lab						

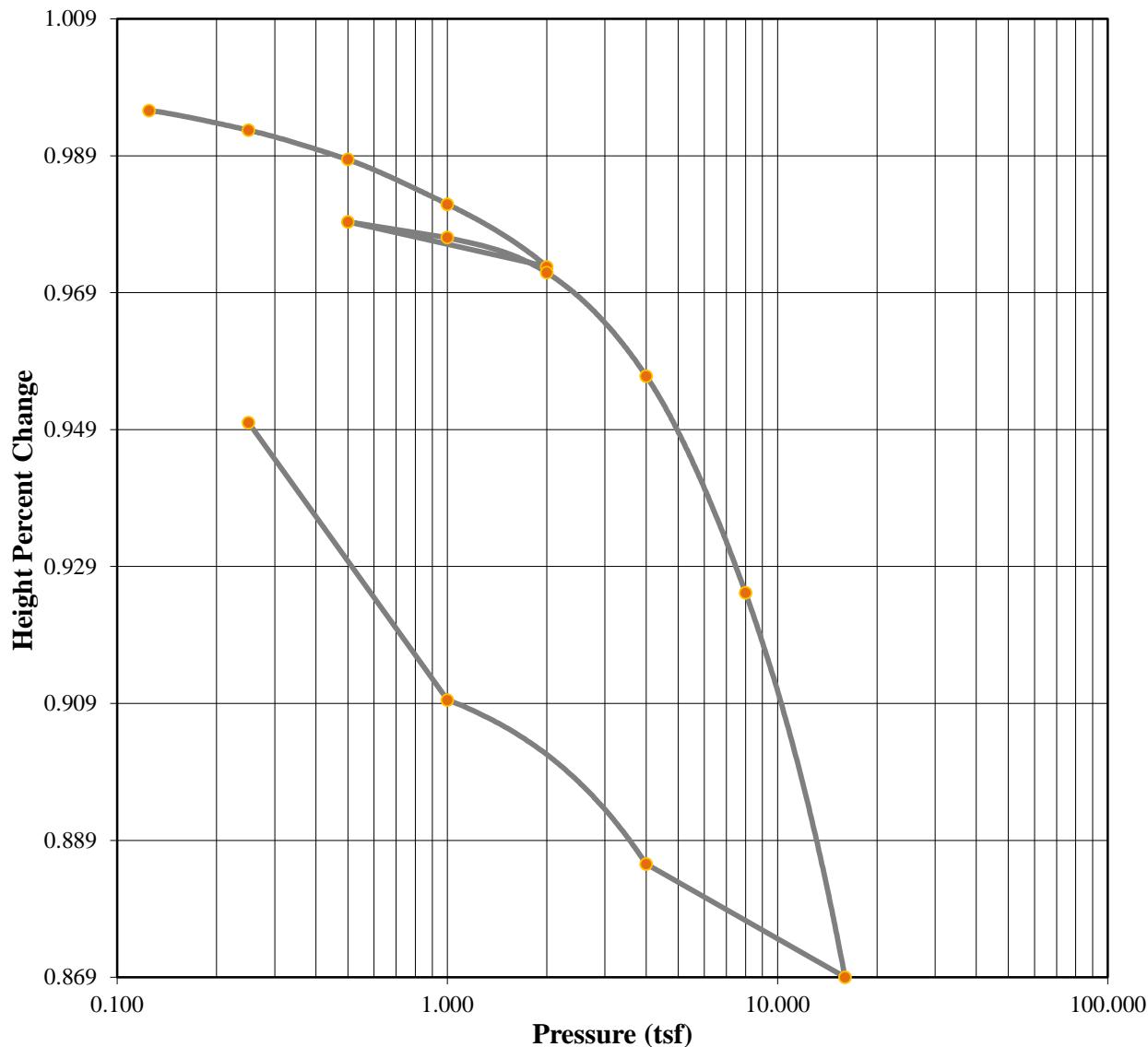
## Consolidation Test Test Results



Moisture (%):	Before	After	Liquid Limits:	0	Test Date:	6/5/18
Dry Density (pcf):	79.76	83.06	Plastic Limits:	0		
Saturation (%):	88.40	94.43	Plasticity Index (%):	0		
Void Ratio:	1.0779	0.9799	Specific Gravity:	2.660	Assumed	
Soil Description:	SILTY SAND (SM, A-4(0))					
Project Number:	8203		Depth: 23.5-25.5 ft.		Remarks:	
Sample Number:	T-2		Boring Number: TH-31			
Project:	Mobile River Bridge					
Client:	ALDOT					
Location:	Soils Lab					

## Consolidation Test

### Test Results



Moisture (%):	Before	After	Liquid Limits:	0	Test Date:	6/5/18	
Dry Density (pcf):	79.76	83.06	Plastic Limits:	0			
Saturation (%):	88.40	94.43	Plasticity Index (%):	0			
Void Ratio:	1.0779	0.9799	Specific Gravity:	2.660	Assumed		
Soil Description:	SILTY SAND (SM, A-4(0))						
Project Number:	8203		Depth: 23.5-25.5 ft.		Remarks:		
Sample Number:	T-2		Boring Number: TH-31				
Project:	Mobile River Bridge						
Client:	ALDOT						
Location:	Soils Lab						

## Consolidation Test Results

### Summary

**Project:** Mobile River Bridge  
**Location:** Soils Lab  
**Job Number:** 17-1101-0145

**Project Number:** 8203

**Sample Number:** T-2  
**Boring Number:** TH-31  
**Depth:** 23.5-25.5 ft.  
**Sample Type:** Undisturbed

**Sample Description:**  
SILTY SAND (SM, A-4(0))  
**Remarks:**

**Test Number:**  
**Test Date:** 6/5/18

Index	Load Sequence (tsf)	Cummulative Change in Height (in)	Specimen Height (in)	Height of Void (in)	Vertical Strain (%)	Void Ratio	t90 Fitting Time (min)	t50 Fitting Time (min)	t90 Cv (ft <sup>2</sup> /year)	t50 Cv (ft <sup>2</sup> /year)
0	0.000	0.0000	0.9970	0.5173	0.00	1.0783	0.000	0.000	0.000	0.000
1	0.125	0.0014	0.9956	0.5159	0.14	1.0754	0.000	0.000	0.000	0.000
2	0.250	0.0043	0.9927	0.5130	0.43	1.0694	0.622	0.293	1226.894	604.287
3	0.500	0.0086	0.9884	0.5087	0.86	1.0605	1.433	0.579	527.635	303.221
4	1.000	0.0151	0.9819	0.5022	1.52	1.0468	1.433	0.809	520.457	214.213
5	2.000	0.0242	0.9728	0.4931	2.43	1.0278	2.513	0.419	291.433	405.771
6	0.500	0.0177	0.9793	0.4996	1.77	1.0415	0.000	0.000	0.000	0.000
7	1.000	0.0200	0.9770	0.4973	2.00	1.0367	2.619	* 1.4549	282.072	117.948
8	2.000	0.0251	0.9719	0.4922	2.52	1.0260	1.083	0.291	675.007	583.842
9	4.000	0.0402	0.9568	0.4771	4.03	0.9945	1.678	1.014	422.154	162.359
10	8.000	0.0719	0.9251	0.4454	7.21	0.9286	1.847	1.999	358.604	76.986
11	16.000	0.1280	0.8690	0.3893	12.84	0.8115	7.671	7.028	76.176	19.313
12	4.000	0.1115	0.8855	0.4058	11.18	0.8459	0.000	0.000	0.000	0.000
13	1.000	0.0875	0.9095	0.4298	8.78	0.8959	0.000	0.000	0.000	0.000
14	0.250	0.0470	0.9500	0.4703	4.71	0.9804	0.000	0.000	0.000	0.000

Predicted value indicated with \*

**Tested By:** B. Hak

**Checked By:** C. Dugger



## Consolidation Test

### Consolidation Specimen Information

**Project:** Mobile River Bridge

**Project Number:** 8203

**Location:** Soils Lab

**Job Number:** 17-1101-0145

**Test Date:** 6/5/18

**Sample Number:**

T-2

**Sample Description:**

**Boring Number:**

TH-31

SILTY SAND (SM, A-4(0))

**Depth:**

23.5-25.5 ft.

**Remarks:**

**Sample Type:**

Undisturbed

**Test Number:**

**Liquid Limit:** 0.0000

**Initial Void Ratio:** 1.0779

**Initial Height (in):** 0.9970

**Plastic Limit:** 0.0000

**Plasticity Index (%):** 0.0000

**Initial Diameter (in):** 2.4960

**Specific Gravity:** 2.6600  
Assumed

**Weight of Ring (g):** 110.7200

Parameters	Initial Specimen	Final Specimen
Moist Weight + Container (g)	117.46	265.95
Dry Soil + Container (g)	94.98	230.09
Weight of Container (g)	32.47	129.00
Moisture Content (%)	35.96	35.47
Void Ratio	1.0779	0.9799
Saturation (%)	88.40	94.43
Dry Density (pcf)	79.76	83.06

**Tested By:** B. Hak

**Checked By:** C. Dugger

## Consolidation Test Results

**(Sequence 1) Load 0.125 tsf**

**Project:** Mobile River Bridge

**Project Number:** 8203

**Location:** Soils Lab

**Job Number:** 17-1101-0145

**Test Date:** 6/5/18

**Test Number:**

**Sample Number:** T-2

**Soil Description:**

**Boring Number:** SB-4

Gray Sandy Clay

**Depth:** 23.5-25.5 ft.

**Remarks:**

**Sample Type:** Undisturbed

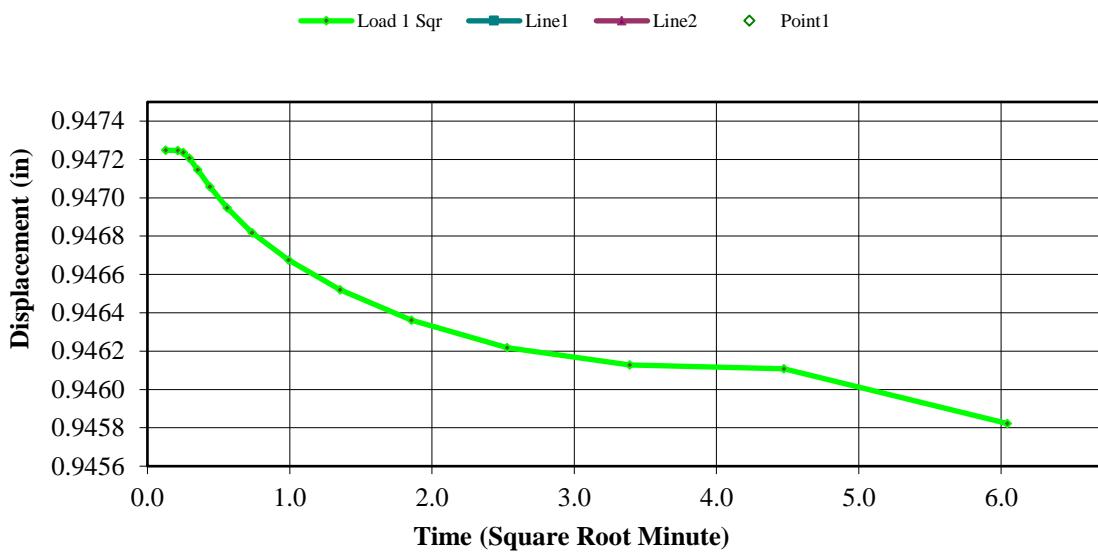
<b>Index</b>	<b>Time</b>	<b>Displacement (in)</b>	<b>Settlement (in)</b>	<b>Axial Strain (%)</b>	<b>Void Ratio</b>
0	00:00:00	0.9472	0.0000	0.0000	1.0779
1	00:00:01	0.9472	0.0000	0.0000	1.0779
2	00:00:02	0.9472	0.0000	0.0000	1.0779
3	00:00:03	0.9472	0.0000	0.0000	1.0779
4	00:00:04	0.9472	0.0000	0.0000	1.0779
5	00:00:05	0.9472	0.0000	0.0000	1.0779
6	00:00:06	0.9472	0.0000	0.0000	1.0779
7	00:00:12	0.9470	0.0003	0.0286	1.0773
8	00:00:15	0.9470	0.0003	0.0286	1.0773
9	00:00:30	0.9467	0.0006	0.0572	1.0767
10	00:01:00	0.9467	0.0006	0.0572	1.0767
11	00:02:00	0.9464	0.0009	0.0858	1.0761
12	00:05:01	0.9461	0.0011	0.1144	1.0755
13	00:10:01	0.9461	0.0011	0.1144	1.0755
14	00:20:01	0.9461	0.0011	0.1144	1.0755
15	00:36:32	0.9458	0.0014	0.1430	1.0749

**Tested By:**

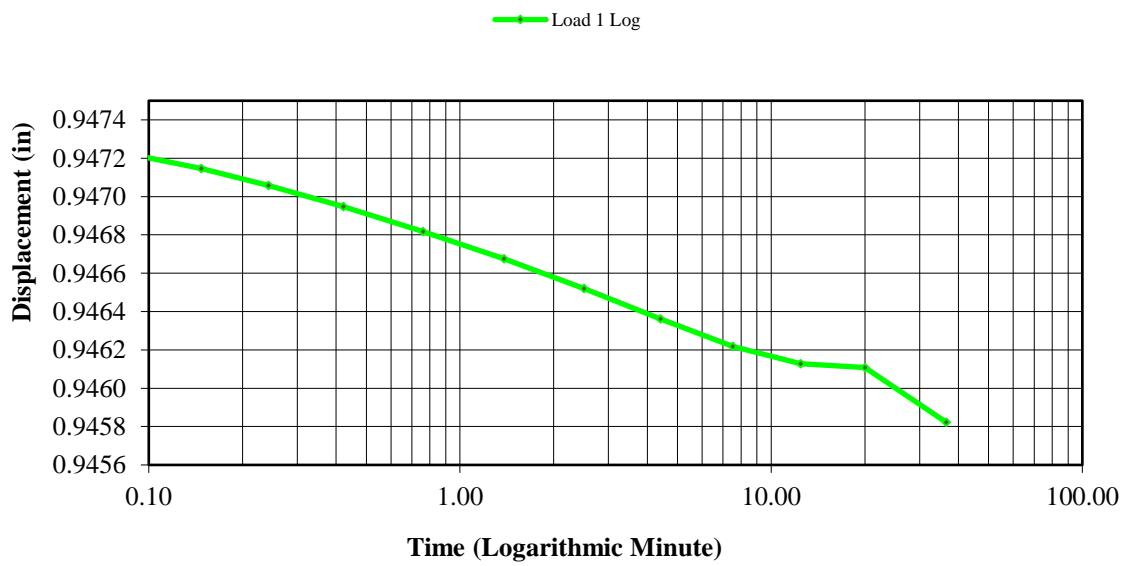
**Checked By:**

## Consolidation Test Results (Sequence 1) Load 0.125 tsf

**Consolidation Graph (Squareroot Time)**



**Consolidation Graph (Logarithmic Time)**



## **APPENDIX D**

- **Drill Rig Hammer Energy Report**



Dynamic  
Measurements  
and Analyses

## Job No. 179034-1

Report on: Standard Penetration Test Energy  
Measurements  
Chattanooga, TN

Prepared for Thompson Engineering  
By Thomas G. Hyatt and Joel S. Webster, E.I.  
June 28, 2017



June 28, 2017

Blake Ellis  
Thompson Engineering  
3707 Cottage Hill Road  
Mobile, AL 36609

**Re: Standard Penetration Test Energy Measurements**  
Chattanooga, TN  
GRL Job No. 179034-1

Dear Mr. Ellis,

This report presents results of energy measurements obtained on June 21, 2017 during Standard Penetration Tests (SPT) sampling. One automatic hammer mounted a Diedrich D-50 drill rig that was tested generally following ASTM D4633-10 standards. All dynamic tests were performed on NWJ drill rods. GRL Engineers, Inc. obtained the dynamic measurements with an instrumented NWJ subsection and a Model 8G Pile Driving Analyzer®. This report describes the testing procedures and summarizes the test results. Appendix A describes our measurement and analysis methods, Appendix B contains calibration information for the gages and equipment used, and Appendix C is a summary of the field data.

### **PURPOSE AND SCOPE OF WORK**

At the request of Thompson Engineering, GRL conducted SPT energy measurements in Chattanooga, TN generally following the ASTM D4633-10 recommendations. Specifically, we recorded SPT energy measurements at five-foot sample intervals between 13.5 and 40.0 feet below the existing ground surface. SPT samples were taken every five feet from the ground surface until a boring depth of about 40.0 feet was reached. All SPT samples were driven for a total of 3 six-inch increments, or 1.5 feet.

### **EQUIPMENT**

#### ***Drilling and SPT Hammer Equipment***

##### **Diedrich D-50 (Serial # 310)**

SPT energy measurements were made on an automatic hammer mounted on a Diedrich D-50 drill rig. The drilling method used to advance the boring was hollow stem auger. Energy measurements for this drill rig were collected at a borehole located in Chattanooga, TN. SPT energy measurements were performed at 5-foot sampling intervals between 13.5 and 40.0 feet. A total of six energy measurement events were performed for this drill rig.

### ***Instrumentation***

A Model 8G Pile Driving Analyzer (PDA) data acquisition system (SN# 4613LE) was used to collect and process the dynamic measurements of force and velocity. The data was collected using a two foot long section of NWJ rod subsection (SN# 231NWJ) with a cross sectional area of 1.46 square inches and instrumented with two full bridge foil resistance strain gages and two piezoresistive accelerometers mounted in the midpoint location of the instrumented rod.

Analog signals from the strain gages and accelerometers were conditioned, digitized, stored and processed with the PDA. The sampling frequency used during the SPT testing was 50 kHz. Selected output from the PDA for each recorded impact included the energy transfer ratio (ETR), maximum rod top velocity (VMX), maximum energy transfer (EFV), maximum rod top force (FMX), and the hammer operating rate (BPM).

## **MEASUREMENTS AND CALCULATIONS**

### ***FV Method (EFV)***

Energy transfer to the PDA gage location, E<sub>FV</sub>, was computed by the PDA using force, F(t), and velocity, v(t), records as follows:

$$EFV = \int_a^b F(t) \cdot v(t) dt$$

The time "a" corresponds to the start of the record when the energy transfer begins, and "b" is the time at which energy transferred to the rod reaches a maximum value. The FV Method is currently recognized in ASTM D4633-10, and is the theoretically correct result; therefore, no other energy calculation methods are reported.

### **Corrected SPT number (N<sub>60</sub>)**

While the primary purpose of SPT energy testing is to calculate the maximum transferred energy (ETR) of each hammer blow, the overall average E<sub>FV</sub> value can be used to calculate the corrected SPT number (N<sub>60</sub>). To adjust the SPT N-values for hammer performance, the following correction as suggested by Seed for N-value adjustment to 60% transfer efficiency (e.g. 210 ft-pounds) was used:

$$N_{60} = \left( \frac{E_m}{210} \right) N_m$$

Where:

N<sub>60</sub> = Corrected N-value

E<sub>m</sub> = overall average measured energy transfer (EFV)

N<sub>m</sub> = number of blows for last 12 inches of sampler penetration

A general introduction to dynamic SPT testing methods is included in this report as Appendix A. References for more detailed descriptions of our testing and analysis methods are available upon request.

Any cross-sectional area difference between the GRL rod subsection and the drill rods, any loose connections or changes in area at section joints, or any cross-sectional area differences between the individual drill rod sections will result in stress wave reflections that can potentially influence the energy transfer. The EFV transferred energy calculation method, utilizing both force and velocity records, is theoretically correct and gives energy transfer results that are not adversely affected by cross-sectional area changes or loose connectors. The EFV results are included in Appendix C for all records collected and accepted after checking them for consistency.

## **RESULTS**

Upon return to the office, the records collected by the PDA were checked for consistency and accuracy. For example, records from very weak startup or final impacts were not included in average results. Appendix C contains a representative plot of force and normalized velocity versus time, as well as tables of PDA results for all hammer blows at each dynamically monitored sampling depth. The results include the EFV (transferred energy by the FV method, as recommended by ASTM D4633-10), ETR (energy transfer efficiency for the EFV method), BPM (hammer operating rate), FMX (maximum rod top force) and VMX (maximum rod top velocity). The tables show statistical summaries for the final two 6 inch increments over which the SPT N value is calculated. At the end of each table is a statistical evaluation of these results which include the average and standard deviation.

The table below and the summary tables in Appendix C summarize the average transferred energy values calculated by the EFV method. The records consist of averaged hammer blows from the last 12 inches (i.e. N value) at each dynamically monitored sampling depth. The “energy transfer ratio” (ETR) is defined as the ratio of maximum transferred energy EFV divided by the theoretical hammer potential energy of 350 ft-lbs (i.e., computed per the 140 lb SPT hammer and the standard 30 inch drop as specified by ASTM D1586-08). The average hammer operating rate is reported in blows per minute (BPM). A summary of the dynamic measurements of the energy transfer to the drill rods using the EFV equation is provided in the table below.

Drill Rig	Avg. EFV (ft-lbs)	Avg ETR (%)	Range of EFV (ft-lbs)	Range of ETR (%)
Diedrich D-50 SN 310	329	94	299 – 357	86 – 102

## **CONCLUSIONS**

Based upon the dynamic test data obtained, the following conclusions are presented:

1. Loose connections in the drill string were sometimes observed in the force and velocity records. However, energy transfer values calculated using the EFV equation are not adversely affected by the connectors and therefore are considered a better indication of transferred energy.
2. Dynamic measurements of the transferred energy to the drill rods using the EFV equation ranged from 299 to 357 ft-lbs for the Diedrich D-50, SN 310 drill rig. This corresponds to a transfer efficiency ranging from 86 to 102% of the SPT hammer energy of 350 ft-lbs.
3. The average transferred energy (EFV) and energy transfer ratio (ETR) for the Diedrich D-50 drill rig tested was as follows:

Diedrich D-50, SN 310: Average EFV = 329 ft-lbs; Average ETR = 94%

Please review both ASTM D4633-10 and ASTM D1586-08 prior to applying these test results. The energy calibrations reported herein are valid for the same hammer/drill rig, with the same drill operator, same anvil dimensions, and same drilling methods.

We appreciate the opportunity to be of assistance to you on this project. Please contact our office should you have any questions regarding this submittal, require additional information, or if we may be of further service.

Sincerely,

GRL Engineers, Inc.



Joel S. Webster, E.I.



Thomas G. Hyatt

TGH:JSW:dms

## **Appendix A**

***An Introduction into SPT Dynamic Pile Testing***

## APPENDIX A

### AN INTRODUCTION INTO SPT DYNAMIC PILE TESTING

The following has been written by GRL Engineers, Inc. and may only be copied with its written permission.

#### 1. BACKGROUND

The Standard Penetration Test is frequently conducted as an in-situ assessment of soil strength. This test requires that a 140 lb weight is dropped 30 inches onto a drive rod at whose bottom a sampler is usually installed. The sampler is driven for 18 inches; the number of blows required for the last 12 inches of driving is the so-called N-value. The N-value may be used as a strength indicator for foundation design or as a means of assessing the liquefaction potential of soils.

Obviously, the SPT hammer efficiency is an important consideration when using the N-values for design purposes. Measurements have indicated that the energy in the drive rod is sometimes only 30% and may reach 90% of the potential or rated energy of the SPT hammer ( $E_{\text{rated}} = 0.35 \text{ kip-ft}$  or  $0.475 \text{ kJ}$ ). The type of hammer used to drive the rod is the main reason for these variations. On the average, the energy in the drive rod is 60% of the standard rated energy.

Because of the variability of energy, methods based on N-values are considered unreliable. However, measurements during SPT testing using the Case Method can be done on a routine basis and these measurements yield the transferred energy values. With measured energy,  $EM_x$ , known, an adjustment of the measured N-value,  $N_m$ , can be made as follows.

$$N_{60} = N_m [E_m / (0.6E_r)] \quad (1)$$

Thus, if the measured energy value is equal to the normally expected transferred energy of 60% of  $E_{\text{rated}}$  then the adjusted and measured N-values are identical. On the other hand, if the measured energy is only 30% then the adjusted blow count will be reduced by 50%.

#### 2. DYNAMIC TESTING AND ANALYSIS METHODS APPLIED TO SPT

The Case Method of dynamic pile testing, named after the Case Institute of Technology where it was

developed between 1964 and 1975, requires that a substantial ram mass (e.g. a pile driving hammer) impacts the pile top such that the pile undergoes at least a small permanent set. Thus, the method is also referred to as a "High Strain Method". The Case Method requires dynamic measurements on the pile or shaft under the ram impact and then a calculation of various quantities. Conveniently, for SPT applications, the measurements and analyses are done by a single piece of equipment: the SPT Analyzer. The Pile Driving Analyzer® (PDA) is also suitable to perform these measurements and data processing.

A related analysis method is the "Wave Equation Analysis" which calculates a relationship between bearing capacity, pile stresses, transferred energy and field blow count. The GRLWEAP™ program performs this analysis and provides a complete set of helpful information and input data. This program can be used very effectively to simulate the SPT driving process.

#### 3. MEASUREMENTS

GRL uses equipment manufactured by Pile Dynamics, Inc. The system includes either an SPT-Analyzer™ (SPTA) or a Pile Driving Analyzer® (PDA), an instrumented rod section and two accelerometers. SPT energy testing is very closely related to and borrows procedures from dynamic pile testing. Those interested in the basis of the SPT energy testing method may obtain extensive literature on dynamic pile testing from GRL Engineers, Inc.

##### 3.1 SPT Analyzer or Pile Driving Analyzer

The basis for the results calculated by the SPTA or PDA are strain and acceleration measured in an instrumented rod section. These signals are converted to rod top force,  $F(t)$ , and rod top velocity,  $v(t)$ . The SPTA or PDA conditions, calibrates and displays these signals and immediately computes average pile force and velocity thereby eliminating bending effects. The product of these two

measurements is then integrated over time which yields the energy transferred to the instrumented section as a function of time (see Section 4.1).

For convenience and accuracy, strain measurements are usually taken on an instrumented section of SPT drive rod. Ideally, the section properties of the instrumented rod and those of the drive rod are the same, however, using subs, other sections can also be utilized.

For the instrumented section, PDI provides a force calibration in such a way that the output of the instrumented rod is directly calculated without the need for an accurate elastic modulus or cross sectional area of the rod section.

The acceleration measurements are often demanding in the SPT environment, because of high frequency and high acceleration motion components. An experienced measurement engineer, therefore, has to evaluate the quality of this data before final conclusions are drawn from the numerical results calculated by SPTA or PDA.

SPTA or PDA records are taken while the standard N-value is acquired in the conventional manner. This then allows a direct correlation between N-value and average transferred energy.

### **3.2 HPA**

The SPT hammer's ram velocity may be directly obtained using radar technology in the Hammer Performance Analyzer™. The impact velocity results can be automatically processed with a PC or recorded on a strip chart. HPA measurements yield a hammer kinetic energy, but not the energy transferred to the drive rod.

## **4 RECORD EVALUATION BY SPTA OR PDA**

### **4.1 HAMMER PERFORMANCE**

The PDA calculates the energy transferred to the pile top from:

$$E(t) = \int_0^t F(\tau)v(\tau) d\tau \quad (2)$$

The maximum of the  $E(t)$  curve is often called **ENTHRU** or **EMX**; it is the most important quantity for an overall evaluation of the performance of a hammer

and driving system. **EMX** allows for a classification of the hammer's performance when presented as,  $e_T$ , the rated transfer efficiency, also called energy transfer ratio (**ETR**) or global efficiency.

$$e_T = EMX/E_R \quad (3)$$

where  $E_R$  is the hammer manufacturer's rated energy value or 0.35 kip-ft (0.475 kJ) in the case of the SPT hammer.

Often in the SPT literature one finds also reference to the EF2 energy. This evaluation is based on assumed proportionality between force and velocity (see also Section 5):

$$v(t) = F(t) / Z \quad (4)$$

where  $Z = EA/c$  is the pile impedance, E is the elastic modulus, A is the cross sectional area and c is the speed of the stress wave in the pile material..

Combining equations 2 and 4 leads to

$$EF(t) = \int_0^t F(\tau)^2 / Z d\tau \quad (5)$$

The EF2 transferred energy value is the EF-value at the time  $t = 2L/c$ , where L is the drive rod length and c is the stress wave speed in steel (16,800 ft/s or 5,124 m/s). Since the force is easier to measure than both force and velocity, Equation 5 is preferred by some test engineers. However, the EF method is fraught with errors and certain correction factors have to be applied to make it approximately correct. Among the error sources are the following:

- Proportionality is often violated prior to time  $2L/c$ . The proportionality between force and velocity in a downward traveling wave only holds if the wave does not encounter a disturbance prior to reflecting off the pile toe. Such disturbances include a change in cross sectional area, an open or loose splice or joint, or resistance along the shaft.
- Using only one force measurement precludes a data quality check based on the proportionality between force and velocity. Thus, a force measurement that is for some reason in error may not be detectable, which will lead to errors in the EF2 value. Data quality checks will be discussed further in Section 5.

The use of EF2 is therefore not recommended but it is often included in result presentations for the sake of completeness.

#### 4.2 STRESSES

During SPT monitoring, it is also of interest to monitor compressive stresses at both the top of the drive rod and at its bottom.

At the pile top (location of sensors) the maximum compression stress averaged over the rod's cross section, **CSX**, is directly obtained from the measurements. Note that this stress value refers to the instrumented section. If the rod has a different cross sectional area then the stress in the rod will be different from CSX.

The SPTA or PDA can also calculate, in an approximate manner, the force at the rod bottom, **CFB**. To obtain the corresponding stress, this force value should be divided by the appropriate cross sectional area, e.g. by the rod area just above the sampler or by the sampler area itself. Of course, non-uniform stress components as they might occur at the sampler tip due to a sloping rock are not considered in this calculation.

#### 5. DATA QUALITY CHECKS

Quality data is the first and foremost requirement for accurate dynamic testing results. It is therefore important that the measurement engineer performing SPTA or PDA tests has the experience necessary to recognize measurement problems and take appropriate corrective action should problems develop. Fortunately, dynamic pile testing allows for certain data quality checks because two independent measurements are taken that have to conform to the so-called proportionality relationship.

As long as there is only a wave traveling in one direction, as is the case during impact when only a downward traveling wave exists in the rod, force and velocity measured at its top are proportional

$$F = v Z \quad (5)$$

where Z is again the pile impedance,  $Z = EA/c$ . This relationship can also be expressed in terms of stress

$$\sigma = F/A = v (E/c) \quad (6)$$

or strain

$$\epsilon = \sigma/E = v / c \quad (7)$$

This means that the early portion of strain times wave speed must be equal to the velocity unless the proportionality is affected by high friction near the pile top or by a pile cross sectional change not far below the sensors. Checking the proportionality is an excellent means of assuring meaningful measurements but is only truly meaningful for perfectly uniform rods. Open or loose splices, for example, will lead to a non-proportionality. For SPT rods it is fortunate that usually no soil resistance acts along the shaft and for that reason, proportionality can exist until the stress wave returns from sampler top or rod bottom unless connectors are not sufficiently tightened or have a significant mass.

Velocity data quality can also be checked by looking at the final displacement, DFN, which is calculated from the acceleration by double integration. If the calculated final displacement is much higher or lower than indicated by the N-value, the accelerometer attachment may be loose or the sensor may be faulty. If major drift in the velocity is observed, the EMX value may be in error, even though proportionality from impact to time  $2L/c$  exists. In this case, it may be useful to evaluate the energy transferred to the drill rod at time  $2L/c$ , which is calculated by the PDA or SPTA as the E2E quantity.

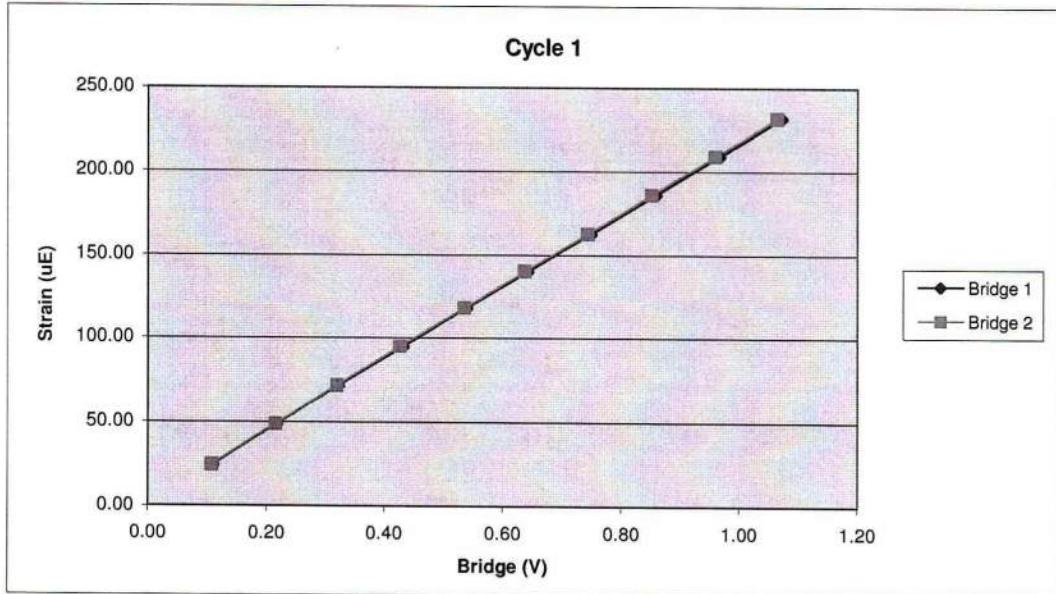
## **APPENDIX B**

### **Instrumentation Calibration Information**

231NWJ		Cycle 1		
Sample	Force (lb)	Strain ( $\mu\text{E}$ )	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1012.13	24.71	0.11	0.11
3	2008.29	48.73	0.22	0.22
4	2984.34	71.57	0.32	0.32
5	3989.18	95.13	0.43	0.43
6	4994.80	117.95	0.54	0.54
7	5955.87	139.98	0.64	0.64
8	6944.74	162.72	0.75	0.74
9	7955.89	186.14	0.86	0.85
10	8962.89	209.00	0.97	0.96
11	9948.41	231.79	1.07	1.06

Bridge 1	Bridge 2
Force Calibration (lb/V)	9283.84
Offset	-6.70
Correlation	0.999999
Strain Calibration ( $\mu\text{E}/\text{V}$ )	214.44
Offset	2.14
Correlation	0.999981
Force Calibration (lb/V)	9345.66
Offset	-0.19
Correlation	0.999999
Strain Calibration ( $\mu\text{E}/\text{V}$ )	215.86
Offset	2.29
Correlation	0.999982

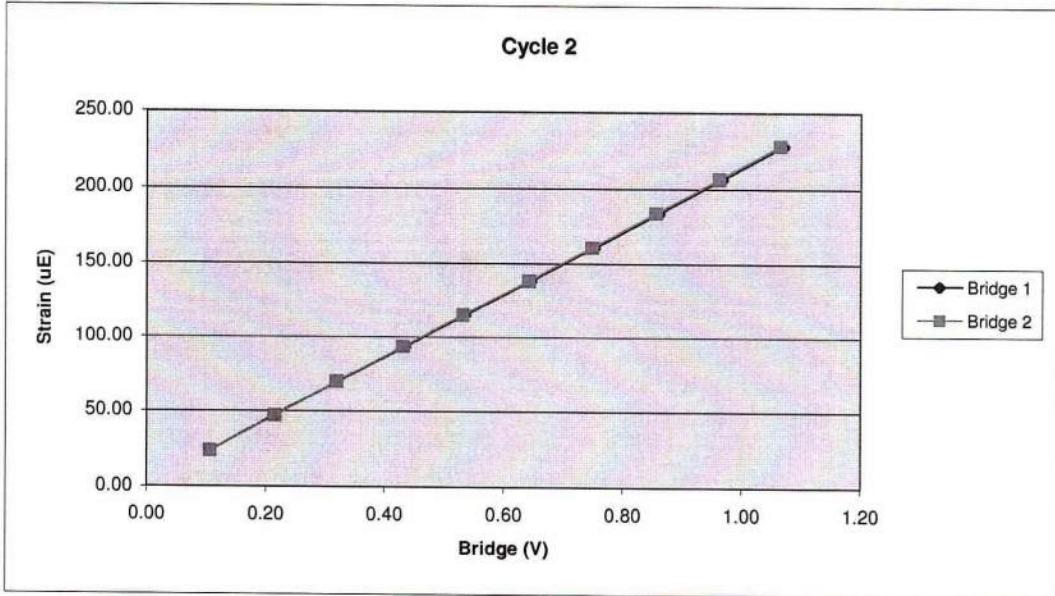
Force Strain Calibration	
EA (Kips)	43292.53
Offset	-99.16
Correlation	0.999979



231NWJ		Cycle 2		
Sample	Force (lb)	Strain ( $\mu\text{E}$ )	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	976.64	23.62	0.11	0.11
3	1976.95	47.01	0.21	0.22
4	2948.66	69.69	0.32	0.32
5	3992.73	93.38	0.43	0.43
6	4928.56	115.08	0.53	0.53
7	5953.31	138.50	0.64	0.64
8	6923.84	160.74	0.75	0.75
9	7942.09	183.61	0.86	0.85
10	8927.21	206.62	0.97	0.96
11	9887.09	228.02	1.07	1.06

Bridge 1		Bridge 2	
Force Calibration (lb/V)	9250.68	Force Calibration (lb/V)	9301.08
Offset	-9.91	Offset	-18.55
Correlation	0.999998	Correlation	0.999998
Strain Calibration ( $\mu\text{E}/\text{V}$ )	212.11	Strain Calibration ( $\mu\text{E}/\text{V}$ )	213.27
Offset	1.53	Offset	1.33
Correlation	0.999994	Correlation	0.999994

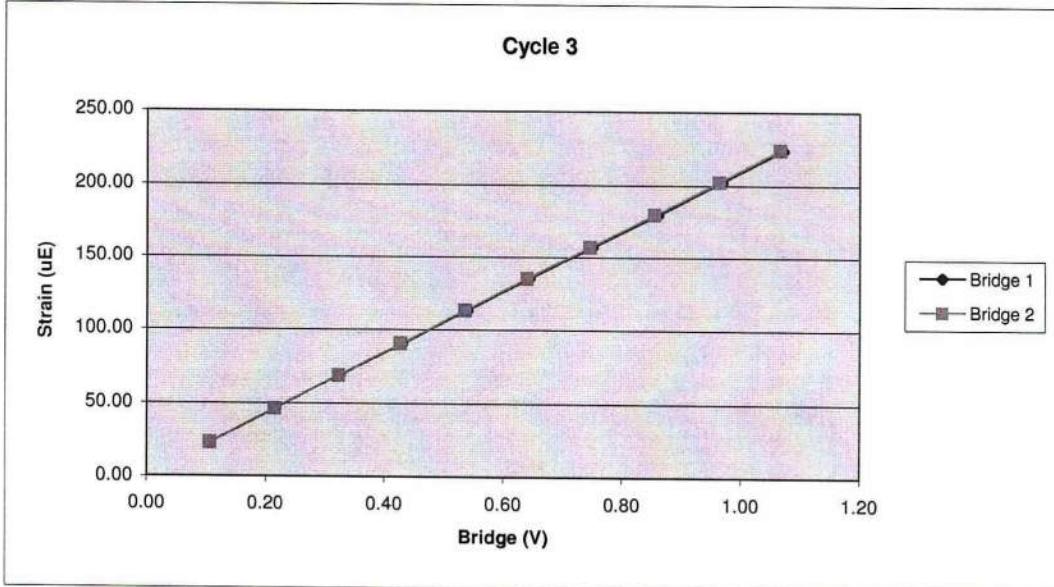
Force Strain Calibration	
EA (Kips)	43611.25
Offset	-76.62
Correlation	0.999990



231NWJ		Cycle 3		
Sample	Force (lb)	Strain ( $\mu\text{E}$ )	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	976.05	22.97	0.11	0.11
3	1980.69	46.32	0.21	0.21
4	2977.64	68.91	0.32	0.32
5	3954.48	90.43	0.43	0.43
6	4961.09	113.14	0.54	0.54
7	5931.03	135.05	0.64	0.64
8	6916.55	156.82	0.75	0.74
9	7928.09	179.47	0.86	0.85
10	8932.14	202.49	0.97	0.96
11	9894.98	224.03	1.07	1.07

Bridge 1		Bridge 2	
Force Calibration (lb/V)	9251.71	Force Calibration (lb/V)	9303.81
Offset	-8.61	Offset	-17.09
Correlation	0.999998	Correlation	0.999998
Strain Calibration ( $\mu\text{E}/\text{V}$ )	208.00	Strain Calibration ( $\mu\text{E}/\text{V}$ )	209.17
Offset	1.35	Offset	1.16
Correlation	0.999992	Correlation	0.999996

Force Strain Calibration	
EA (Kips)	44479.19
Offset	-68.49
Correlation	0.999991



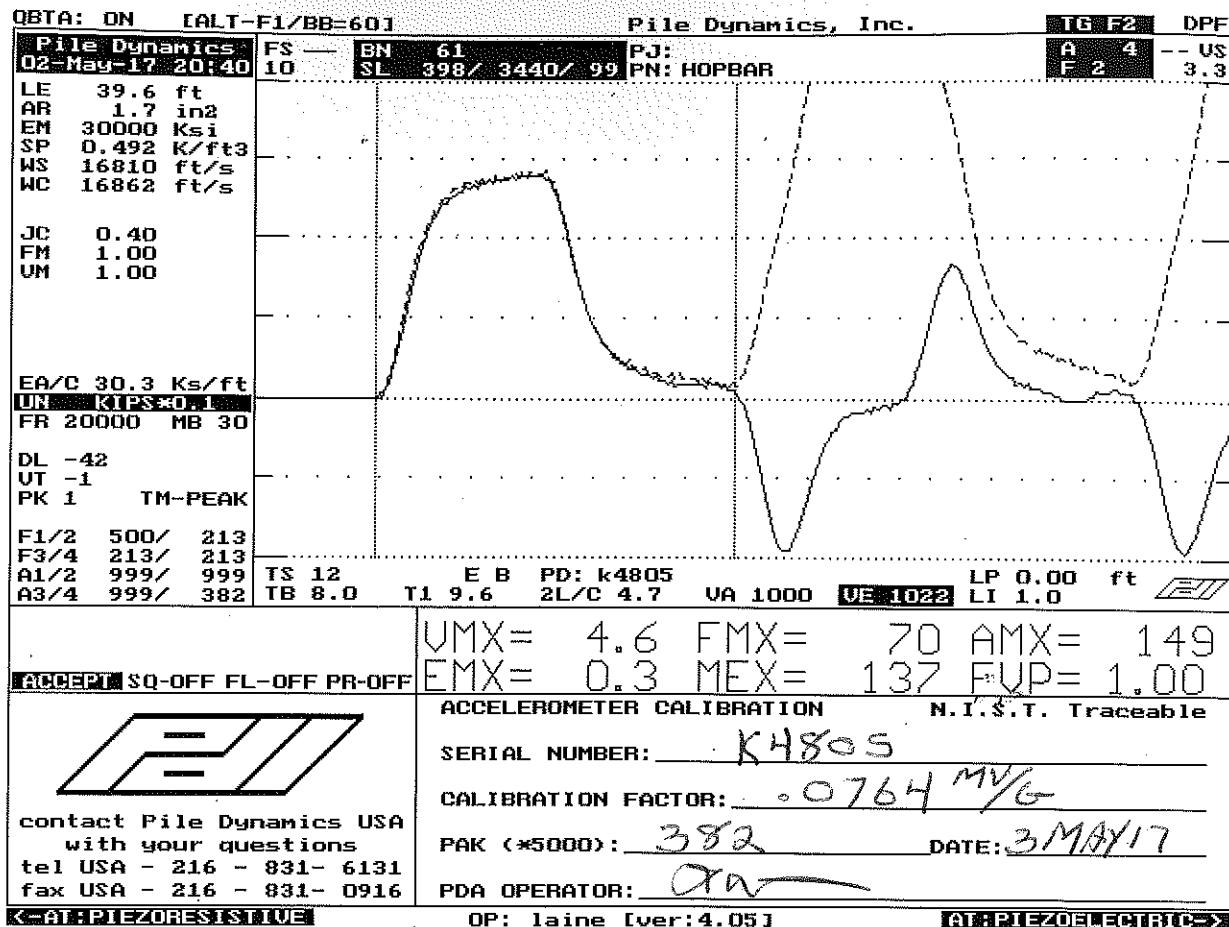
Bridge Excitation (V) 5  
Shunt Resistor (ohm) 60.4k

Calibration Factors	231NWJ		
Bridge 1 ( $\mu$ E/V)	211.52	Bridge 2 ( $\mu$ E/V)	212.77
EA Factor (Kips)	43794.32	Area (in <sup>2</sup> )	1.46

Calibrated by:   
Calibrated Date: 9/28/2015

Pile Dynamics Inc  
30725 Aurora Rd  
Solon, OH 44139

Traceable to N.I.S.T.



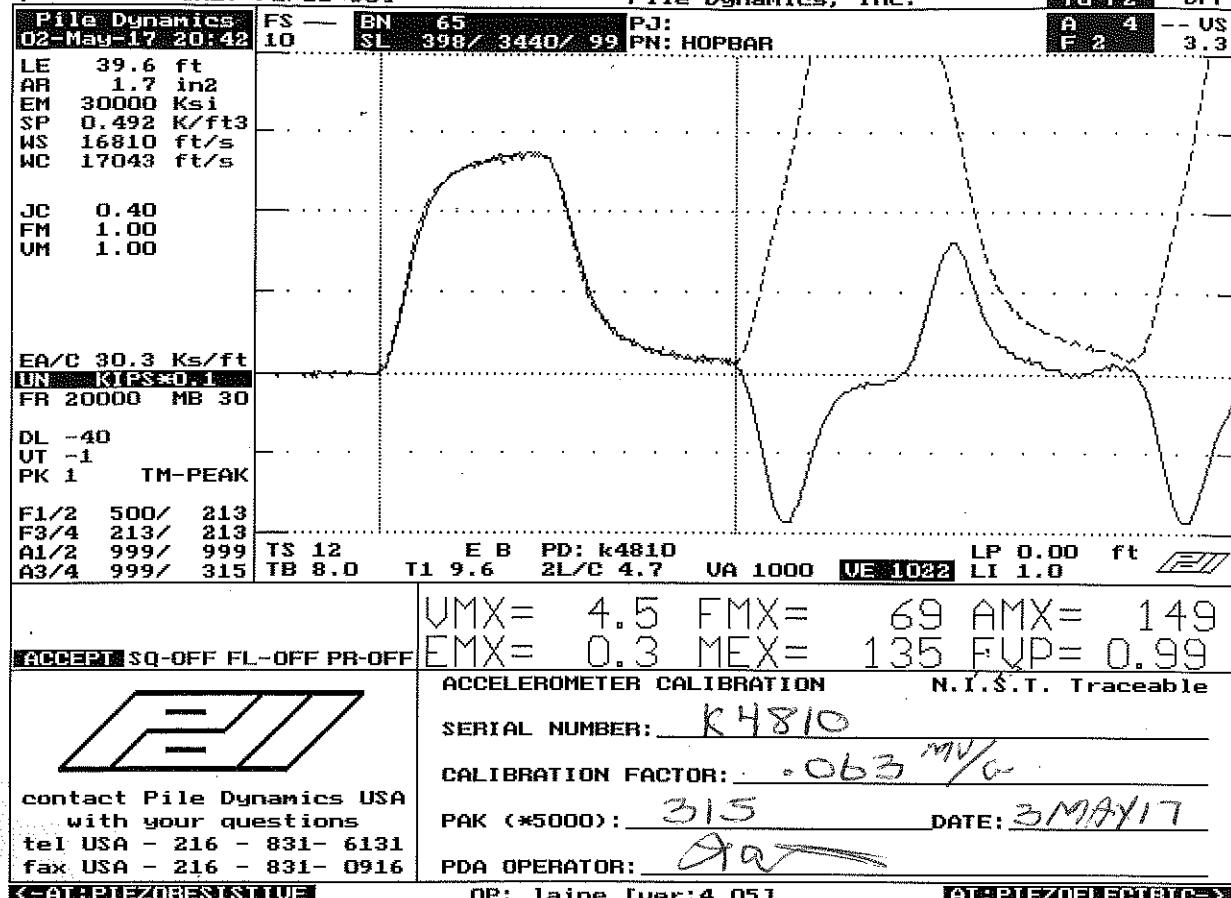
Smart Sensor

Smart Chip Programmed By Z.M.W on 3 MAY 17 CRC Value B578

QBTA: ON [ALT-F1/BB=60]

Pile Dynamics, Inc.

TG F2 DPF



## Smart Sensor

Smart Chip Programmed By M.W. on 3MAY17 CRC Value 9E7A

# *Certificate of Calibration*

**Pile Dynamics, Inc. certifies that the**

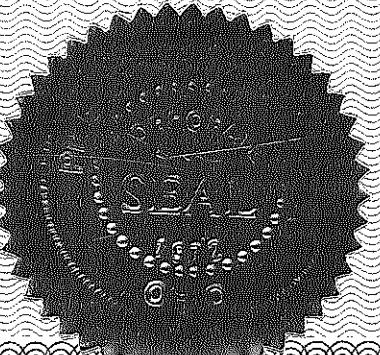
**Pile Driving Analyzer®, Model 8G**

**Serial Number: 4613 LE**

was calibrated on 4 May 2017

using a PDA Calibration Box whose output was calibrated with test equipment  
traceable to NIST.

This certificate is valid for 2 years from above date.



Tested by



Pile Dynamics, Inc.  
30725 Aurora Road  
Cleveland, Ohio 44139 USA

# **Appendix C**

## ***SPT Calibration Results***

### Summary of SPT Test Results

Project: Diedrich D-50 SN310, Test Date: 6/21/2017

FMX: Maximum Force

ETR: Energy Transfer Ratio - Rated

VMX: Maximum Velocity

DFN: Final Displacement

BPM: Blows/Minute

FVP: Force/Velocity Proportionality

EFV: Maximum Energy

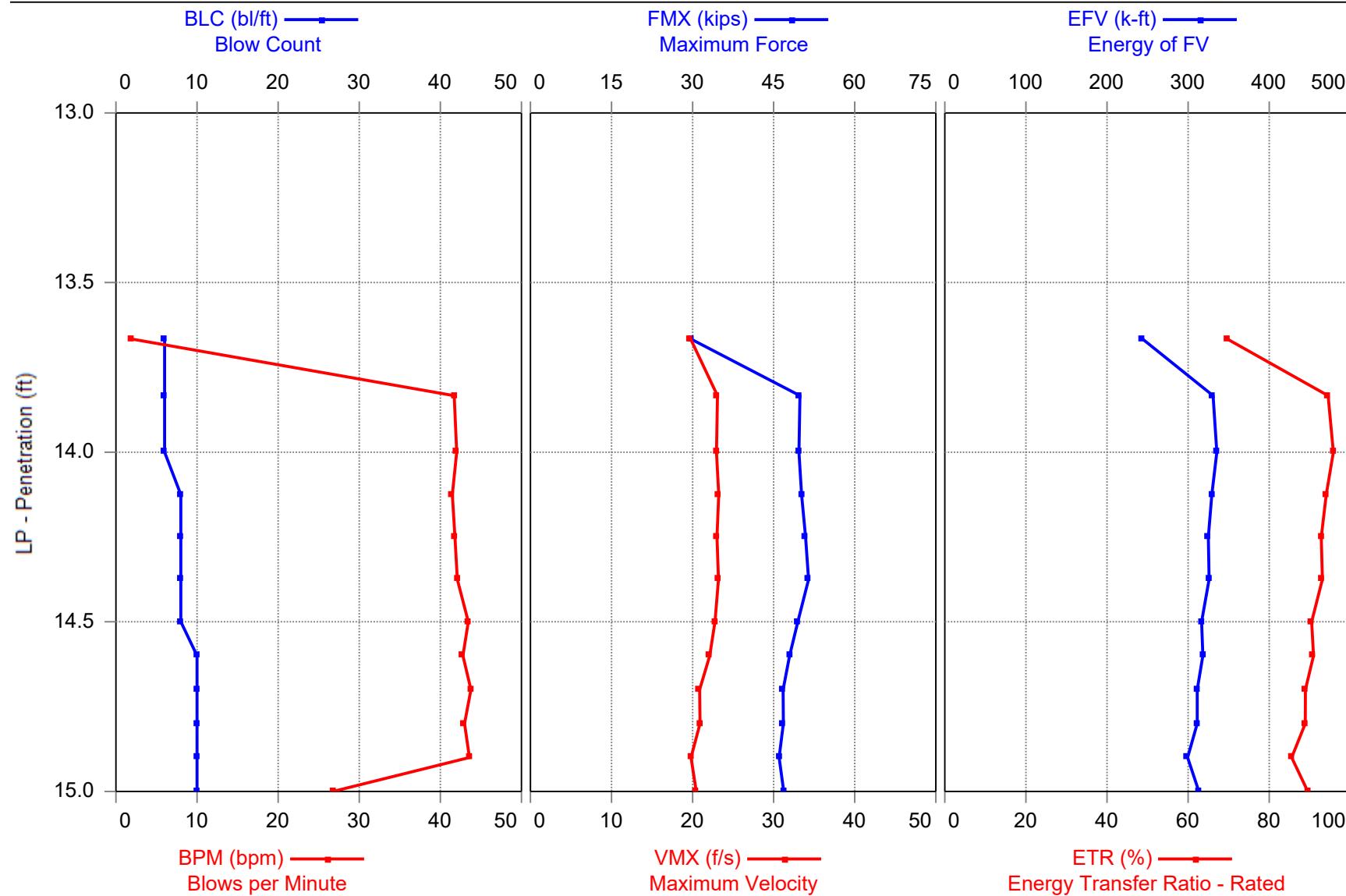
Instr. Length ft	Blows Applied /6"	Start Depth ft	Final Depth ft	N Value	N60 Value	Average FMX kips	Average VMX ft/s	Average BPM bpm	Average Efv ft-lb	Average ETR (%)	Average DFN in	Average FVP []
19.00	<b>3-4-5</b>	13.50	15.00	<b>9</b>	<b>14</b>	48	21.8	41.0	317	90.5	1.33	0.9
24.00	<b>3-6-8</b>	18.50	20.00	<b>14</b>	<b>21</b>	50	19.4	44.4	326	93.0	0.86	0.9
29.00	<b>4-8-11</b>	23.50	25.00	<b>19</b>	<b>29</b>	50	19.0	44.5	340	97.1	0.63	0.9
34.00	<b>5-6-9</b>	28.50	30.00	<b>15</b>	<b>23</b>	48	17.0	44.8	323	92.4	0.80	1.0
39.00	<b>7-10-15</b>	33.50	35.00	<b>25</b>	<b>39</b>	49	17.5	44.6	325	92.8	0.47	1.1
46.00	<b>4-4-6</b>	38.50	40.00	<b>10</b>	<b>15</b>	46	17.9	44.2	340	97.0	1.20	0.9
<b>Overall Average Values:</b>						49	18.5	44.2	329	93.9	0.78	1.0
<b>Standard Deviation:</b>						2	1.6	1.9	12	3.5	0.32	0.1
<b>Overall Maximum Value:</b>						52	23.2	45.4	357	102.1	1.50	1.1
<b>Overall Minimum Value:</b>						44	15.9	26.8	299	85.5	0.39	0.8

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 13.5-15



Diedrich D-50 SN310 - SS 13.5-15

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 19.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
3	14.0	6	AV3	29	43	21.9	303	87	29.5	2.39	2.00	0.90
7	14.5	8	AV4	42	50	23.0	324	93	34.6	2.09	1.50	0.88
12	15.0	10	AV5	40	47	20.8	311	89	32.1	1.30	1.20	0.89
Average				38	47	21.8	313	90	32.3	1.83	1.50	0.89

Total number of blows analyzed: 12

### Sensors

Blows: 1-12

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 16 seconds 9:00 AM - 9:00 AM BN 1 - 12

Diedrich D-50 SN310

JW

AR: 1.46 in<sup>2</sup>

LE: 19.00 ft

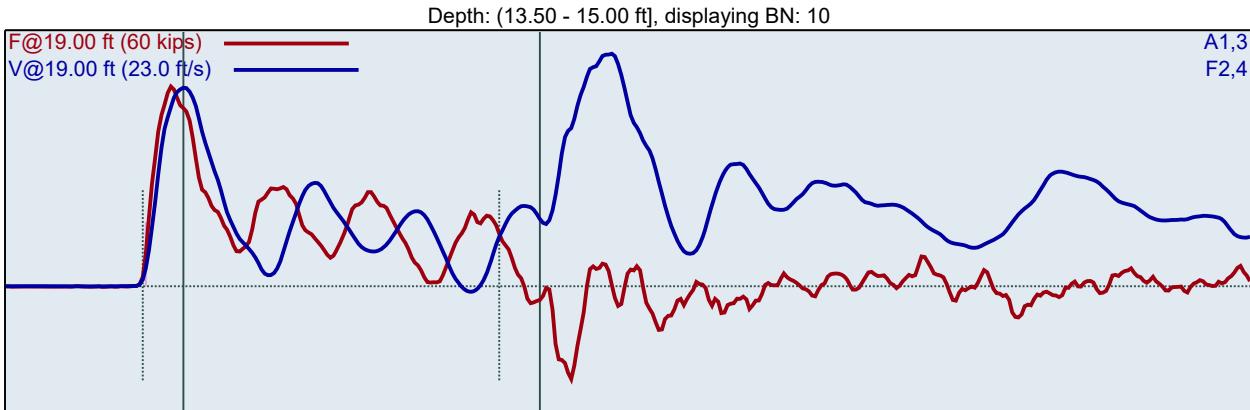
WS: 16807.9 ft/s

SS 13.5-15

Test date: 6/21/2017

SP: 0.492 k/ft<sup>3</sup>

EM: 30000 ksi



FMX: Maximum Force

ETR: Energy Transfer Ratio - Rated

VMX: Maximum Velocity

DFN: Final Displacement

BPM: Blows/Minute

FVP: Force/Velocity Proportionality

EFV: Maximum Energy

BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
1	3	13.67	30	19.8	1.9	244	69.7	2.00	0.9
2	3	13.83	50	23.1	41.7	331	94.5	2.00	0.9
3	3	14.00	50	22.9	42.0	335	95.8	2.00	0.9
4	4	14.13	50	23.2	41.5	329	94.1	1.50	0.9
5	4	14.25	51	23.0	41.8	325	92.9	1.50	0.9
6	4	14.38	51	23.2	42.1	326	93.1	1.50	0.9
7	4	14.50	49	22.8	43.4	317	90.5	1.50	0.9
8	5	14.60	48	22.1	42.8	318	90.9	1.20	0.9
9	5	14.70	47	20.9	43.8	311	88.9	1.20	0.9
10	5	14.80	47	20.9	43.0	311	88.9	1.20	0.9
11	5	14.90	46	19.8	43.6	299	85.5	1.20	0.9
12	5	15.00	47	20.4	26.8	313	89.5	1.20	0.9
		Average	48	21.8	41.0	317	90.5	1.33	0.9
		Std Dev	2	1.2	5.1	9	2.5	0.15	0.0
		Maximum	51	23.2	43.8	329	94.1	1.50	0.9
		Minimum	46	19.8	26.8	299	85.5	1.20	0.9
N-value: 9									

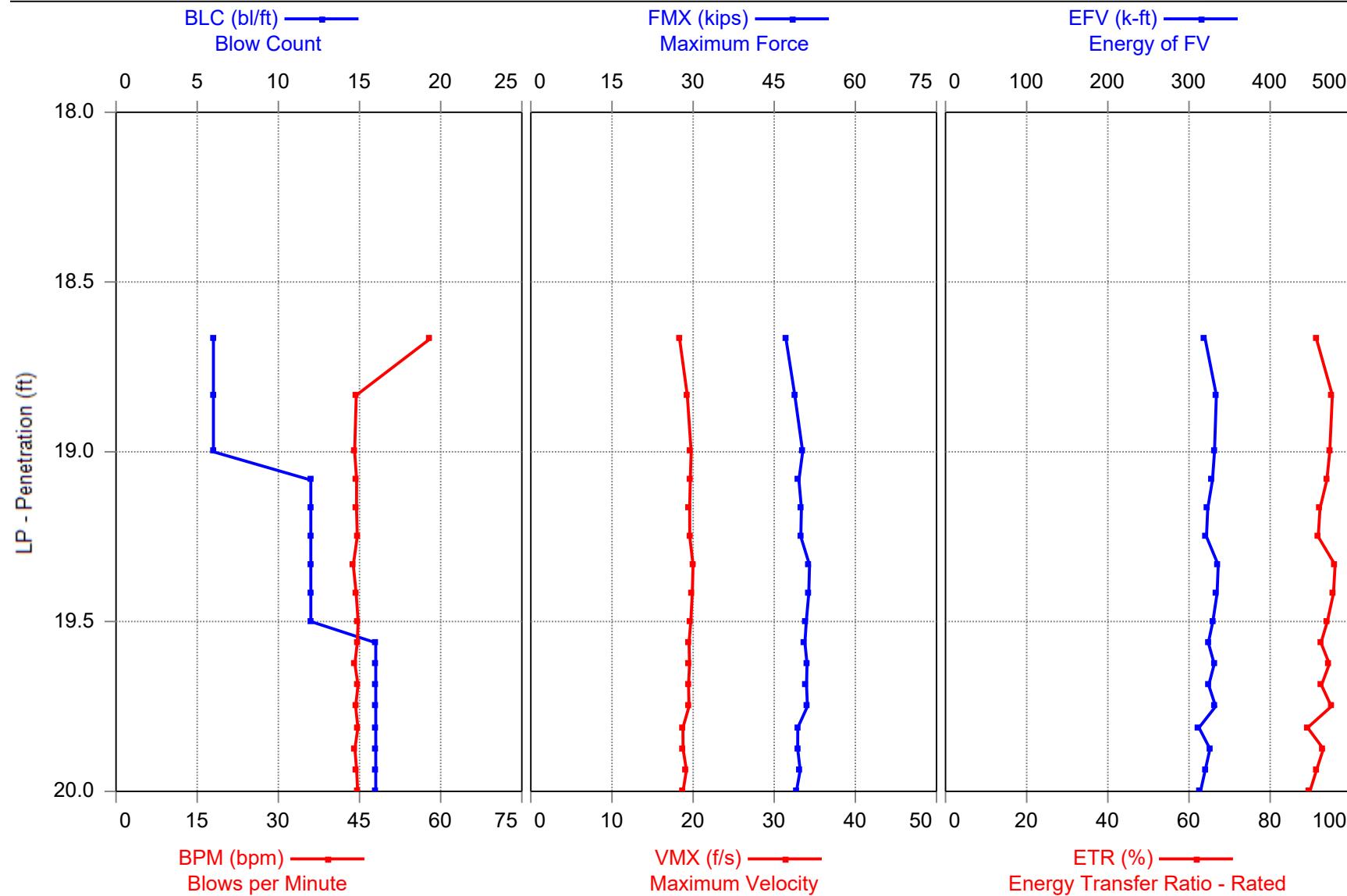
Sample Interval Time: 16.33 seconds.

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 18.5-20



Diedrich D-50 SN310 - SS 18.5-20

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 24.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
3	19.0	6	AV3	49	49	19.1	328	94	33.4	2.41	2.00	0.86
9	19.5	12	AV6	44	51	19.7	329	94	34.6	1.38	1.00	0.85
17	20.0	16	AV8	44	50	19.2	323	92	34.4	1.08	0.75	0.87
Average				45	50	19.4	326	93	34.3	1.42	1.06	0.86

Total number of blows analyzed: 17

### Sensors

Blows: 1-17

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 21 seconds 9:09 AM - 9:09 AM BN 1 - 17

Diedrich D-50 SN310

JW

AR: 1.46 in^2

LE: 24.00 ft

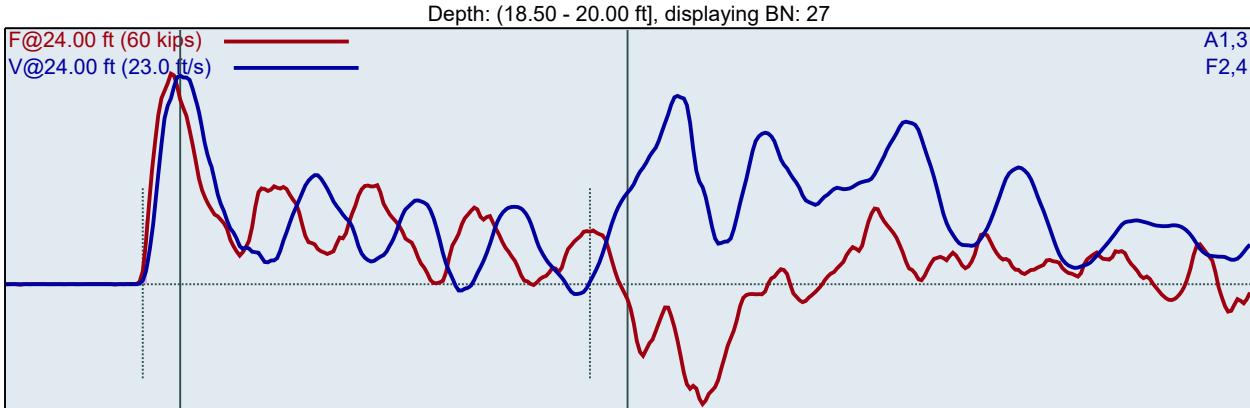
WS: 16807.9 ft/s

SS 13.5-15

Test date: 6/21/2017

SP: 0.492 k/ft<sup>3</sup>

EM: 30000 ksi



BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
13	3	18.67	47	18.3	58.1	320	91.4	2.00	0.9
14	3	18.83	49	19.3	44.4	334	95.3	2.00	0.9
15	3	19.00	50	19.8	44.1	331	94.7	2.00	0.8
16	6	19.08	50	19.7	44.5	329	94.0	1.00	0.9
17	6	19.17	50	19.6	44.4	323	92.3	1.00	0.8
18	6	19.25	50	19.6	44.6	322	91.9	1.00	0.9
19	6	19.33	52	20.0	43.8	336	96.0	1.00	0.8
20	6	19.42	51	19.9	44.4	335	95.6	1.00	0.8
21	6	19.50	51	19.7	44.7	329	94.1	1.00	0.9
22	8	19.56	51	19.5	44.6	324	92.5	0.75	0.8
23	8	19.63	51	19.6	44.2	331	94.6	0.75	0.9
24	8	19.69	51	19.4	44.7	324	92.7	0.75	0.9
25	8	19.75	51	19.5	44.3	333	95.1	0.75	0.9
26	8	19.81	49	18.7	44.7	312	89.2	0.75	0.9
27	8	19.88	49	18.8	44.2	326	93.1	0.75	0.9
28	8	19.94	50	19.2	44.5	320	91.4	0.75	0.9
29	8	20.00	49	18.8	44.7	314	89.8	0.75	0.9
Average		50	19.4	44.4	326	93.0	0.86	0.9	
Std Dev		1	0.4	0.3	7	2.0	0.12	0.0	
Maximum		52	20.0	44.7	336	96.0	1.00	0.9	
Minimum		49	18.7	43.8	312	89.2	0.75	0.8	

N-value: 14

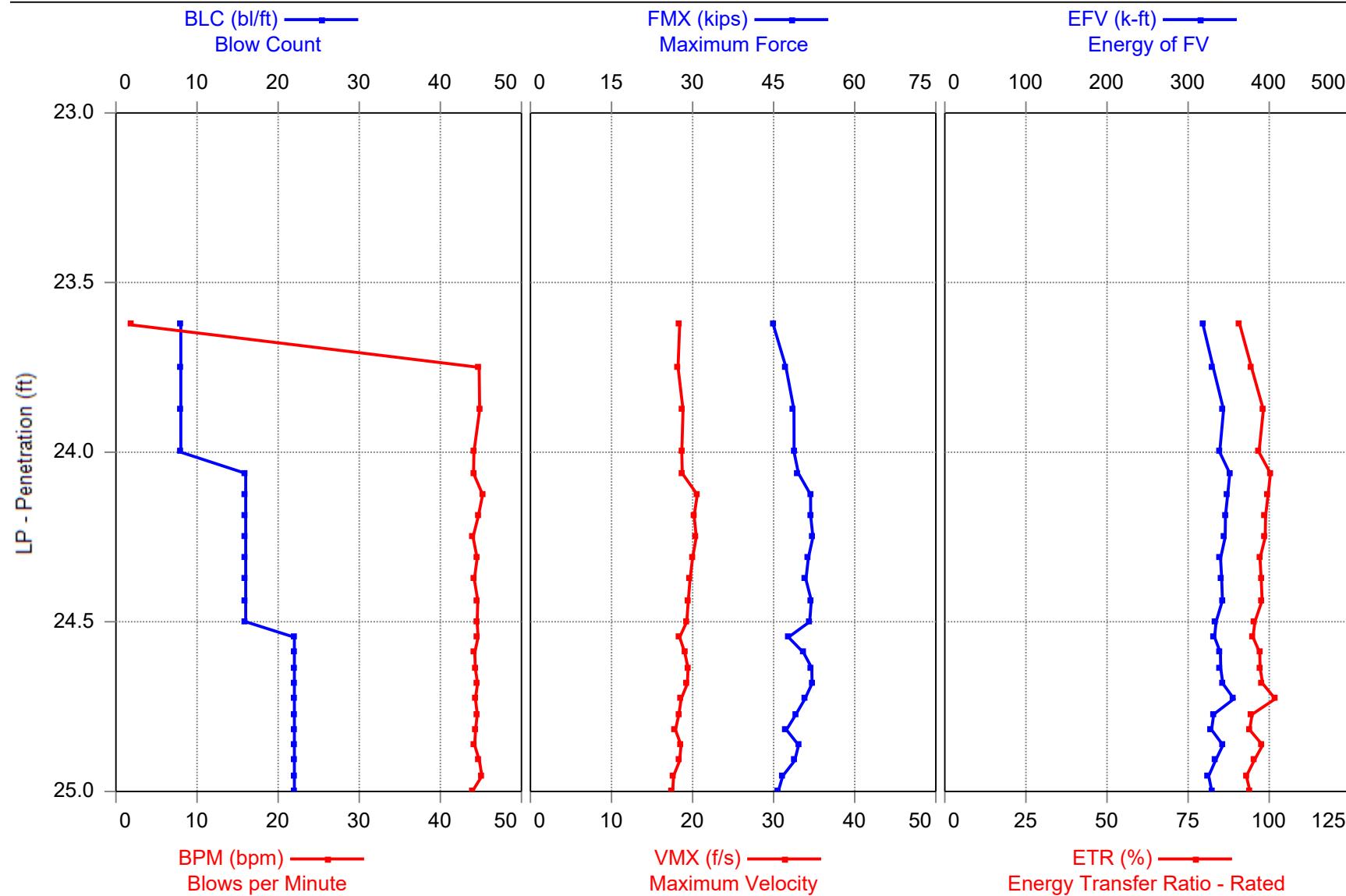
Sample Interval Time: 21.59 seconds.

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 23.5-25



Diedrich D-50 SN310 - SS 23.5-25

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 29.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
4	24.0	8	AV4	34	47	18.5	333	95	32.5	1.86	1.50	0.93
12	24.5	16	AV8	44	51	19.8	344	98	35.2	1.26	0.75	0.90
23	25.0	22	AV11	44	49	18.5	337	96	33.7	1.01	0.55	0.88
Average				43	50	18.9	339	97	34.0	1.24	0.78	0.89

Total number of blows analyzed: 23

### Sensors

Blows: 1-23

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 29 seconds 9:18 AM - 9:19 AM BN 1 - 23

GRL Engineers, Inc.  
SPT Analyzer Results

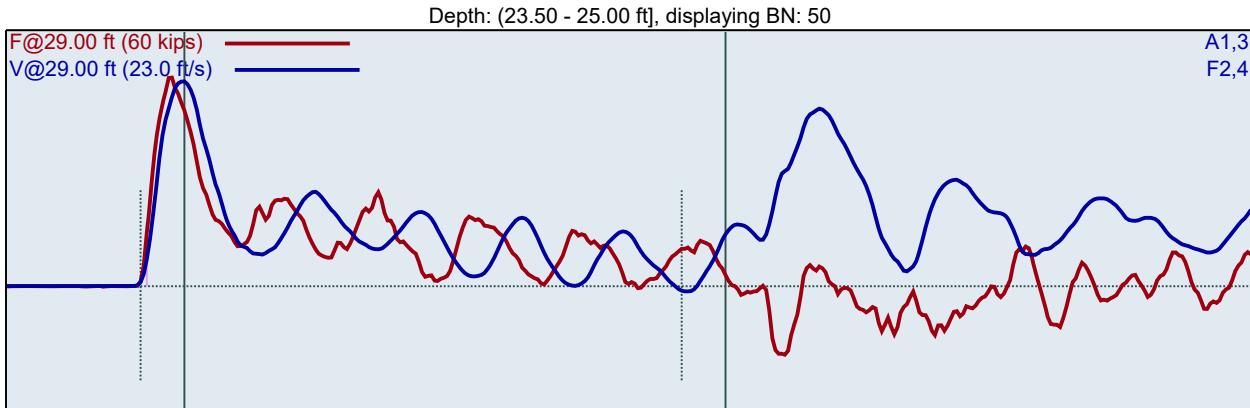
PDA-S Ver. 2017.18 - Printed: 6/23/2017

Diedrich D-50 SN310

JW

AR: 1.46 in<sup>2</sup>  
LE: 29.00 ft  
WS: 16807.9 ft/s

SS 13.5-15  
Test date: 6/21/2017  
SP: 0.492 k/ft<sup>3</sup>  
EM: 30000 ksi



BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
30	4	23.63	45	18.4	1.9	318	91.0	1.50	0.9
31	4	23.75	47	18.2	44.8	331	94.6	1.50	0.9
32	4	23.88	49	18.8	44.8	344	98.2	1.50	0.9
33	4	24.00	49	18.7	44.1	339	96.8	1.50	0.9
34	8	24.06	50	18.7	44.1	351	100.4	0.75	0.9
35	8	24.13	52	20.6	45.2	349	99.7	0.75	0.9
36	8	24.19	52	20.2	44.7	346	98.9	0.75	0.9
37	8	24.25	52	20.5	44.0	346	98.8	0.75	0.9
38	8	24.31	51	20.0	44.5	340	97.2	0.75	0.9
39	8	24.38	51	19.7	44.2	341	97.6	0.75	0.9
40	8	24.44	52	19.5	44.6	342	97.8	0.75	0.9
41	8	24.50	52	19.3	44.5	335	95.6	0.75	0.9
42	11	24.55	48	18.4	44.6	333	95.0	0.54	0.9
43	11	24.59	51	19.0	44.2	340	97.1	0.55	0.9
44	11	24.64	52	19.4	44.3	340	97.2	0.55	0.8
45	11	24.68	52	19.4	44.6	343	98.0	0.55	0.8
46	11	24.73	51	18.6	44.3	356	101.9	0.55	0.9
47	11	24.77	49	18.3	44.6	332	94.8	0.54	0.9
48	11	24.82	47	17.9	44.3	329	94.0	0.54	0.9
49	11	24.86	50	18.6	44.2	343	98.0	0.55	0.9
50	11	24.91	49	18.4	44.8	334	95.4	0.54	0.9
51	11	24.95	47	17.7	45.1	325	93.0	0.55	0.9
52	11	25.00	46	17.5	43.9	329	94.1	0.55	0.9
Average		50	19.0	44.5	340	97.1	0.63	0.9	
Std Dev		2	0.9	0.3	8	2.3	0.10	0.0	
Maximum		52	20.6	45.2	356	101.9	0.75	0.9	
Minimum		46	17.5	43.9	325	93.0	0.54	0.8	

N-value: 19

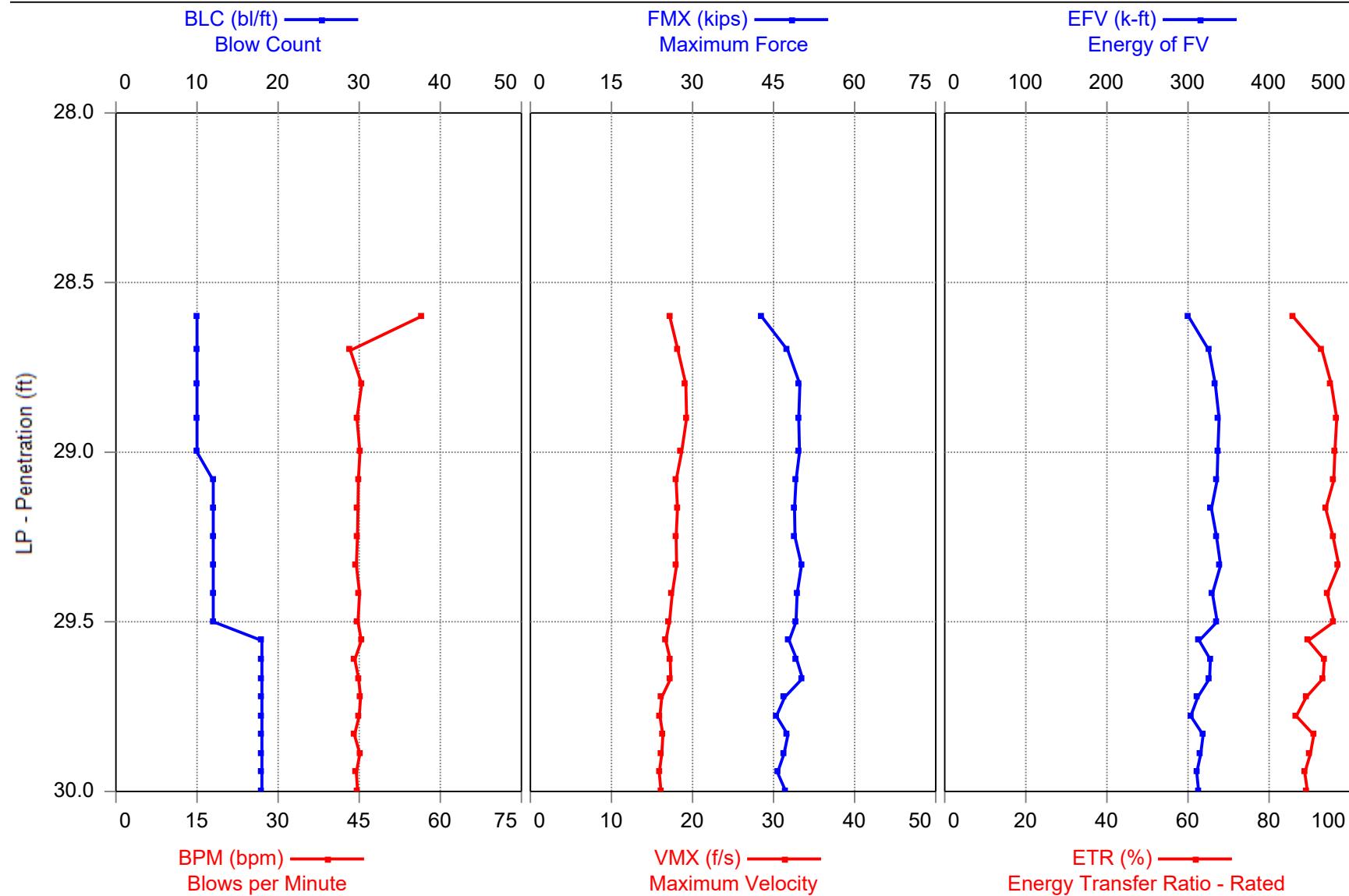
Sample Interval Time: 29.69 seconds.

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 28.5-30



Diedrich D-50 SN310 - SS 28.5-30

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 34.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
5	29.0	10	AV5	47	48	18.5	327	93	32.8	1.40	1.19	1.00
11	29.5	12	AV6	45	49	17.8	334	96	33.8	1.01	1.00	1.04
20	30.0	18	AV9	45	48	16.4	316	90	32.5	0.74	0.66	1.05
Average				45	48	17.4	324	93	33.0	0.99	0.90	1.04

Total number of blows analyzed: 20

### Sensors

Blows: 1-20

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 25 seconds 9:28 AM - 9:28 AM BN 1 - 20

GRL Engineers, Inc.  
SPT Analyzer Results

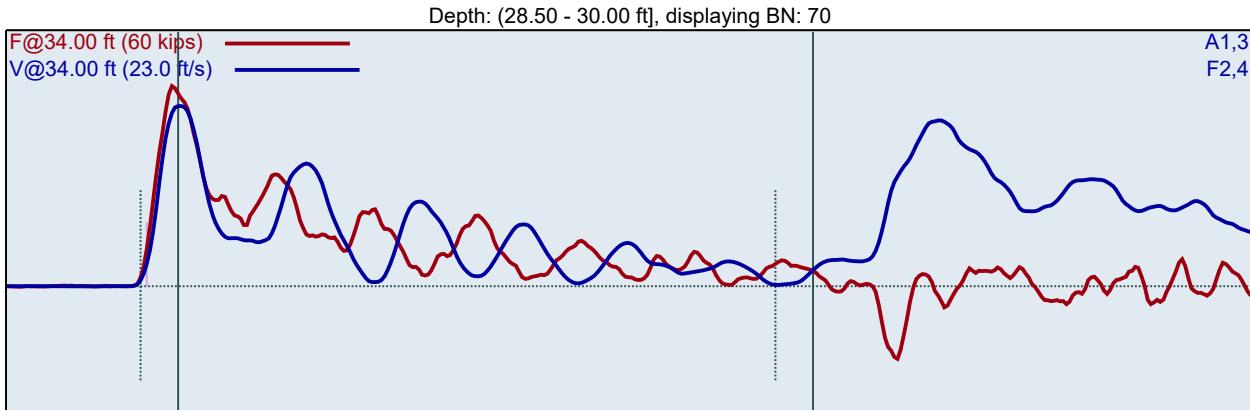
PDA-S Ver. 2017.18 - Printed: 6/23/2017

Diedrich D-50 SN310

JW

AR: 1.46 in<sup>2</sup>  
LE: 34.00 ft  
WS: 16807.9 ft/s

SS 13.5-15  
Test date: 6/21/2017  
SP: 0.492 k/ft<sup>3</sup>  
EM: 30000 ksi



BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
53	5	28.60	43	17.2	56.5	301	85.9	1.20	0.9
54	5	28.70	48	18.2	43.4	326	93.1	1.19	1.0
55	5	28.80	50	19.2	45.5	334	95.4	1.19	1.0
56	5	28.90	50	19.3	44.6	338	96.7	1.19	1.0
57	5	29.00	50	18.7	45.1	337	96.2	1.20	1.0
58	6	29.08	49	18.0	44.8	336	96.0	1.00	1.0
59	6	29.17	49	18.1	44.8	329	94.0	1.00	1.1
60	6	29.25	49	18.0	44.7	335	95.8	1.00	1.0
61	6	29.33	50	18.0	44.5	340	97.2	1.00	1.0
62	6	29.42	49	17.5	45.1	330	94.4	1.00	1.0
63	6	29.50	49	17.2	44.8	336	96.0	1.00	1.1
64	9	29.56	48	16.7	45.4	314	89.7	0.66	1.1
65	9	29.61	49	17.2	44.2	328	93.6	0.66	1.0
66	9	29.67	50	17.3	44.9	327	93.3	0.66	1.0
67	9	29.72	47	16.2	45.2	312	89.2	0.66	1.1
68	9	29.78	46	16.0	45.0	304	86.7	0.66	1.0
69	9	29.83	48	16.4	44.1	319	91.0	0.66	1.1
70	9	29.89	47	16.2	45.1	316	90.2	0.66	1.1
71	9	29.94	46	15.9	44.5	311	88.8	0.66	1.1
72	9	30.00	47	16.1	44.7	313	89.4	0.66	1.1
Average		48	17.0	44.8	323	92.4	0.80	1.0	
Std Dev		1	0.8	0.4	11	3.1	0.16	0.0	
Maximum		50	18.1	45.4	340	97.2	1.00	1.1	
Minimum		46	15.9	44.1	304	86.7	0.66	1.0	
N-value: 15									

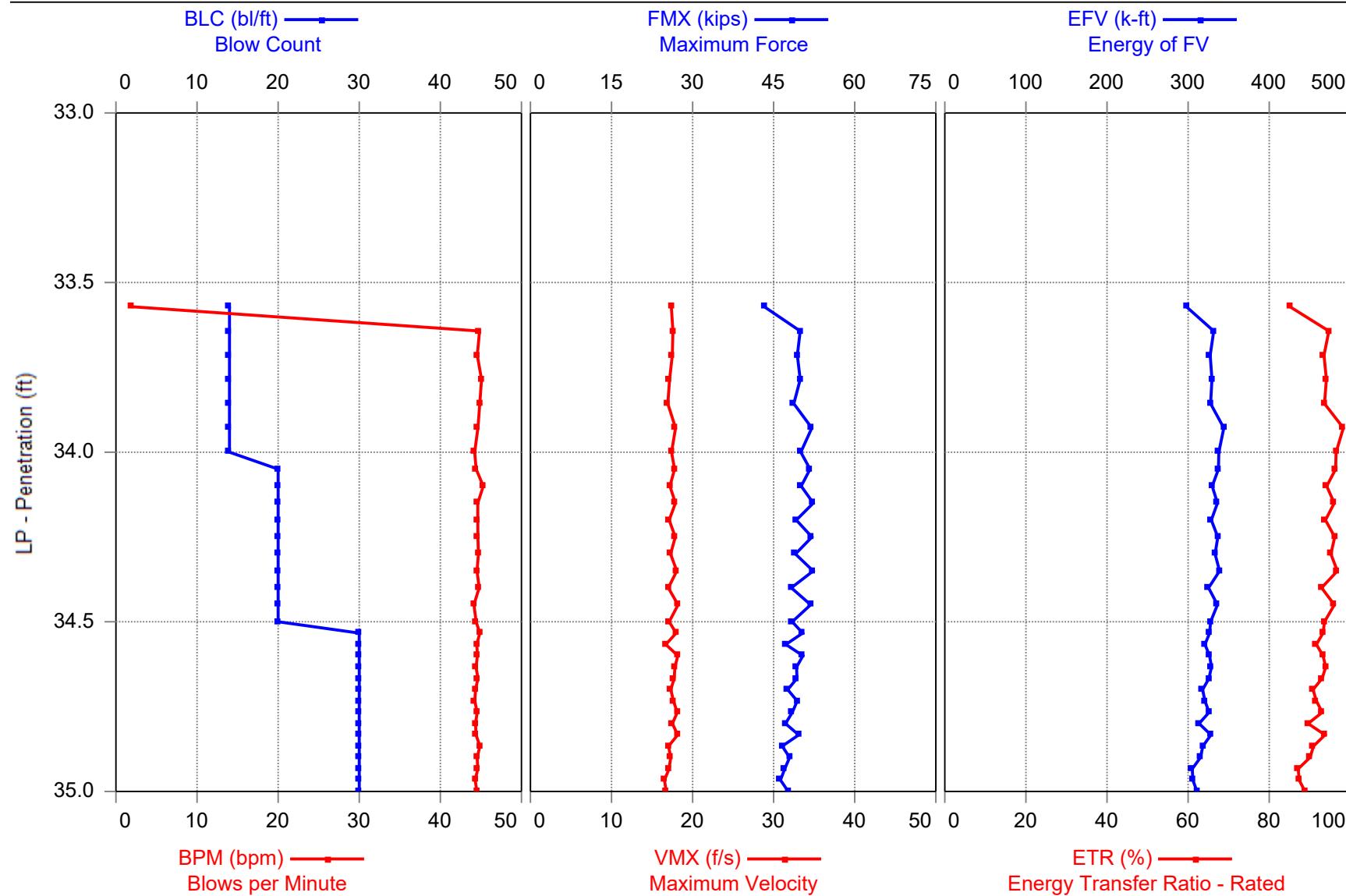
Sample Interval Time: 25.44 seconds.

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 33.5-35



Diedrich D-50 SN310 - SS 33.5-35

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 39.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
7	34.0	14	AV7	39	49	17.4	328	94	33.6	0.93	0.85	1.05
17	34.5	20	AV10	45	51	17.6	333	95	34.6	0.63	0.59	1.09
32	35.0	30	AV15	45	48	17.5	319	91	33.1	0.47	0.40	1.05
Average				43	49	17.5	325	93	33.7	0.62	0.56	1.06

Total number of blows analyzed: 32

### Sensors

Blows: 1-32

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 41 seconds 9:38 AM - 9:39 AM BN 1 - 32

GRL Engineers, Inc.  
SPT Analyzer Results

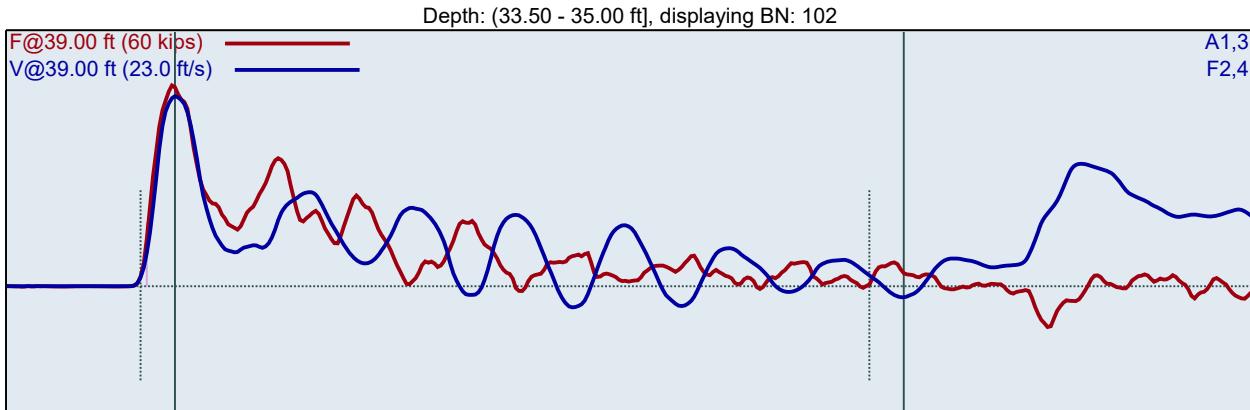
PDA-S Ver. 2017.18 - Printed: 6/23/2017

Diedrich D-50 SN310

JW

AR: 1.46 in<sup>2</sup>  
LE: 39.00 ft  
WS: 16807.9 ft/s

SS 13.5-15  
Test date: 6/21/2017  
SP: 0.492 k/ft<sup>3</sup>  
EM: 30000 ksi



BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
73	7	33.57	43	17.4	1.9	298	85.1	0.84	1.0
74	7	33.64	50	17.6	44.8	332	94.7	0.85	1.1
75	7	33.71	49	17.5	44.6	327	93.5	0.85	1.0
76	7	33.79	50	17.2	45.1	329	94.1	0.85	1.1
77	7	33.86	49	16.9	44.9	328	93.6	0.85	1.1
78	7	33.93	52	17.9	44.6	344	98.3	0.85	1.1
79	7	34.00	50	17.4	44.2	338	96.5	0.85	1.1
80	10	34.05	52	17.8	44.4	337	96.4	0.59	1.1
81	10	34.10	50	17.2	45.3	330	94.2	0.59	1.1
82	10	34.15	52	17.9	44.6	336	96.1	0.59	1.1
83	10	34.20	49	17.1	44.6	329	93.9	0.59	1.1
84	10	34.25	52	17.9	44.6	337	96.2	0.59	1.1
85	10	34.30	49	17.3	44.7	333	95.2	0.60	1.1
86	10	34.35	52	18.1	44.5	339	96.8	0.60	1.1
87	10	34.40	48	17.0	44.8	325	92.9	0.59	1.1
88	10	34.45	52	18.2	44.1	336	96.1	0.60	1.1
89	10	34.50	48	17.1	44.4	328	93.6	0.59	1.1
90	15	34.53	50	18.0	44.9	326	93.3	0.40	1.0
91	15	34.57	47	16.7	44.5	321	91.7	0.40	1.1
92	15	34.60	50	18.2	44.6	326	93.3	0.40	1.1
93	15	34.63	49	17.8	44.4	329	93.9	0.40	1.1
94	15	34.67	49	17.7	44.6	326	93.1	0.40	1.0
95	15	34.70	48	17.3	44.3	318	90.8	0.40	1.0
96	15	34.73	49	17.6	44.2	321	91.7	0.39	1.1
97	15	34.77	48	18.1	44.5	326	93.1	0.39	1.0
98	15	34.80	47	17.5	44.3	314	89.6	0.39	1.0
99	15	34.83	50	18.2	44.4	328	93.8	0.39	1.0
100	15	34.87	47	17.0	44.9	318	90.9	0.40	1.0
101	15	34.90	48	17.3	44.5	315	90.1	0.40	1.0
102	15	34.93	47	17.1	44.6	305	87.2	0.40	1.0
103	15	34.97	46	16.5	44.3	306	87.4	0.40	1.1
104	15	35.00	48	16.7	44.5	311	88.8	0.40	1.1

GRL Engineers, Inc.

SPT Analyzer Results

PDA-S Ver. 2017.18 - Printed: 6/23/2017

Average	49	17.5	44.6	325	92.8	0.47	1.1
Std Dev	2	0.5	0.2	9	2.7	0.10	0.0
Maximum	52	18.2	45.3	339	96.8	0.60	1.1
Minimum	46	16.5	44.1	305	87.2	0.39	1.0

N-value: 25

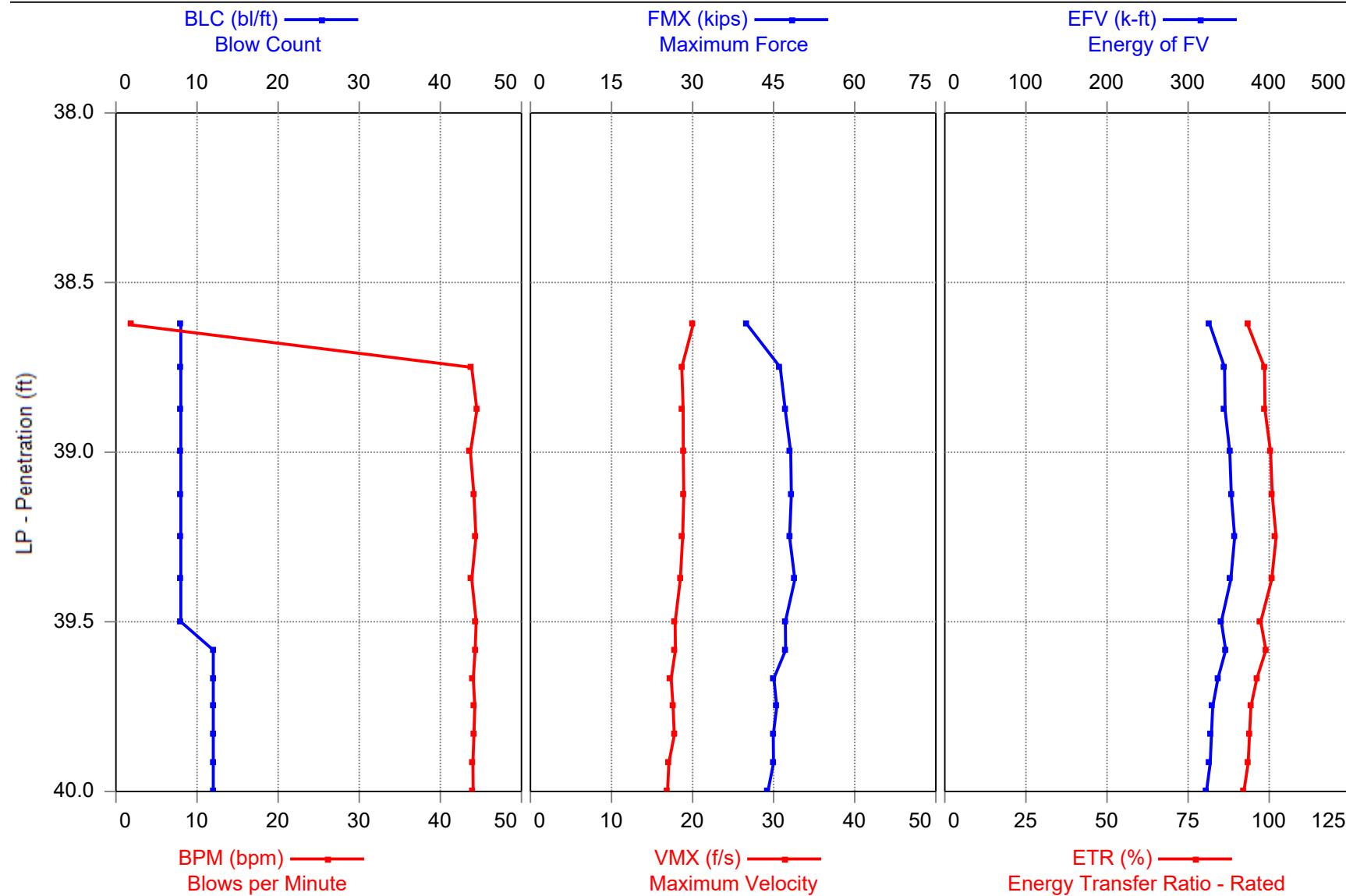
Sample Interval Time: 41.75 seconds.

Printed: 23-June-2017

Test started: 21-June-2017



## Diedrich D-50 SN310 - SS 38.5-40



Diedrich D-50 SN310 - SS 38.5-40

B2-4

OP: JW

Date: 21-June-2017

AR: 1.46 in<sup>2</sup>

SP: 0.492 k/ft<sup>3</sup>

LE: 46.00 ft

EM: 30,000 ksi

WS: 16,807.9 f/s

JC: 0.90 □

BPM: Blows per Minute

CSX: Max Measured Compr. Stress

FMX: Maximum Force

DMX: Maximum Displacement

VMX: Maximum Velocity

DFN: Final Displacement

EFV: Energy of FV

FVP: Force/Velocity proportionality

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC bl/ft	TYPE	BPM bpm	FMX kips	VMX f/s	EFV k-ft	ETR (%)	CSX ksi	DMX in	DFN in	FVP □
4	39.0	8	AV4	34	45	19.1	342	98	31.1	1.83	1.50	0.87
8	39.5	8	AV4	44	48	18.5	351	100	32.9	1.81	1.50	0.94
14	40.0	12	AV6	44	45	17.4	332	95	31.0	1.52	1.00	0.95
Average				41	46	18.2	340	97	31.6	1.69	1.29	0.92

Total number of blows analyzed: 14

### Sensors

Blows: 1-14

Sensor	Type	Serial Nr.	Calibration	Replay Factor
F2	Strain	231NWJ1	211.5	1.00
F4	Strain	231NWJ2	212.8	1.00
A1	PR Accel	K4810	315.0	1.00
A3	PR Accel	K4805	382.0	1.00

### Time Summary

Drive 17 seconds 9:51 AM - 9:51 AM BN 1 - 14

Diedrich D-50 SN310

JW

AR: 1.46 in^2

LE: 46.00 ft

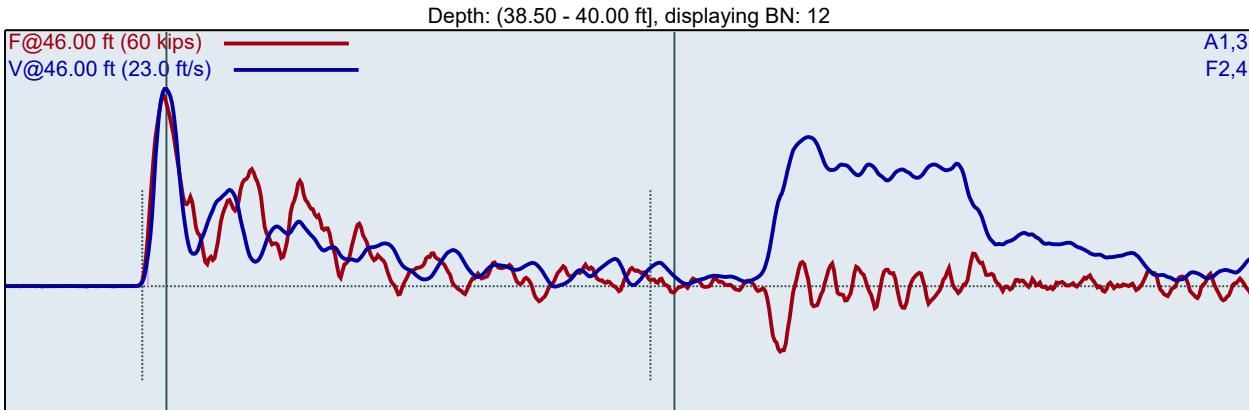
WS: 16807.9 ft/s

SS 38.5-40

Test date: 6/21/2017

SP: 0.492 k/ft<sup>3</sup>

EM: 30000 ksi



FMX: Maximum Force

ETR: Energy Transfer Ratio - Rated

VMX: Maximum Velocity

DFN: Final Displacement

BPM: Blows/Minute

FVP: Force/Velocity Proportionality

EFV: Maximum Energy

BL#	BC /6"	LP ft	FMX kips	VMX ft/s	BPM bpm	EFV ft-lb	ETR (%)	DFN in	FVP
1	4	38.63	40	20.1	1.9	327	93.4	1.50	0.8
2	4	38.75	46	18.7	43.9	345	98.6	1.50	0.9
3	4	38.88	47	18.8	44.5	346	98.7	1.50	0.9
4	4	39.00	48	18.9	43.7	352	100.4	1.50	0.9
5	4	39.13	48	18.9	44.1	353	101.0	1.50	0.9
6	4	39.25	48	18.8	44.4	357	102.1	1.50	0.9
7	4	39.38	49	18.5	43.9	353	100.8	1.50	1.0
8	4	39.50	47	17.8	44.4	341	97.4	1.50	0.9
9	6	39.58	47	17.9	44.3	346	99.0	1.00	0.9
10	6	39.67	45	17.4	44.1	337	96.2	1.00	1.0
11	6	39.75	46	17.6	44.2	330	94.4	1.00	1.0
12	6	39.83	45	17.7	44.1	329	93.9	1.00	0.9
13	6	39.92	45	17.1	44.0	327	93.5	1.00	1.0
14	6	40.00	44	16.9	44.1	323	92.2	1.00	1.0
Average			46	17.9	44.2	340	97.0	1.20	0.9
Std Dev			2	0.6	0.2	12	3.4	0.24	0.0
Maximum			49	18.9	44.4	357	102.1	1.50	1.0
Minimum			44	16.9	43.9	323	92.2	1.00	0.9

N-value: 10

Sample Interval Time: 17.69 seconds.